

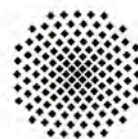



Thermal Analysis of a Heated Rotor Blade for Wind Turbines

Richard Hann and Sven Olaf Neumann
*Institute of Aerospace Thermodynamics, University of
Stuttgart*

Alexander Miller
KENERSYS GmbH

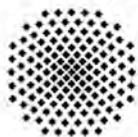
Jeroen Dillingh
VTT Technical Research Centre of Finland

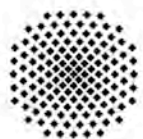
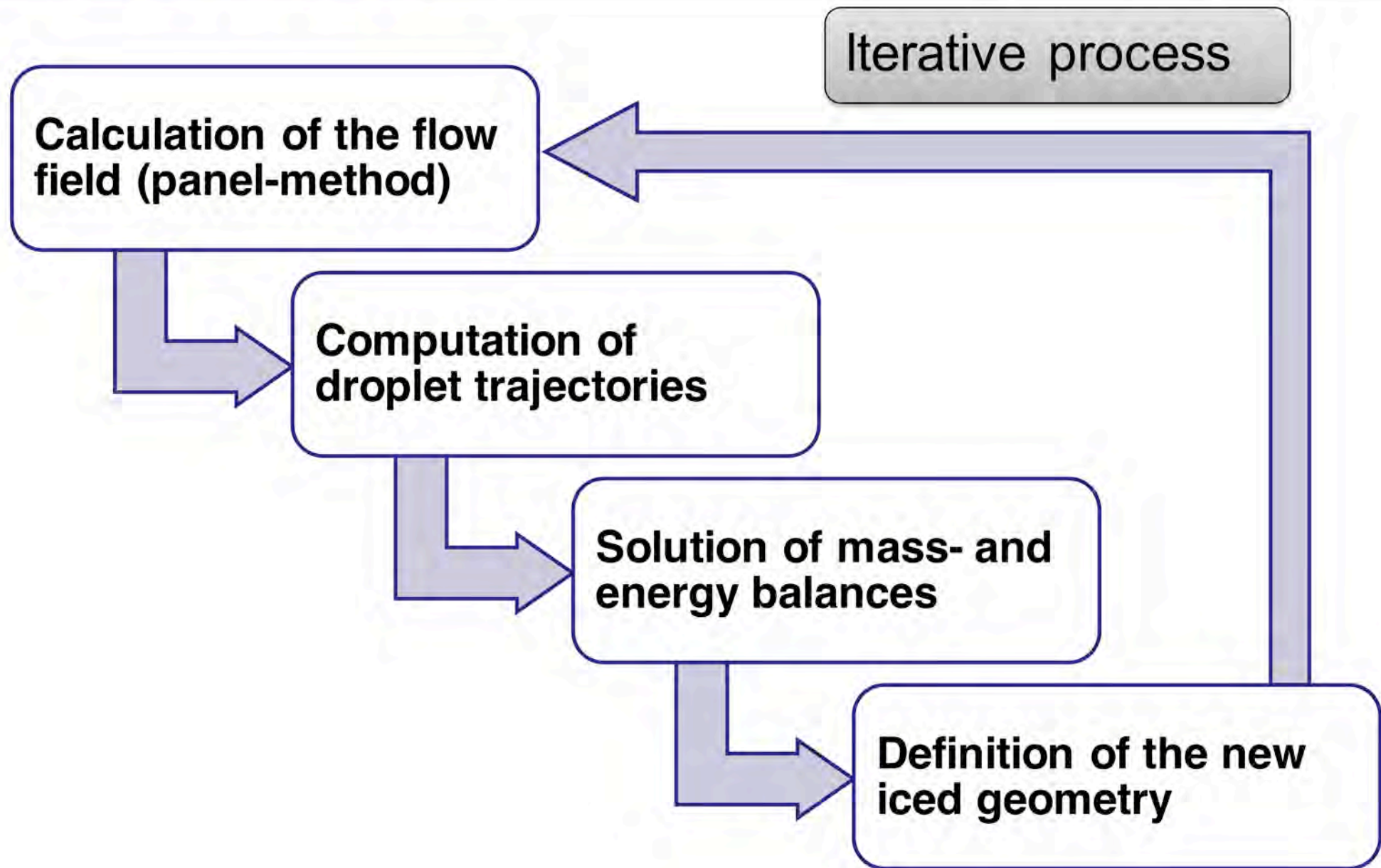


- 
- Results of the final year thesis of Richard Hann at the University of Stuttgart
 - Cooperation with KENERSYS GmbH (Germany)
 - Cooperation with VTT (Finland)

Content

- CFD-simulation of an iced airfoil
- Analysis of the heat transfer on an iced airfoil
- Analysis of the required heat for an electro-thermal anti-icing system



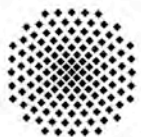


LEWICE 3.2.2 (NASA)

- Developed for aircraft icing
- 2D ice accretion and anti-icing
- Extensive experimental validation

TURBICE 6.0 (VTT)

- Developed specifically for the wind energy
- 2D ice accretion and anti-icing
- Advanced roughness and ice density models



