

# REMOTE SENSING DEVICES IN COLD CLIMATES

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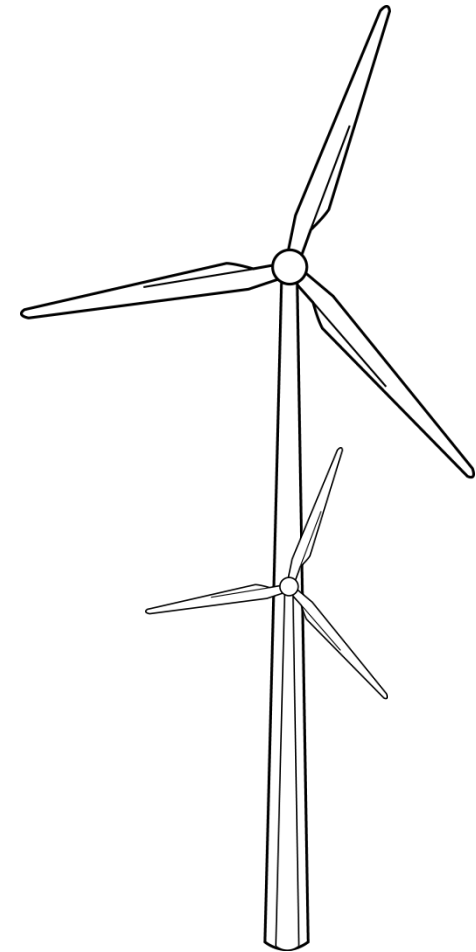
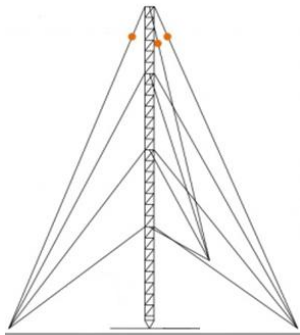
This work was funded by the Swedish Energy Agency  
(Energimyndigheten)

## MET MASTS AND REMOTE SENSING DEVICES: WHY

Met masts can:

- Characterise wind regime
- Aid turbine selection
- Reduce uncertainty
- Maximise project value

But...



## REMOTE SENSING DEVICES IN COLD CLIMATES

With increasing hub heights RSD have much to offer:

- Validate mast measurements at hub height and across the rotor diameter
- Provide hub height measured turbulence and extreme wind speed data
- Offer insight into the effects of low turbulence intensity and high shear on turbine energy yield



## REMOTE SENSING DEVICES IN COLD CLIMATES

This presentation will consider:

- The validation of mast measured shear
- The reliability of turbulence and extreme wind speed data from RSD
- The impact of low turbulence intensity and stable atmospheric conditions on energy content



## LIDAR V1 AT HAVSNÄS WIND FARM

## Remote Sensing Instrumentation Setup

- 1 power performance mast
  - Multiple heated & unheated instruments
- 1 WINDCUBE V1 LiDAR
  - 10 measurement heights
  - 50 m separation distance



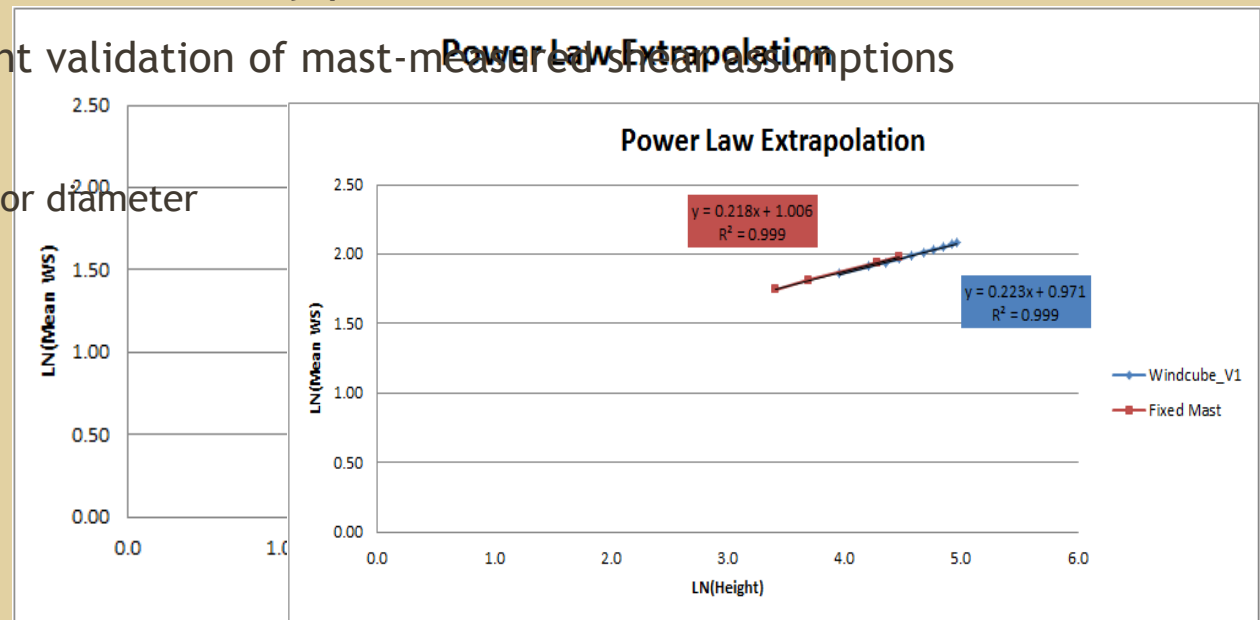
Three shear methodologies are used:

- One-point theoretical log law
  - Roughness length & displacement height
  - 1 wind speed measurement
  - Assume logarithmic profile
- Two-point power law
  - 2 wind speed measurements
  - Power law used for extrapolation
- Multi-point fitted log law
  - 3 or more wind speed measurements
  - Fitted logarithmic profile

## LiDAR-Mast Multi-Point Shear Comparison

- There is excellent agreement between fixed mast and WINDCUBE
  - Benefits from small separation distance for LiDAR devices
  - Different measurement techniques yet remarkable agreement
- ❖ The WINDCUBE-measured velocity profile

- provides excellent validation of mast-measured shear assumptions
  - To hub height
  - Across full rotor diameter



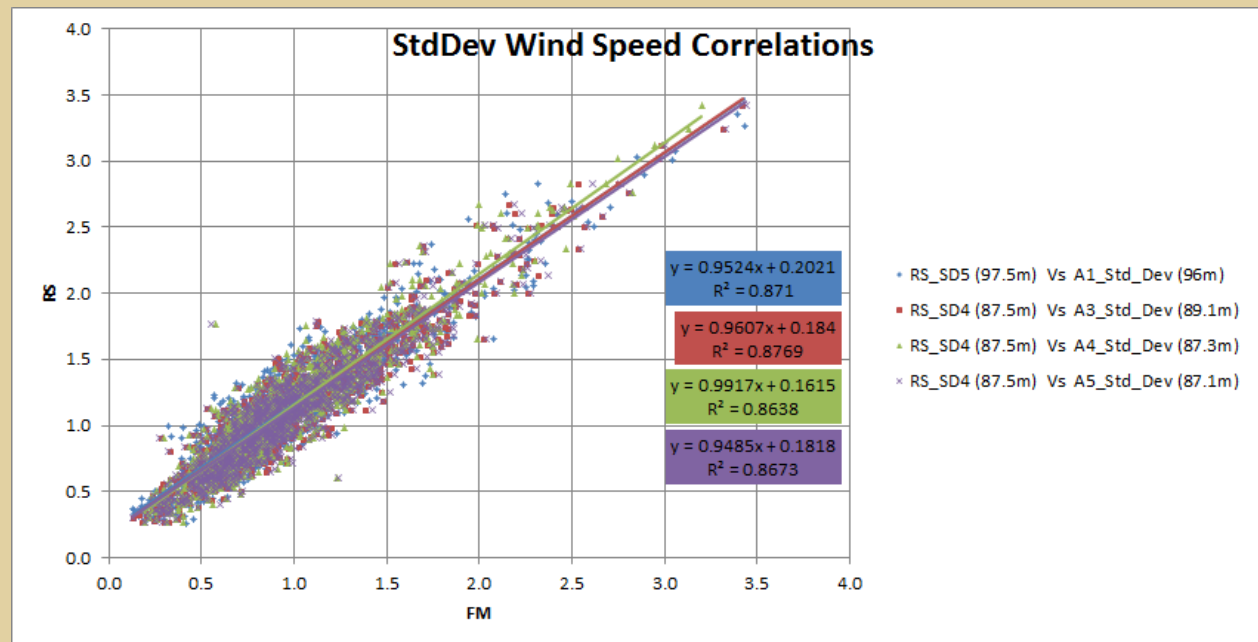


## Extrapolating measurements to hub height

- All three methods perform acceptably well, where
  - Forestry is well parameterised
  - Measurements are IEC-compliant
  - Class 1 anemometry is used
- On more complex sites
  - Theoretical log law is not recommended
- The multi-point method performs best overall
  - Leading to the lowest extrapolated wind speed error
  - Least sensitive to canopy height errors
- ❖ For extrapolating wind speed to hub height
  - The multi-point method is recommended

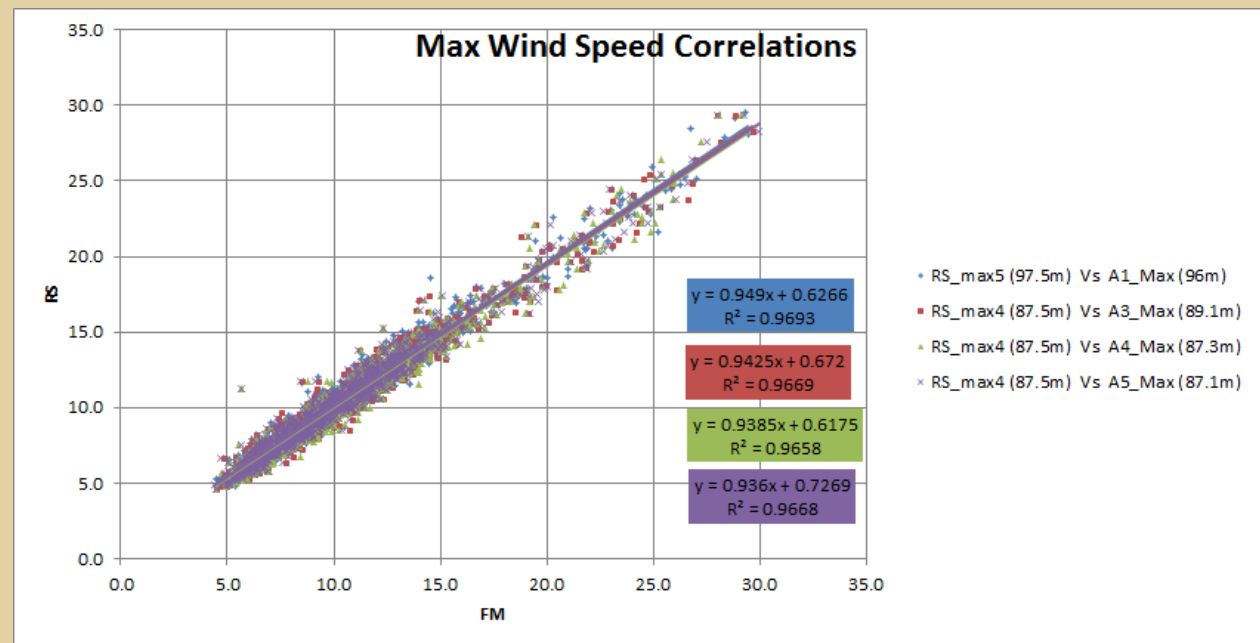
## RELIABILITY OF TURBULENCE DATA FROM WINDCUBE

- At Havsnäs, there is a well-defined relationship between the WINDCUBE and fixed mast standard deviation of mean wind speed data
- Slope variation
  - For very similar anemometer heights
  - Flow distortion experienced by anemometers is responsible for variation



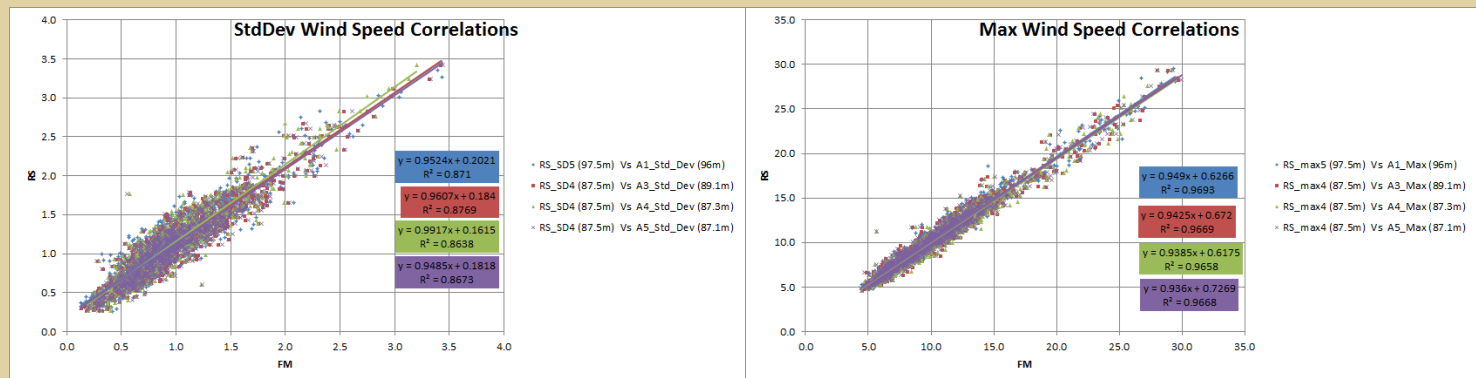
## RELIABILITY OF EXTREME WIND SPEED DATA FROM WINDCUBE

- At Havsnäs, there is a well-defined relationship between the WINDCUBE and fixed mast maximum wind speed data
- $\approx 6\%$  underestimation of maximum wind speed
  - Result of volume averaging
  - Gust underestimation



## RELIABILITY OF TURBULENCE AND EXTREME WIND SPEED DATA: FINDINGS

- At Havsnäs, there is a well-defined relationship for
  - Standard deviation of mean wind speed
  - Maximum wind speed
- Agrees with RES' prior experience
  - Variety of sites
  - Differing levels of terrain complexity
- ❖ WINDCUBE provides reliable turbulence and extreme wind speed data
  - Data should be examined on a deployment-by-deployment basis



## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: BACKGROUND

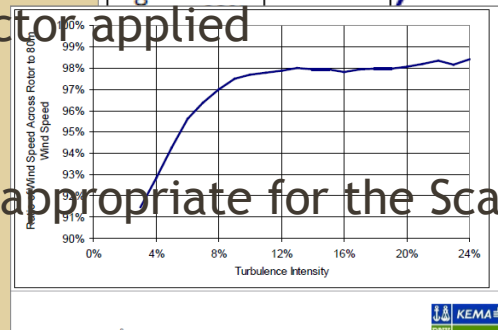
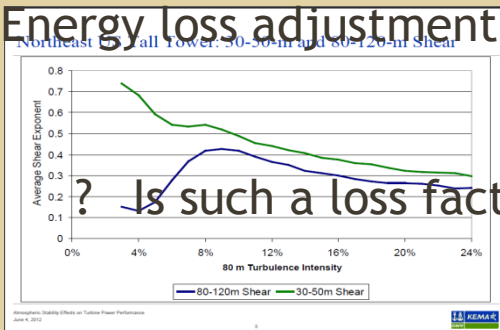
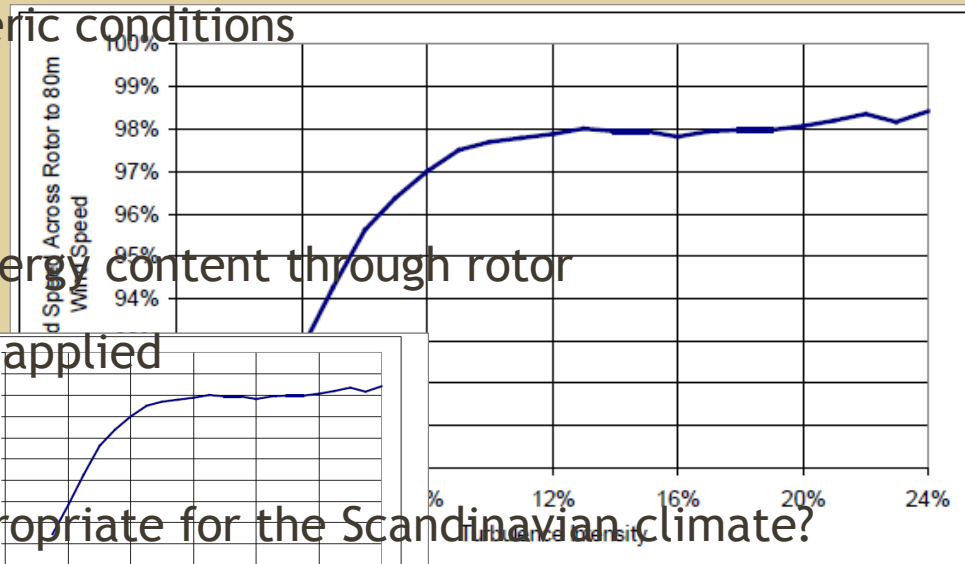
### DNV KEMA findings from northeast USA