Reference case: In-Cloud Icing

Wind speed: 13m/s

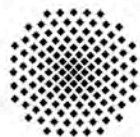
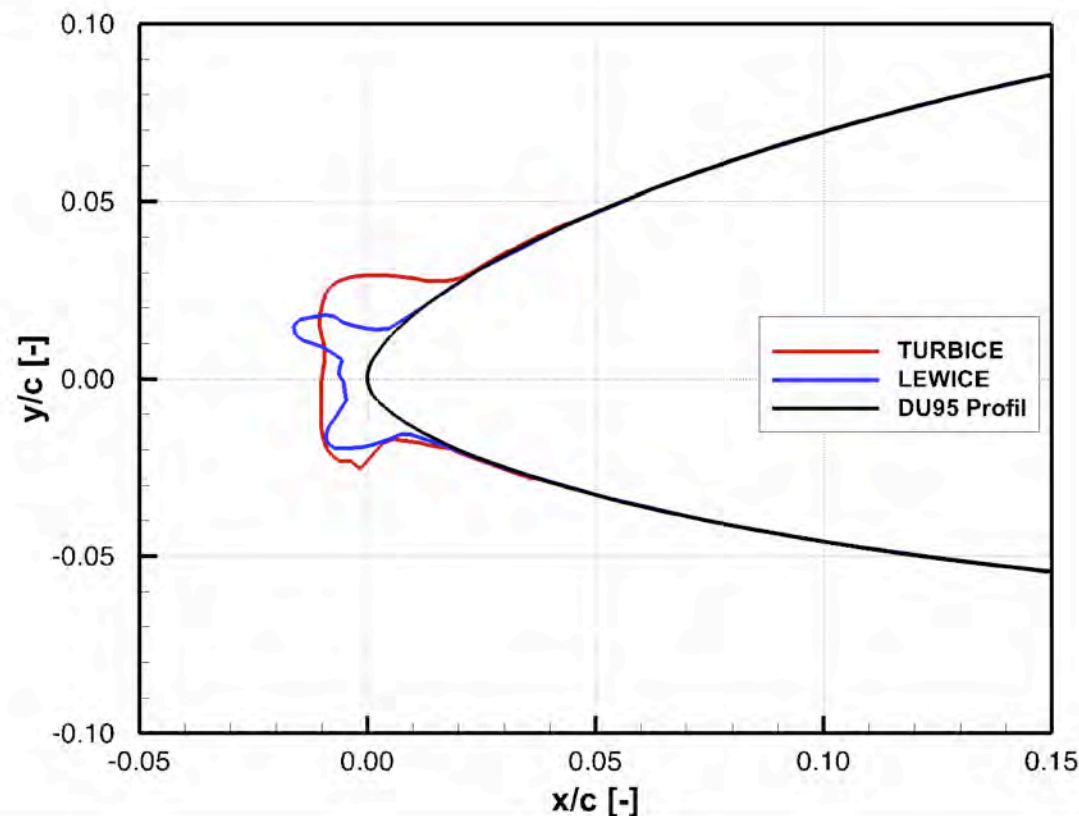
Icing time: 45min

Droplet size (MVD): $20\mu\text{m}$

Rotational speed: 14rpm,

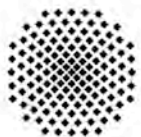
Temperature: -5°C

Water content (LWC): 0.53g/m^3



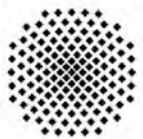
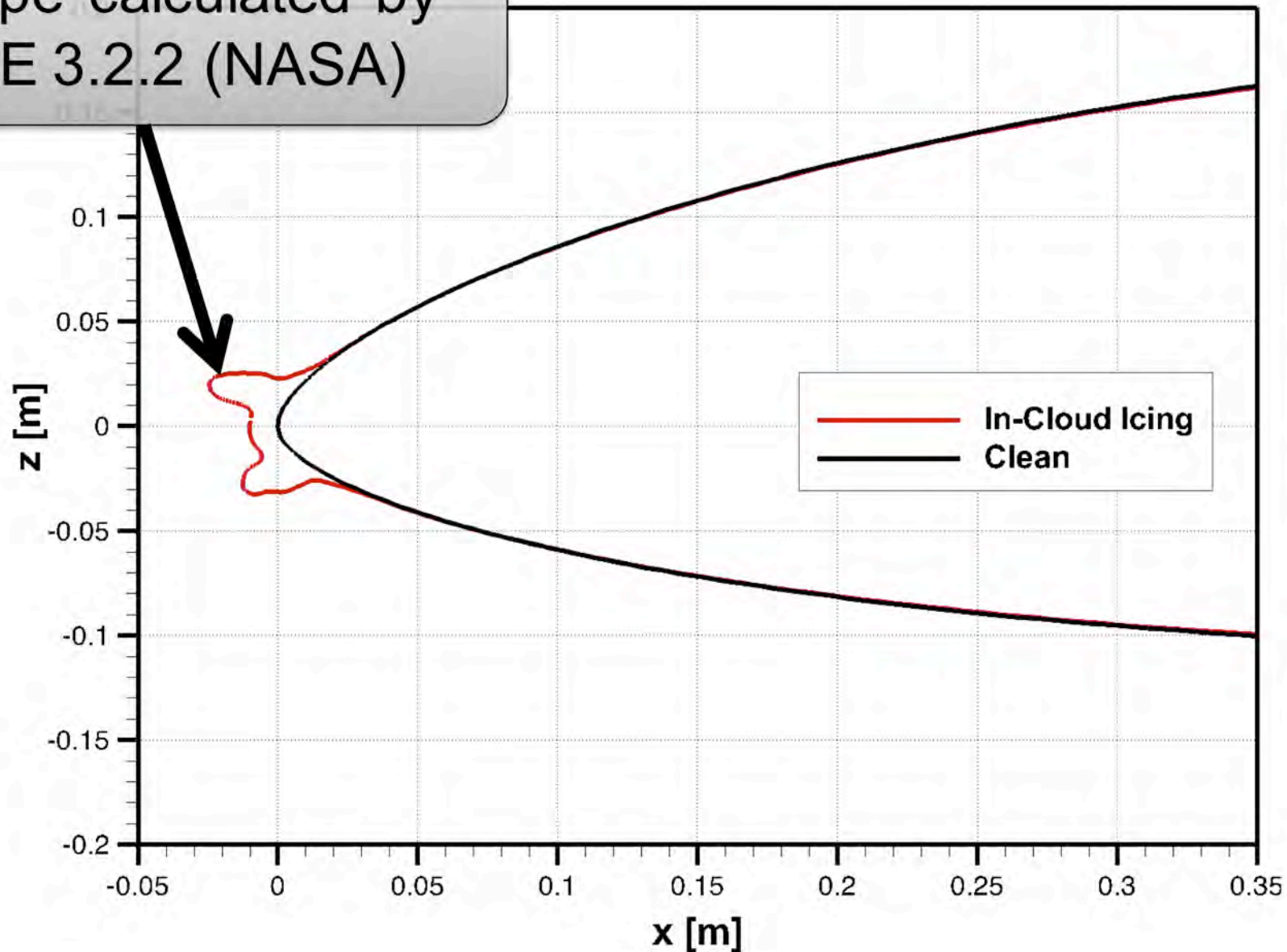


„What is the effect of ice accretion on the aerodynamics of an airfoil?“



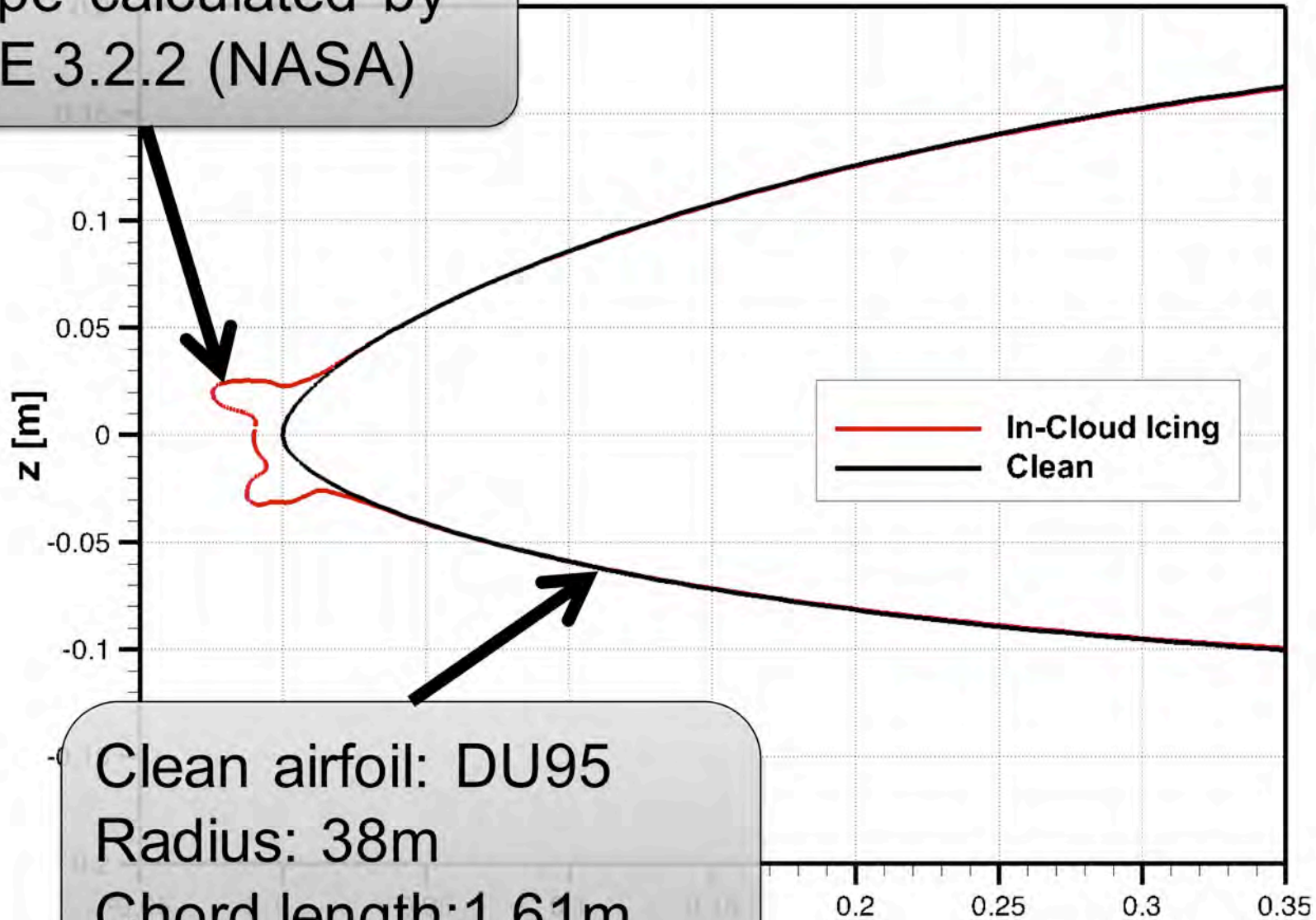
1st step: Define an icing case

Ice-shape calculated by LEWICE 3.2.2 (NASA)

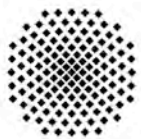


1st step: Define an icing case

Ice-shape calculated by LEWICE 3.2.2 (NASA)