- At turbulence intensities below  $\approx 9\%$ 
  - Shear not consistent across rotor
  - Hub height wind speed significantly overestimates energy through rotor

### • For sites with stable atmospheric conditions

- High shear
- Low TI
- ❖ Mast likely to overestimate energy content through rotor

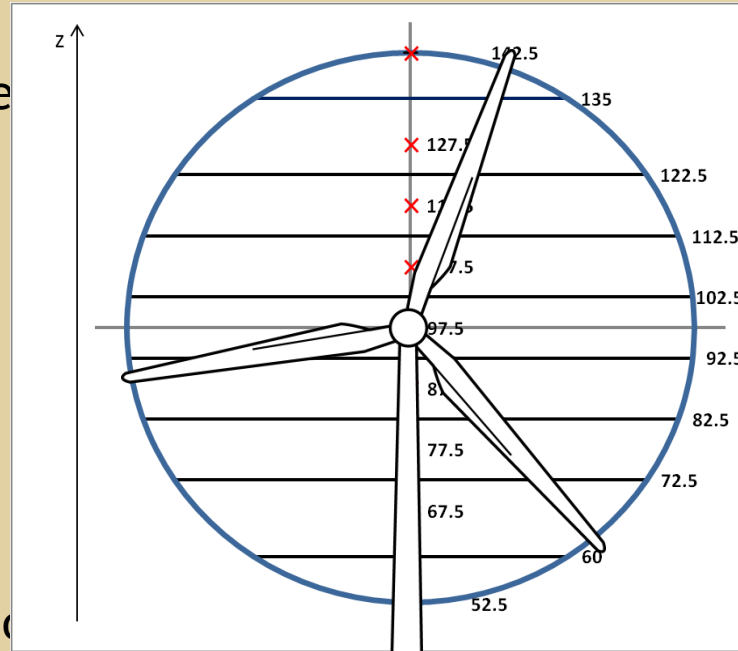
### ❖ Energy loss adjustment factor applied



? Is such a loss factor appropriate for the Scandinavian climate?

## IEC DEFINITIONS: EQUIVALENT WIND SPEED

The rotor-averaged or equivalent wind speed  $v_{eq}$  is defined as:



where

- $n$  is the number of segments ( $n \geq 3$ );
- $v_i$  is the wind speed measured at height  $z_i$ ;
- $A$  is the complete area swept by the rotor (i.e.  $\pi R^2$  with Radius  $R$ );
- $A_i$  is the area of the  $i$ th segment, i.e. the segment the wind speed  $v_i$  is representative for.

## IEC DEFINITIONS: SHEAR CORRECTION FACTOR

A shear correction factor is defined as a ratio of the equivalent wind speed relative to the wind speed measured at hub height according to

$$f_{r,X} = v_{eq,X} / v_{h,X}$$

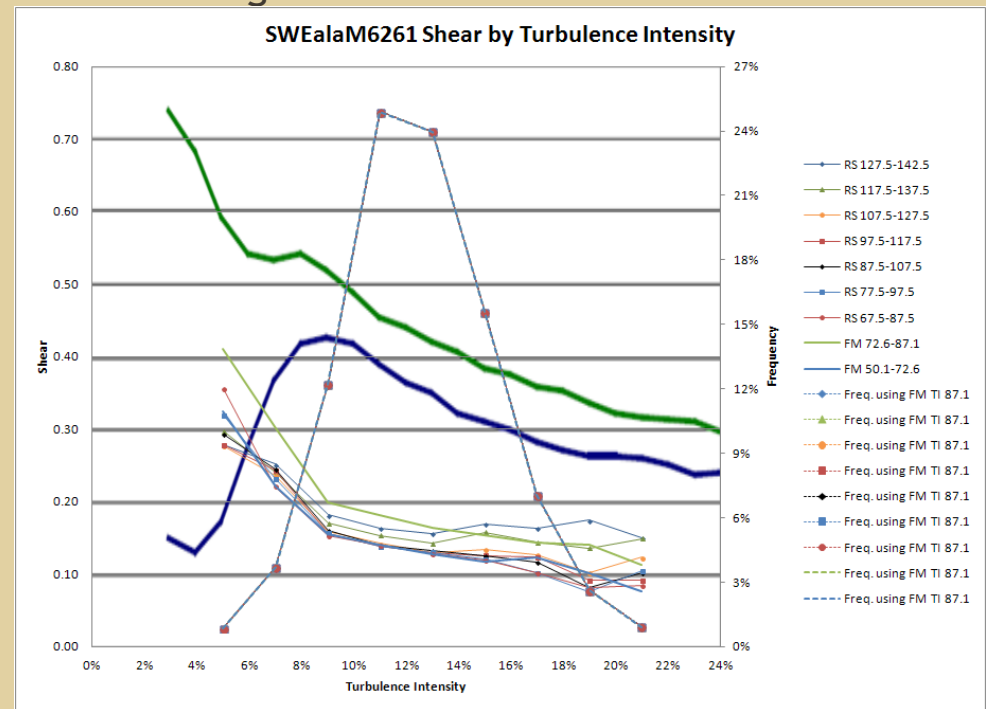
where

- $v_{eq,X}$  is the equivalent wind speed (as defined in previous slide);
- $v_{h,X}$  is the wind speed measured at hub height;
- and the index  $X$  specifies the instrument or instrument setup both,  $v_{eq,X}$  and  $v_{h,X}$ , are measured with.

It is also possible to calculate a shear correction factor for wind speed extrapolated to hub height, something that is done in this analysis.

## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: FINDINGS

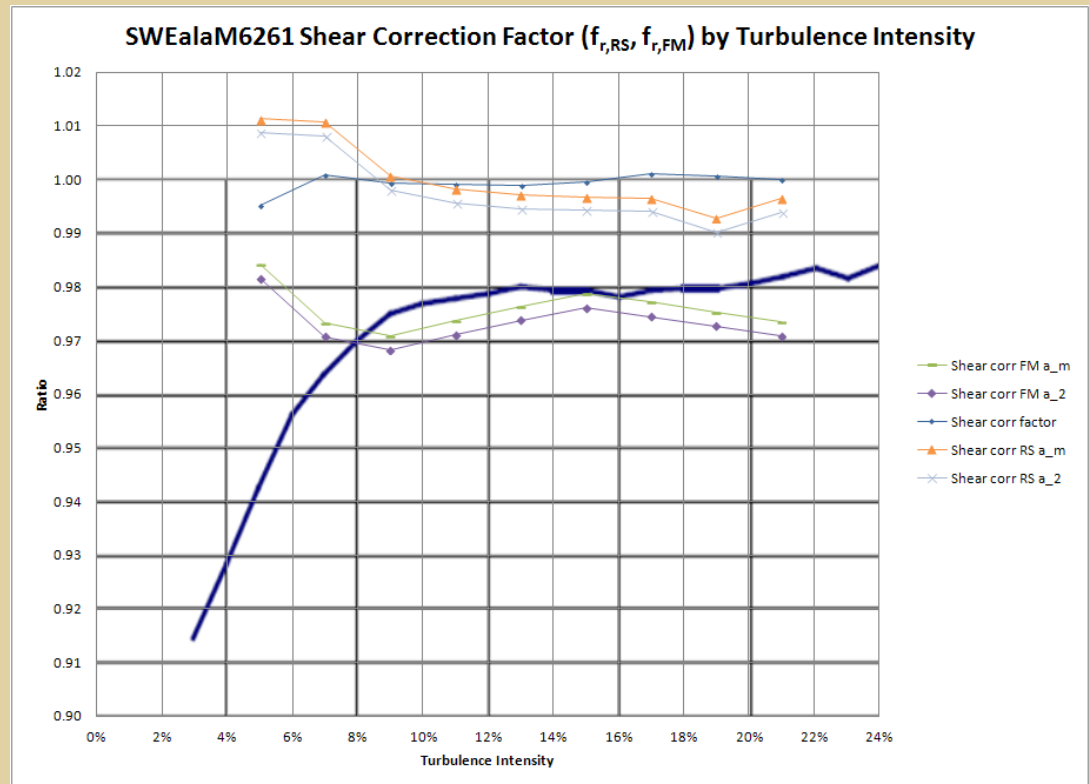
- Shear is consistent across full rotor
- At low TI
  - Turning point exists
  - But shear remains consistent across full range
  - No divergence at  $\approx 9\%$