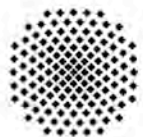
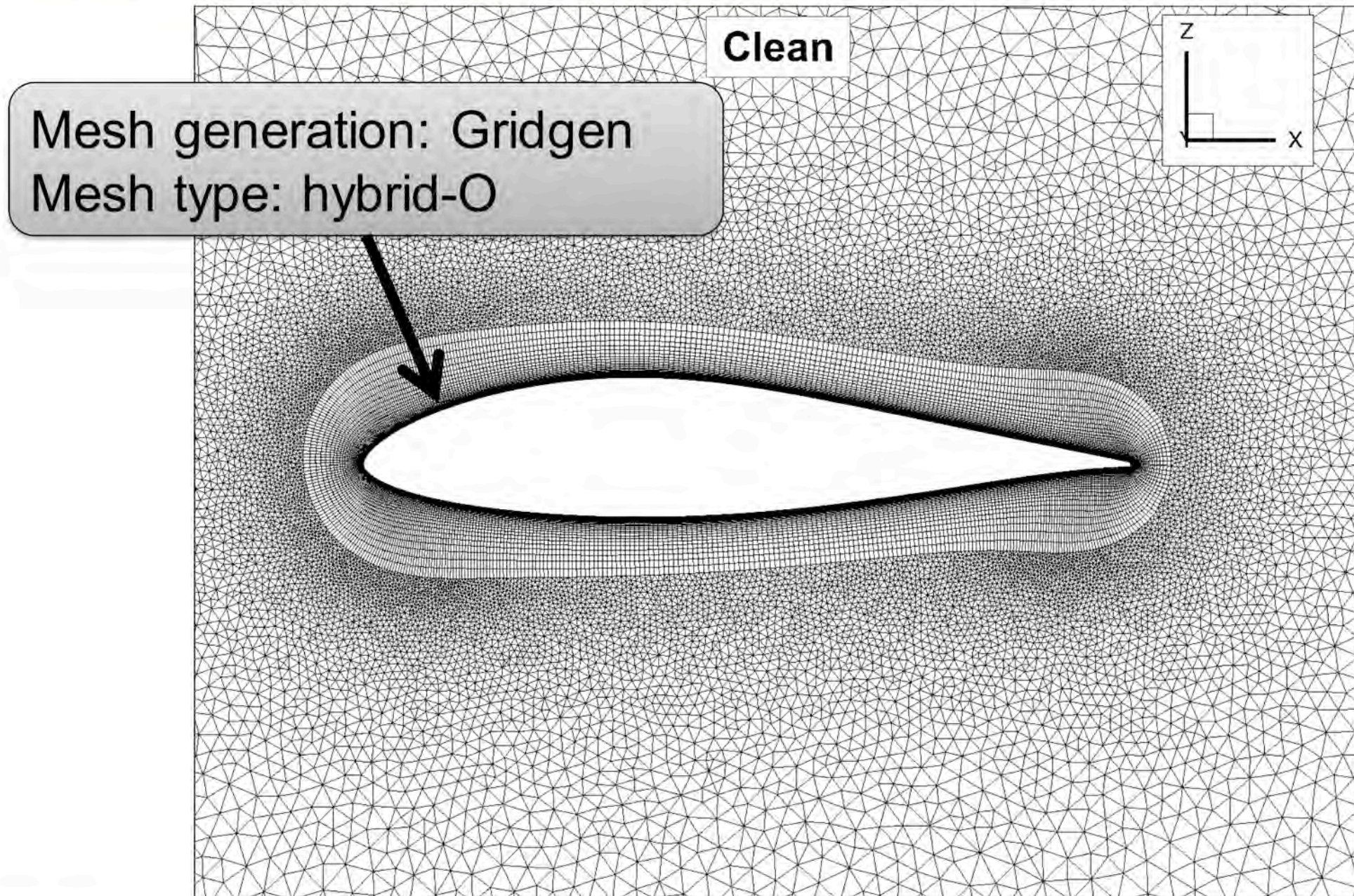


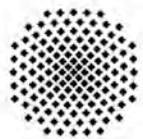
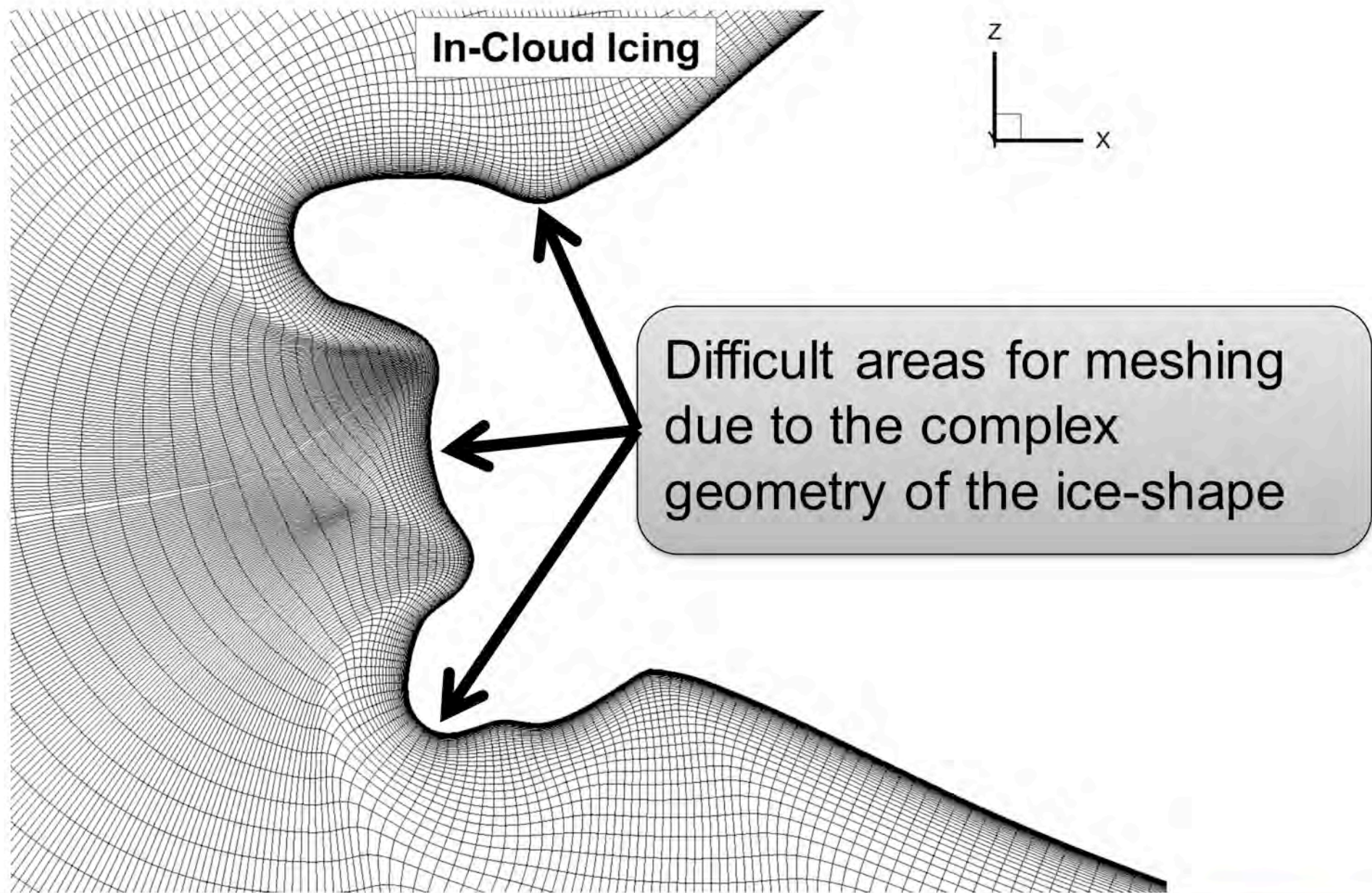
Clean airfoil: DU95
Radius: 38m
Chord length: 1.61m
Thickness ratio: 18.0%



2nd step: Spatial discretization

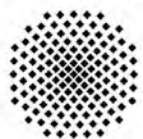
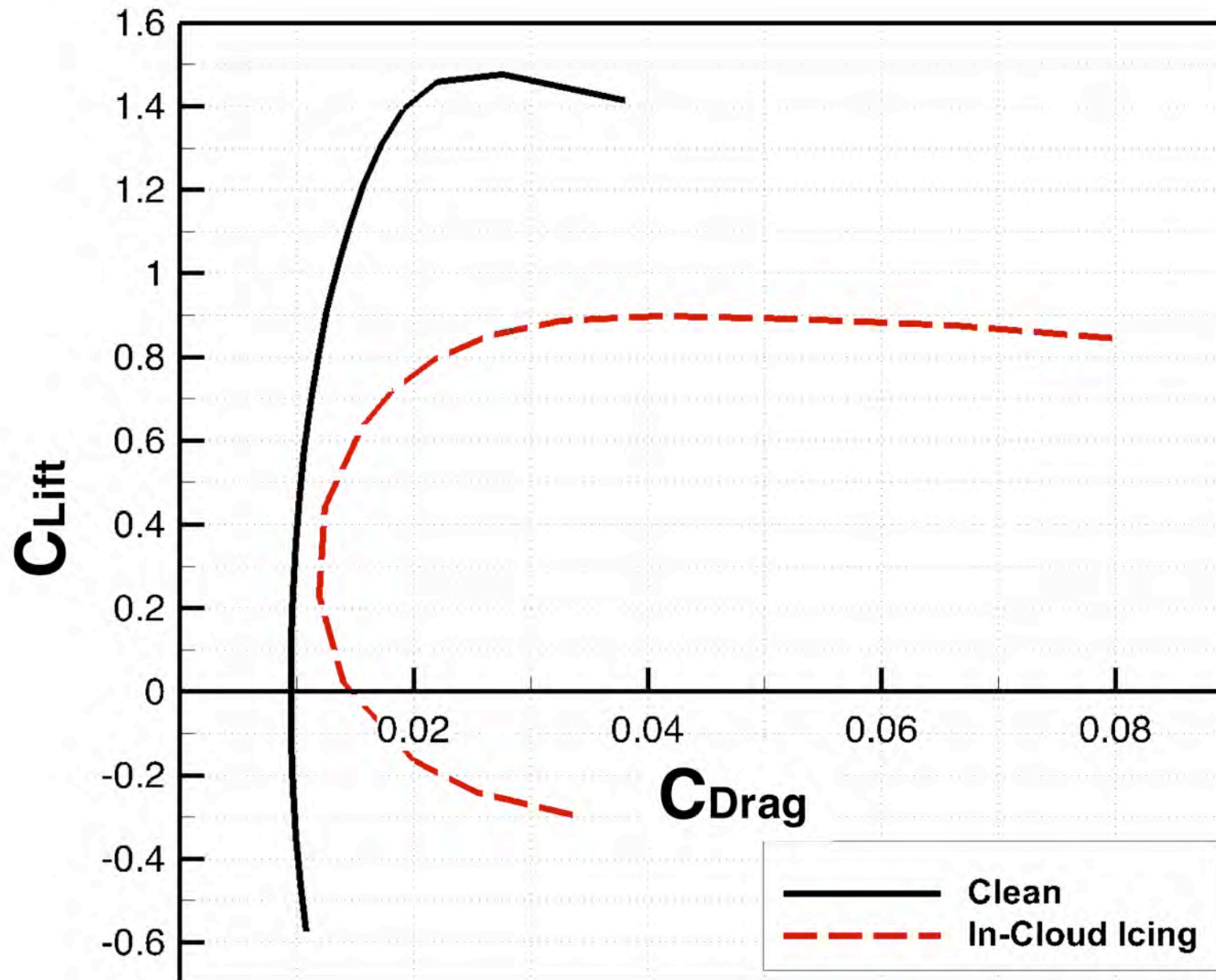
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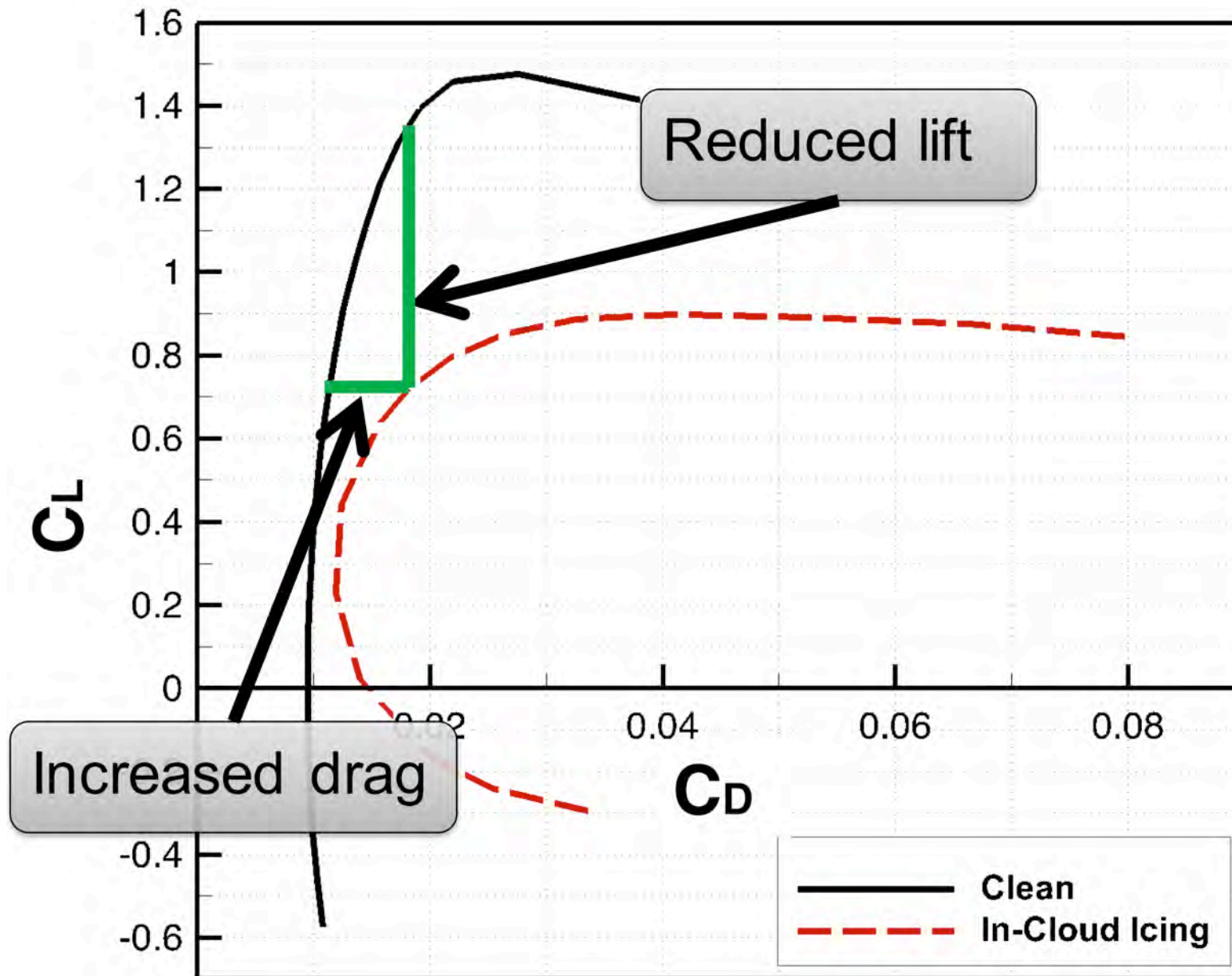