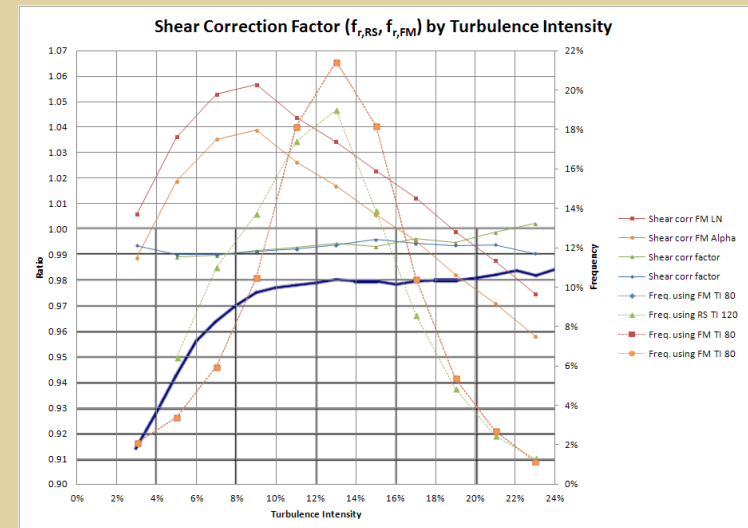
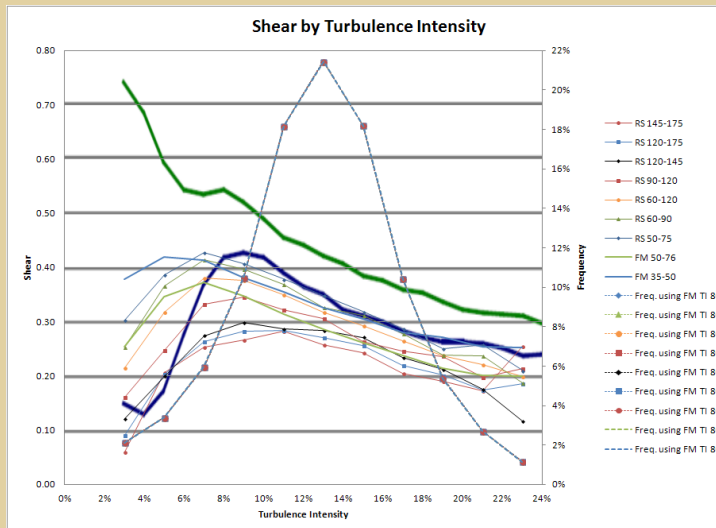
## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: FINDINGS

- Shear correction factors do not vary strongly with turbulence intensity
- At low TI
  - Turning point exists at  $\approx 9\%$
  - Small variation
  - No dramatic plunge



## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: FINDINGS

- ❖ The presence of low TI
  - Does not lead to an overestimation of hub height wind speed
  - Shear profile is not significantly over estimated by only using below hub height measurements
- ❖ Fixed mast measurements are likely to underestimate energy content
  - Findings are consistent with another Swedish site



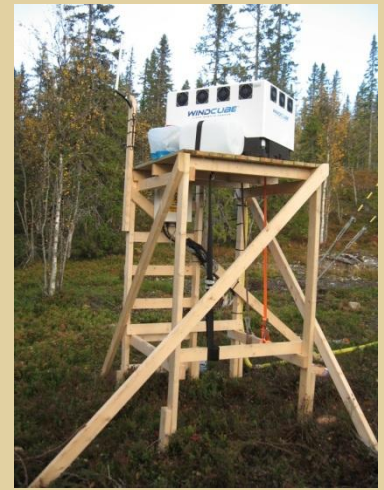
## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: CONCLUSIONS

- ❖ Justification for a universal energy loss adjustment factor is not evident
- ❖ What has been observed in the USA cannot simply be applied in other regions where stable atmospheric conditions prevail
  - Not all stable atmospheric conditions result in an overestimation of energy through the rotor diameter
- ❖ Each region should be treated separately
- ❖ Each individual site should be considered on its own merits
- ❖ RSD and long-term reference mast will indicate appropriateness of an energy loss adjustment factor

## BEST PRACTICE

Following best practice is very important! (For all RSD types)

- Device Siting
- Snow Platform
- IEC Measurement Height Recommendations
- Correctly Configured Measurement Heights
- Low Aerosol Configuration
- Cold Weather Insulation
- Device Monitoring
- Deploy Webcam



## SUMMARY: KEY POINTS

- Following best practice is very important
  - Maximise project value
- Multi-point shear most appropriate for extrapolation to hub height
  - Minimises error
- WINDCUBE gives excellent validation of mast-measured shear assumptions
  - Across full rotor
- WINDCUBE provides reliable turbulence and extreme wind speed data
  - Should be judged on a site-by-site basis
- RSD should be deployed to investigate impact of stability on rotor energy content
  - No negative impacts at Havsnäs or ‘Other Swedish Site’

## FINAL CONCLUSION

- ❖ The deployment of an appropriate RSD in conjunction with a long-term reference mast at each wind farm site
  - Is highly recommended
  - Will enable informed judgements to be taken
  - Minimise uncertainty
  - Maximise project value
- ❖ Full details of analysis in ‘Havsnäs Pilot Project Report’
  - With Swedish Energy Agency for publication

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# REMOTE SENSING DEVICES IN COLD CLIMATES

ADDITIONAL CONTENT





## WINDCUBE & FIXED MAST MEASUREMENT HEIGHTS

Mast	Sweden, RT90, National Map on 2.5 gon W		Mast Altitude (m ASL)	Anemometer Heights (m)	Vane Heights (m)	Data Currently Available
	X (m)	Y (m)				Dates
SWEalaM6261	1495312	7111825	521	30.1, 30.1, 50.1, 50.3, 70.8, 72.6, 72.8, 87.1, 87.3, 89.1, 96.0, 96.0	48.1, 48.3, 70.6, 85.1, 85.3	16/09/2011-25/07/2012

Mast	Sweden, RT90, National Map on 2.5 gon W		Mast Altitude (m ASL)	Measurement Heights (m)	Data Currently Available
	X (m)	Y (m)			Dates
SWEalaM814	1495302	7111875	520	52.5, 67.5, 77.5, 87.5, 97.5, 107.5, 117.5, 127.5, 137.5, 142.5	16/09/2011- 24/07/2012

## OPERATIONAL CONSIDERATIONS: DATA CAPTURE

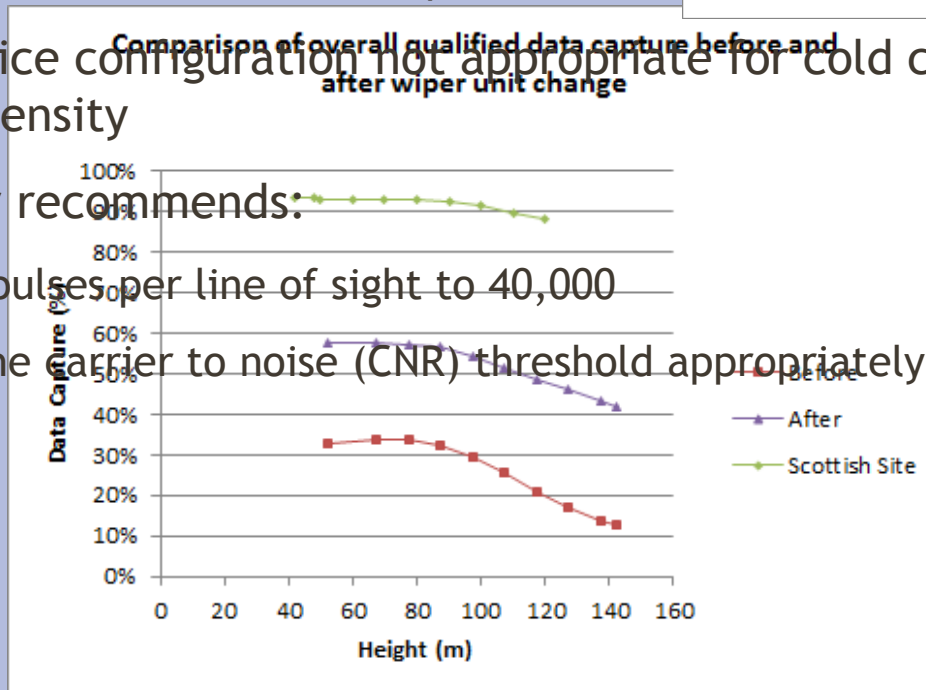
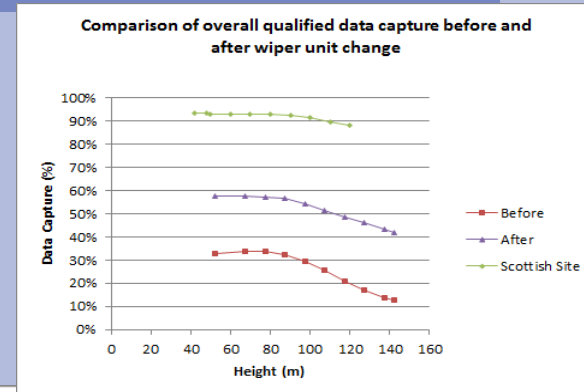
### Cold Climate: Clean air & low aerosol density

- Initial low data capture due to wiper failure
- Following wiper replacement:
  - Data capture still lower than expected

❖ Standard device configuration not appropriate for cold climate sites with low aerosol density

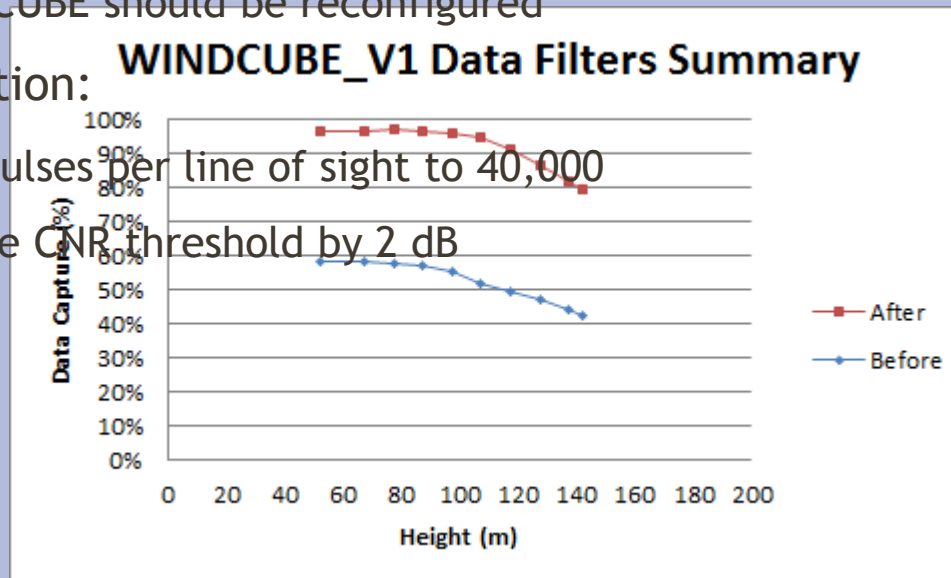
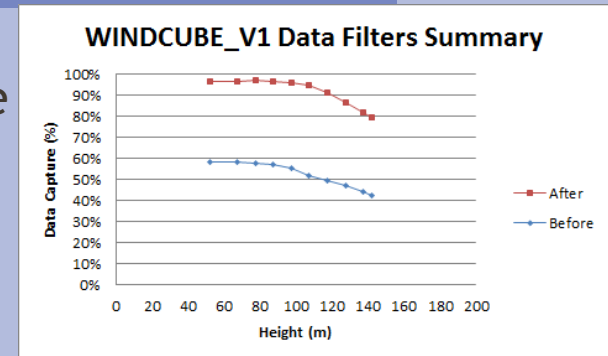
- Manufacturer recommends:

- Increase pulses per line of sight to 40,000
- Reduce the carrier to noise (CNR) threshold appropriately (2dB).



## OPERATIONAL CONSIDERATIONS: DEVICE RECONFIGURATION

- Reconfiguration results in increased data capture
  - Absolute increase around 37%
- Other aspects of device performance unaffected
- ❖ At sites with low aerosol densities
  - The WINDCUBE should be reconfigured
- ❖ Recommendation:
  - Increase pulses per line of sight to 40,000
  - Reduce the CNR threshold by 2 dB



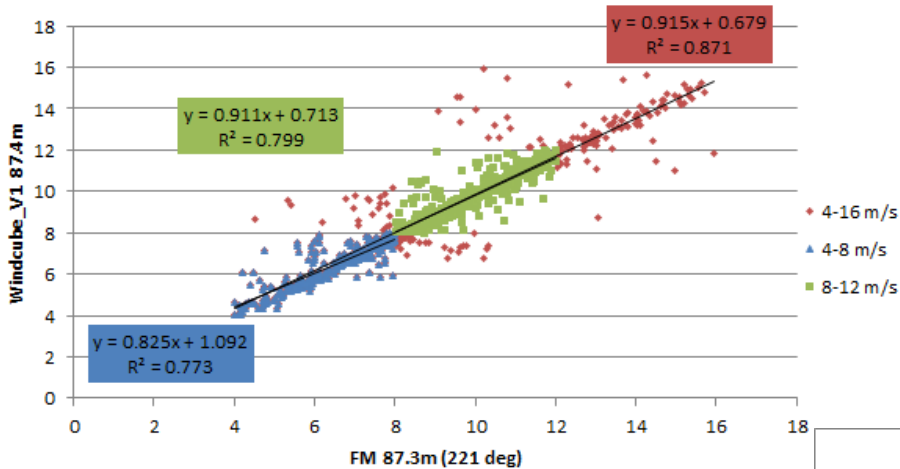
WINDCUBE V1 Filters	
Vertical wind speed censor ( $\text{m.s}^{-1}$ )	1.5
Availability (%)	90