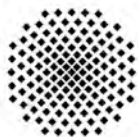
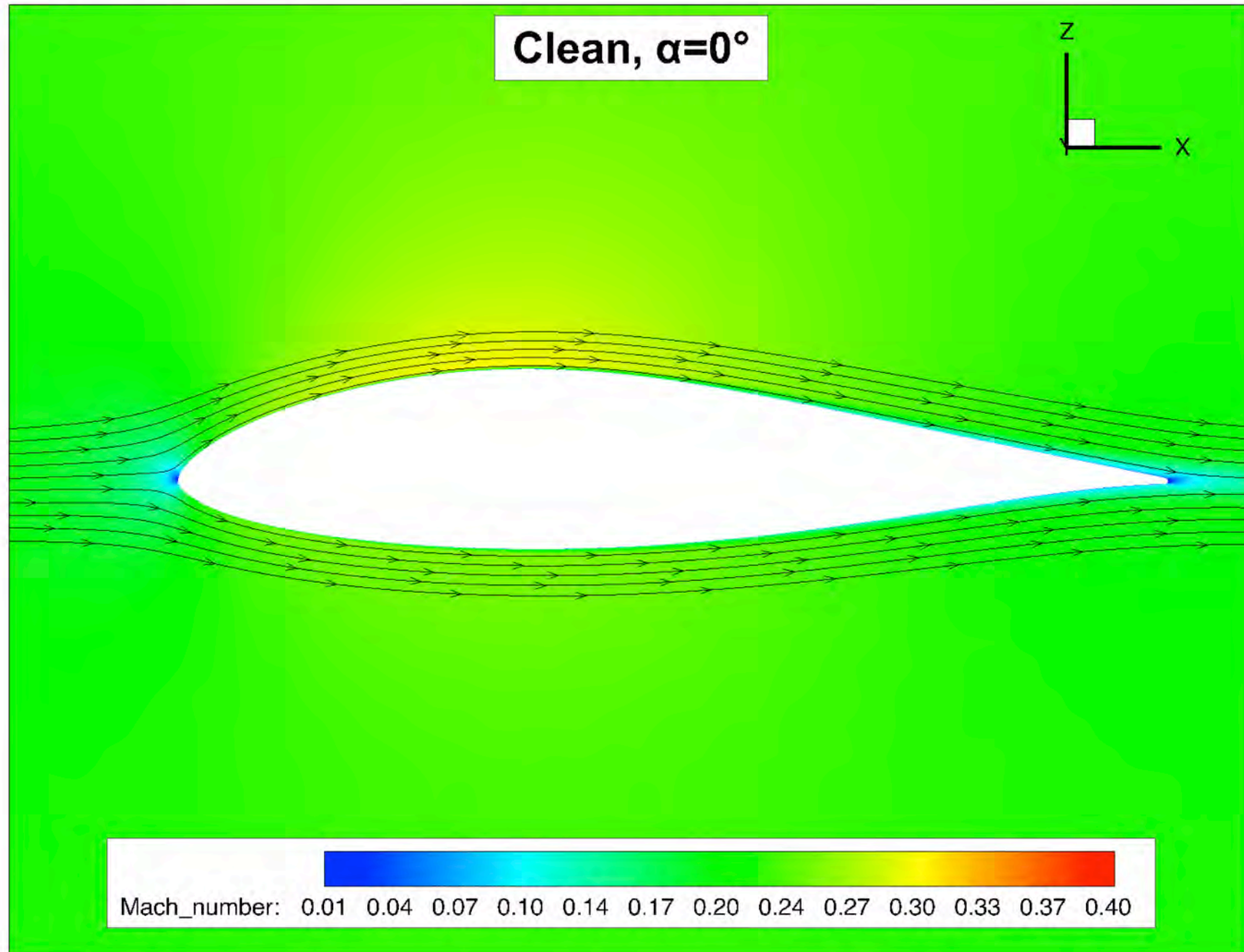


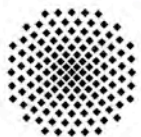
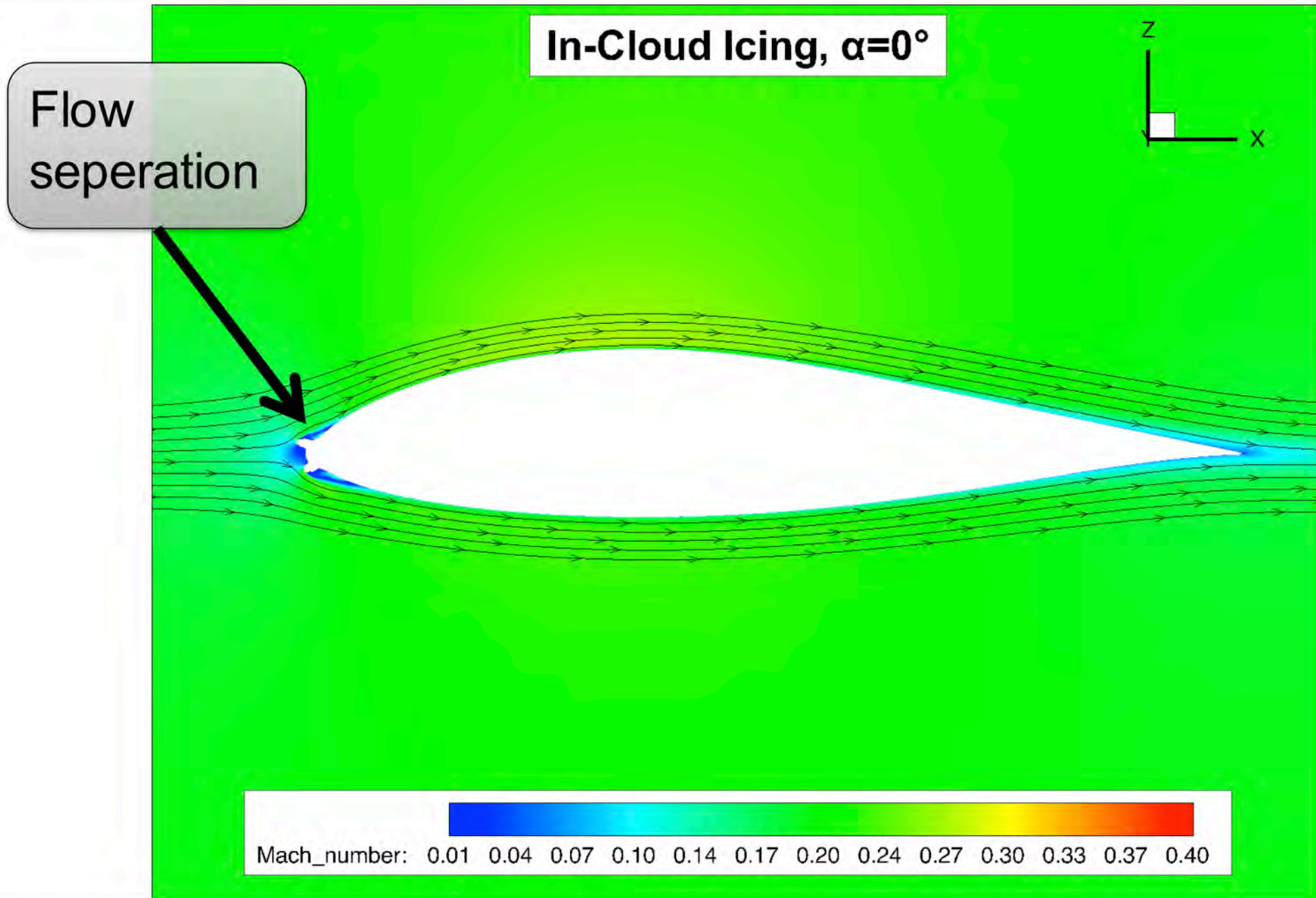
- ☞ CFD-solver: TAU (developed by the German Aerospace Center, DLR)
- ☞ Flow parameters:
 - Reynolds number = $3 \cdot 10^6$
 - Mach number = 0.2
- ☞ Numerical parameters:
 - Turbulence model: Menter SST
 - Time discretization: Backward Euler (CFL=100)
 - Spatial discretization: central Jameson (scalar dissipation)
 - Multigrid: 3v
 - Transition: 4% of chord for clean / turbulent for iced





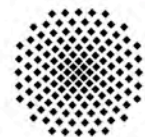
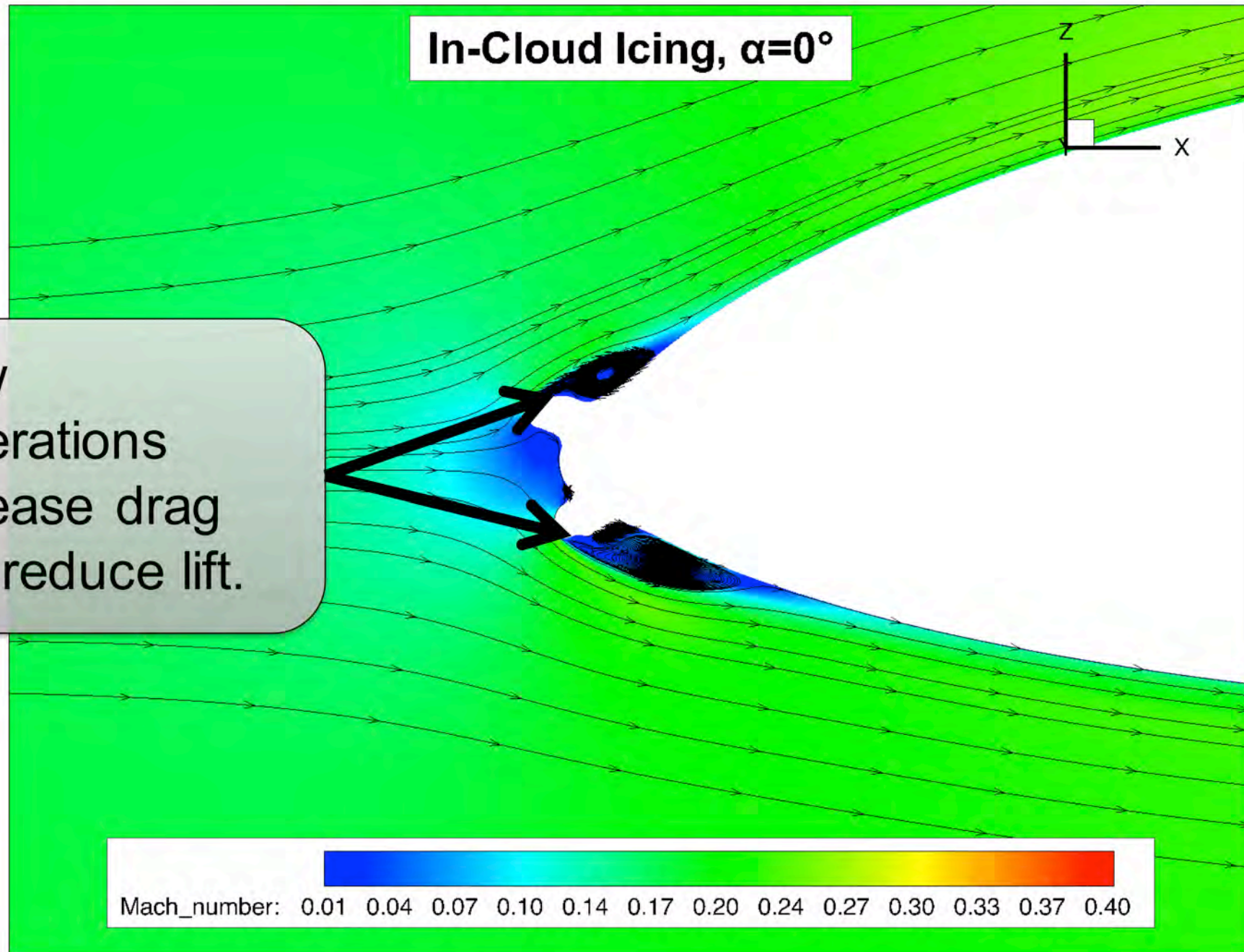