## MAST SEPARATION DISTANCES

	M626	M628	M630
M628	7653		
M630	7131	5025	
M814 (LiDAR)	51	7699	7181

## EFFECT OF WIPER REPLACEMENT: CORRELATIONS

### Linear Regression



Data from

16/09/2011 until 17/11/2011

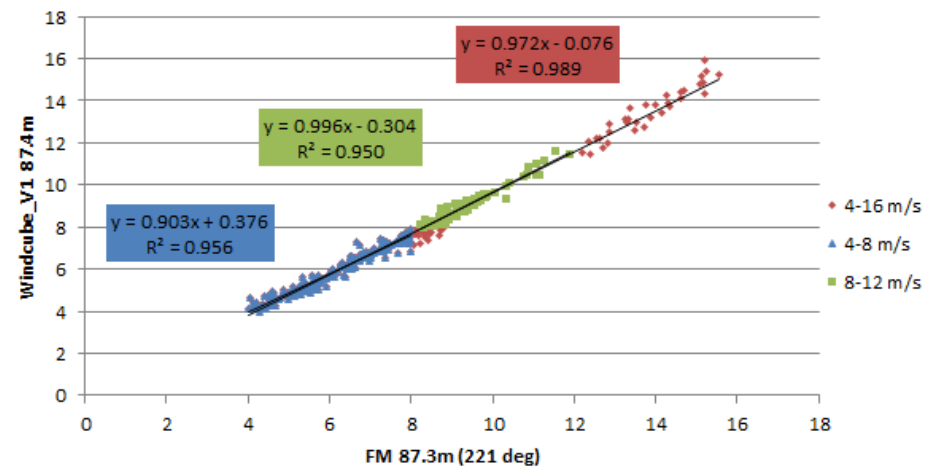
with the original wiper unit

Data from

21/11/2011 until 06/01/2012

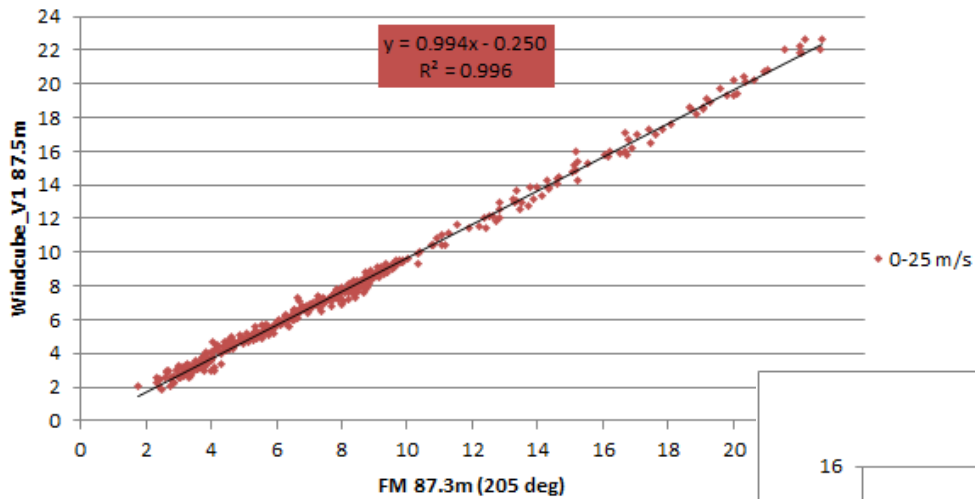
with the replacement unit

### Linear Regression



## EFFECT OF RECONFIGURATION: MEAN WIND SPEED CORRELATIONS

### Linear Regression



Data from

21/11/2011 until 06/01/2012

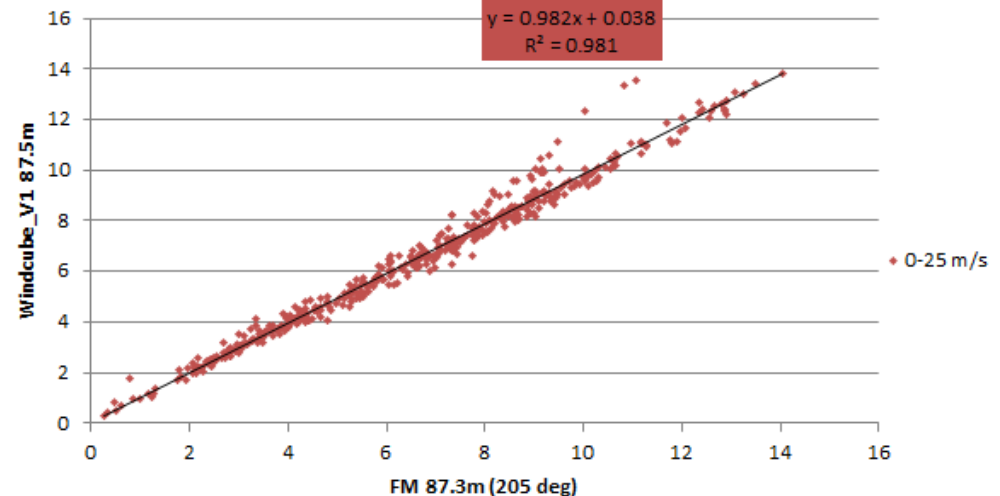
with the original configuration

Data from

01/02/2012 until 16/02/2012

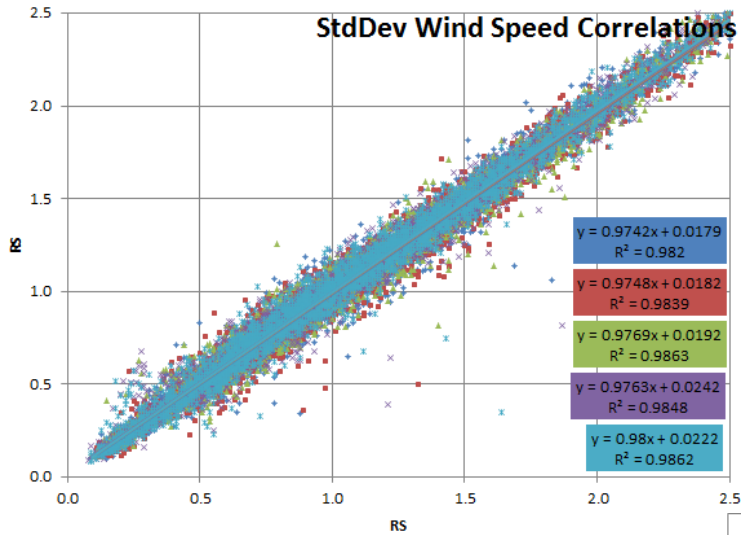
With new configuration

### Linear Regression

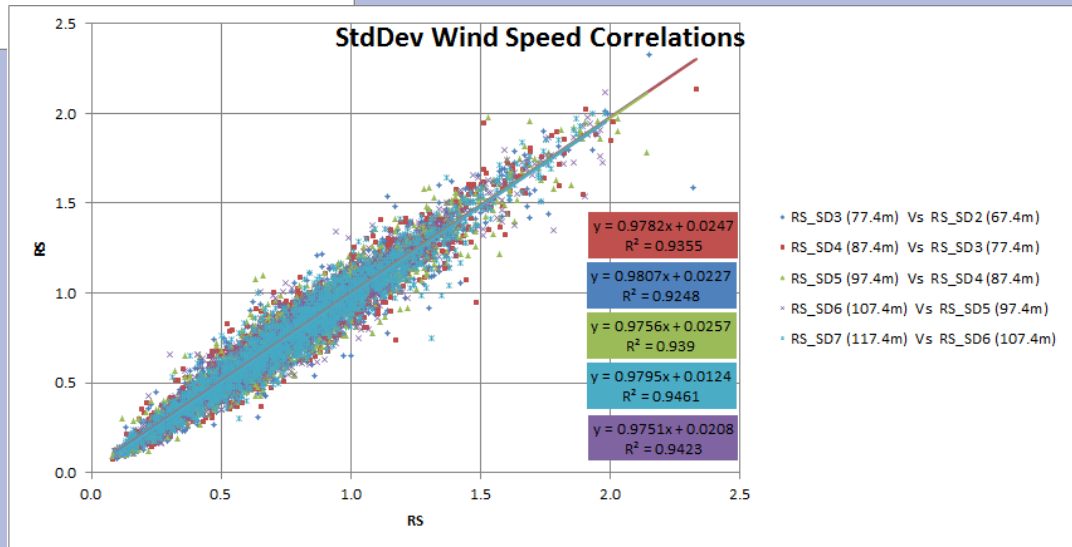


# EFFECT OF RECONFIGURATION: STANDARD DEVIATION CORRELATIONS

Data from  
21/11/2011 until 06/01/2012  
with the original configuration



Data from  
01/02/2012 until 16/02/2012  
With new configuration





## ACCEPTANCE TEST CRITERIA

Parameter	Criteria	Ranges (height & speed)
Absolute error	<0.5m/s for WS range 2-16m/s Within 5% above 16 m/s Not more than 10% of data to exceed those values	All valid data
Data Availability	Assessed case by case – Environmental conditions dependent	All valid data
Linear Regression - Slope	Between 0.98 and 1.01 <0.015 variation in slope between WG-ranges (b) and (c)	Heights all 60 to 116m WS-ranges: (a) 4-16m/s, (b) 4-8m/s & (c) 8-12 m/s
Linear Regression – R <sup>2</sup>	>0.98	Heights: all 60 to 116m WS-ranges: 4-16m/s, 4-8m/s & 8-12 m/s

### Acceptance criteria



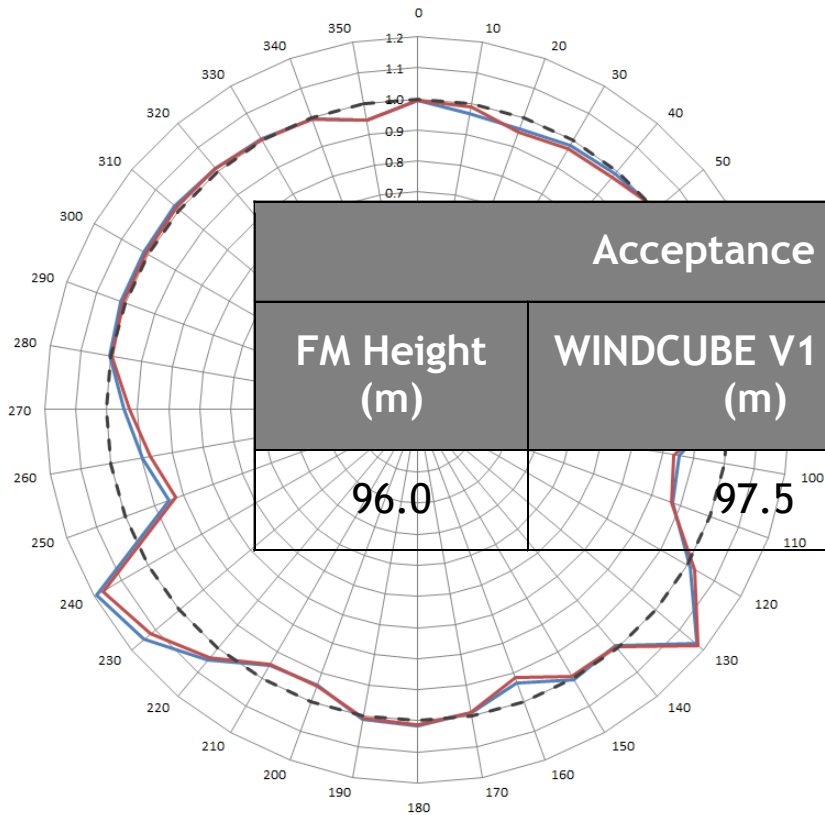
The following criteria for acceptance tests have been adopted and easily satisfied in the past by lidar operators under contract

- 1) 2 week data period
- 2) R<sup>2</sup> value on wind speed correlations >0.96
- 3) Slope of wind speed correlation: 0.97<x<1.03
- 4) RMS on wind direction difference <5°
- 5) Units located adjacent to a tall mast (>40m):
  - Calibrated instruments
  - Mounting in accordance with IEC Pt .11
  - Sited to minimise differences in wind between locations

In addition data availability >95% is typical. The IEA expert committee, on which SgurrEnergy is represented, will publish guidelines by the end of the summer.

# DEVICE VERIFICATION

Wind Speed Ratios by Direction



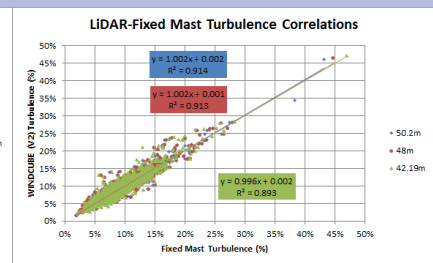
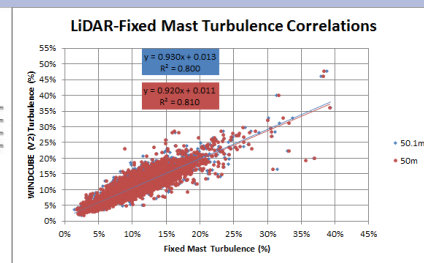
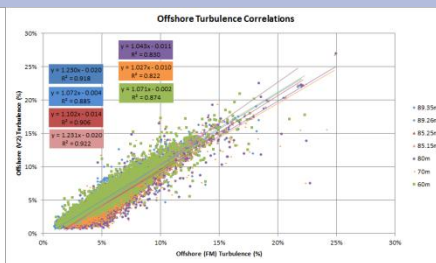
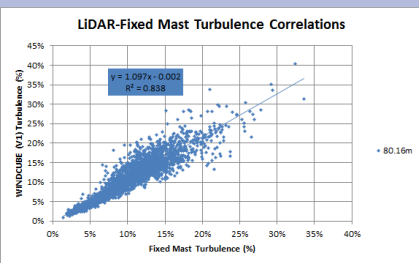
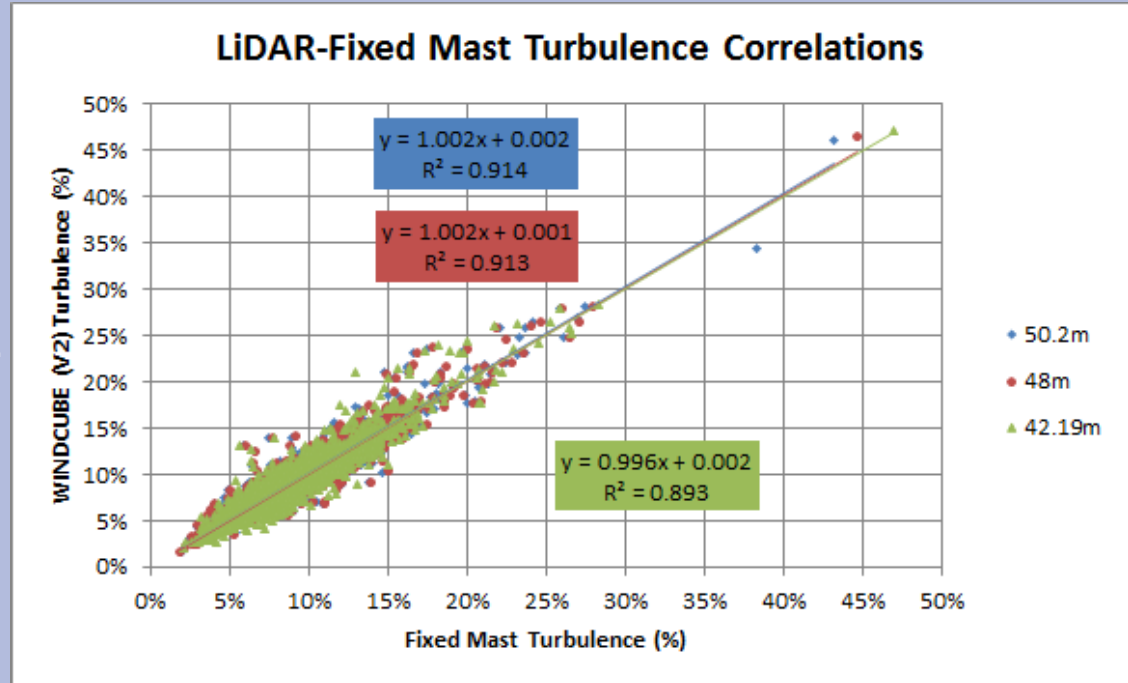
## Acceptance Test Results

FM Height (m)	WINDCUBE V1 Height (m)	Slope	R <sup>2</sup>	Pass/Fail
96.0	97.5	0.975	0.995	PASS

Mast	Wake Free Sector Start (°)	Wake Free Sector End (°)
M626		
M814 (LiDAR)	297	75

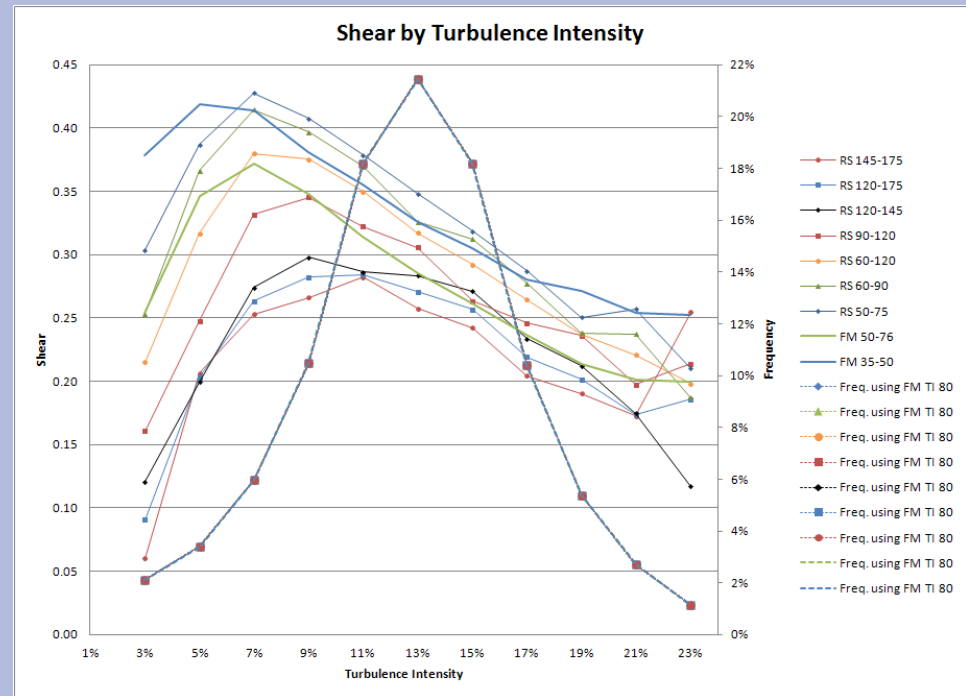
# TURBULENCE: VARIOUS SITES

- Simple
- Offshore
- Moderately complex site1
- Moderately complex site2



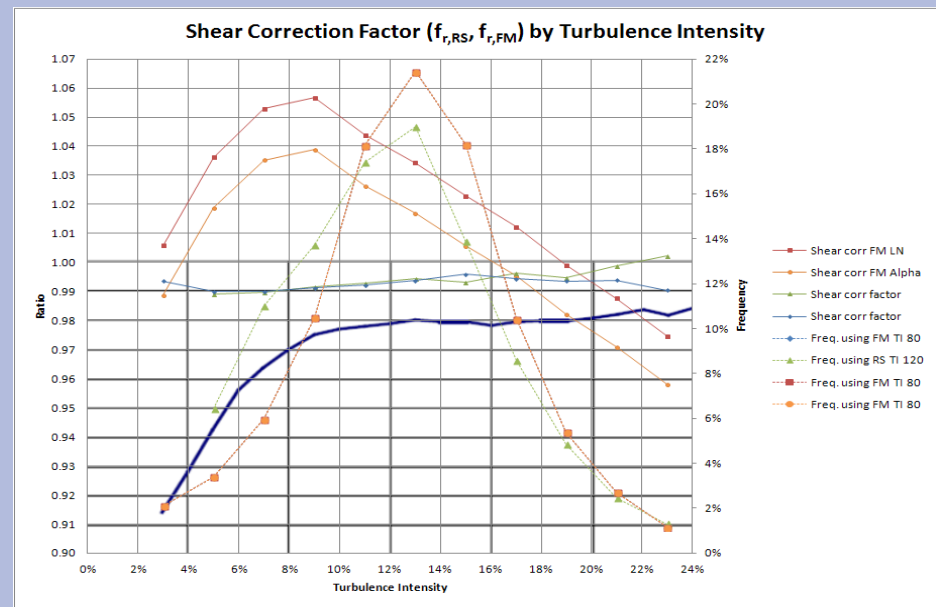
## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: OTHER SWEDISH SITE

- Shear is consistent across full rotor
- At low TI
  - Turning point exists
  - But shear remains consistent across full range
  - No divergence at  $\approx 9\%$



## LOW TURBULENCE STABLE ATMOSPHERIC CONDITIONS: OTHER SWEDISH SITE

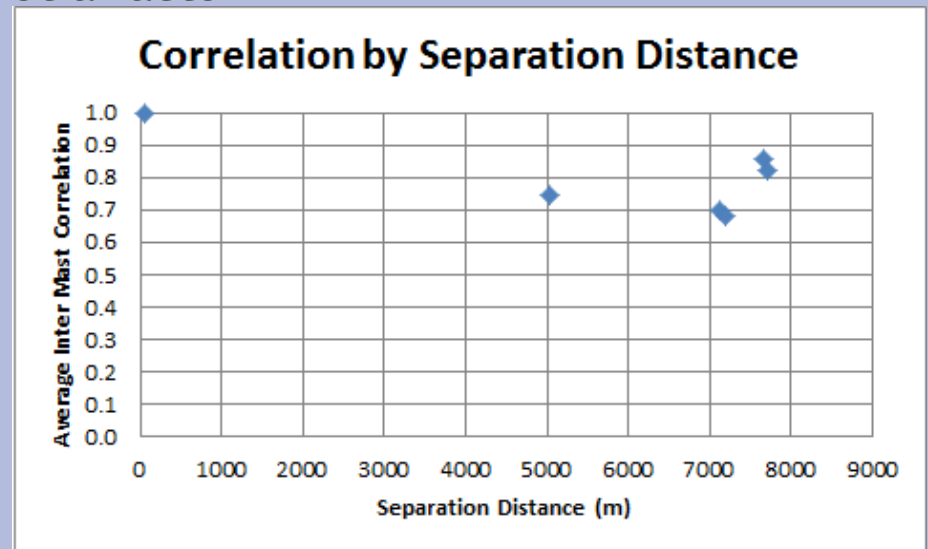
- RS shear correction factors do not vary strongly with turbulence intensity
- At low TI
  - Small variation
  - No dramatic plunge
- FM hub height wind speed tends to underestimate rotor wind speed
- At low TI underestimation decreases
  - Due to the fixed shear exponent not capturing the turbulence dependency of shear
- However, the result does not suggest that an energy loss factor is appropriate



## INTER MAST WIND SPEED CORRELATIONS

The relationship between correlation and separation distance:

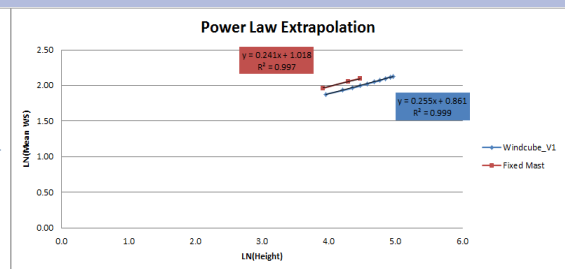
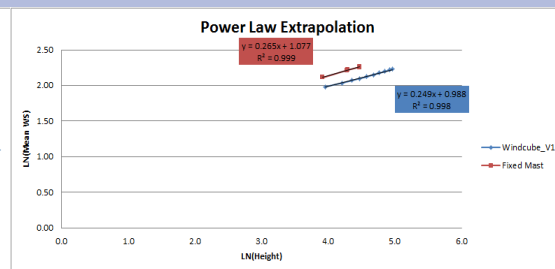
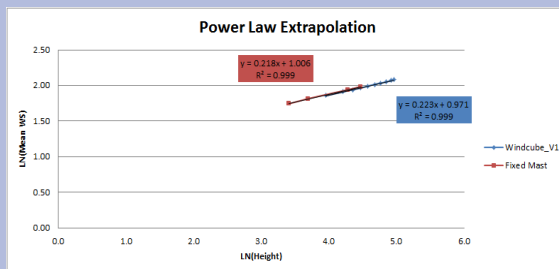
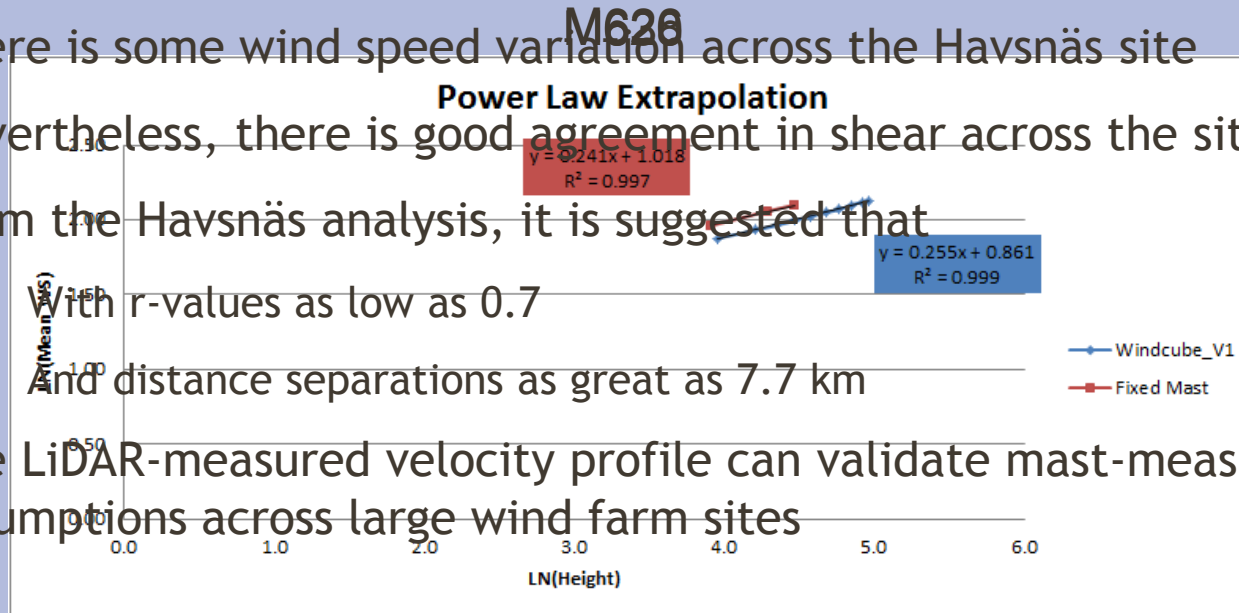
- The nature of the relationship is likely to be site dependent
- At Havsnäs
  - For every 1 km increase in separation distance,
  - The r-value decreases by approximately 0.03
- Generally, measurement height is not a factor



# SHEAR AT HAVSNÄS

## LiDAR-Mast Multi-Point Shear Comparisons

- There is some wind speed variation across the Havsnäs site
- Nevertheless, there is good agreement in shear across the site
- From the Havsnäs analysis, it is suggested that
  - With r-values as low as 0.7
  - And distance separations as great as 7.7 km
- ❖ The LiDAR-measured velocity profile can validate mast-measured shear assumptions across large wind farm sites



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