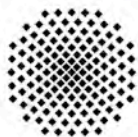
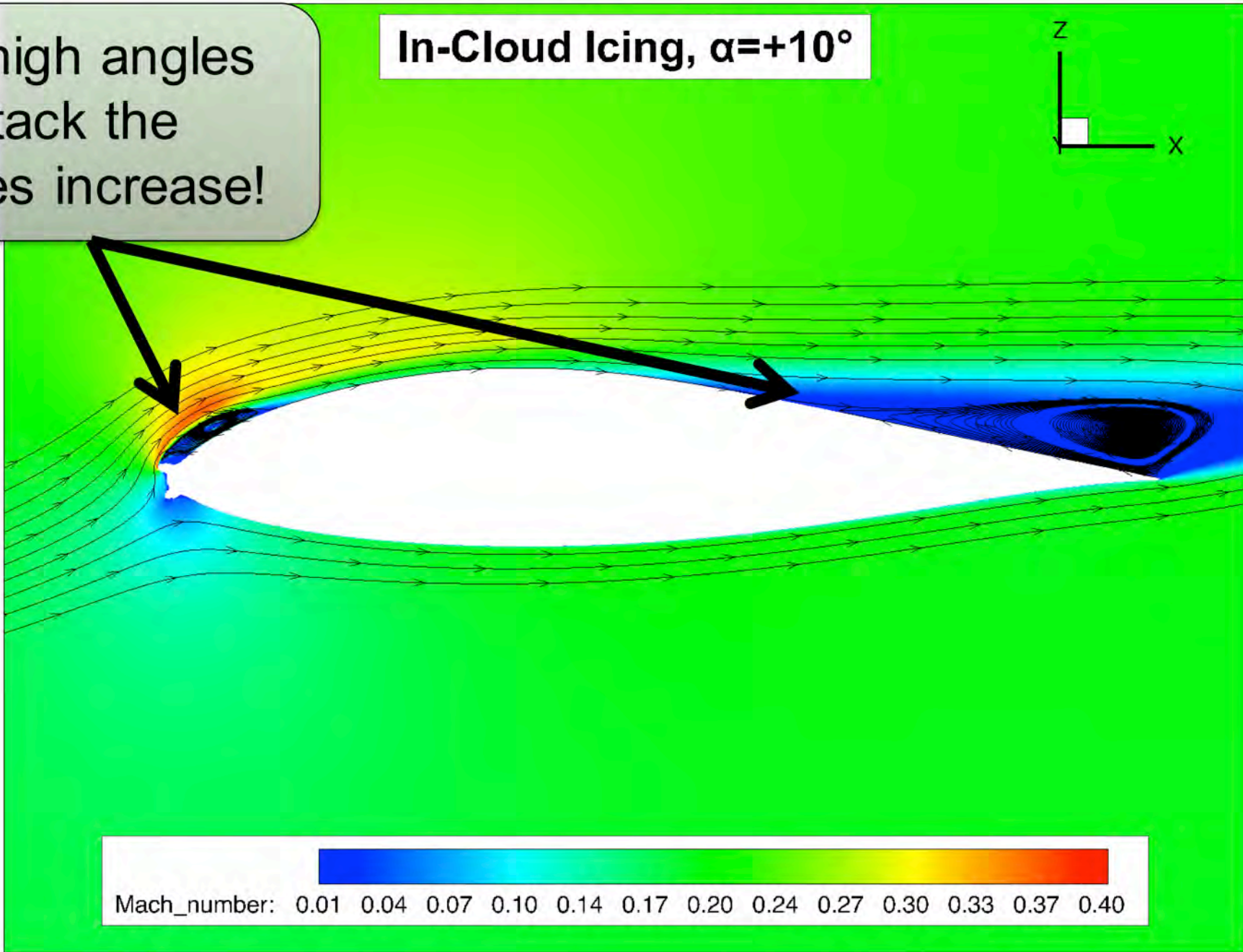
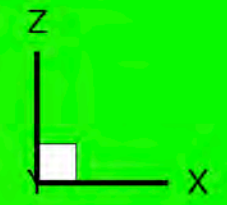
In-Cloud Icing, $\alpha=0^\circ$

Flow separations increase drag and reduce lift.



For high angles of attack the losses increase!

In-Cloud Icing, $\alpha=+10^\circ$



Lift
reduced

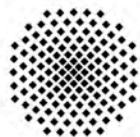
Power
output
reduced

**LOSS
OF
MONEY**

Drag
increased

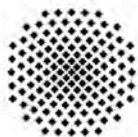
Mechanical
loads
increased

Shutdown
due to
structural
safety





„Why is the heat transfer on an iced-airfoil important?“



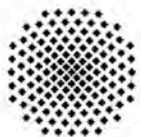


- Heat transfer

- Ice accretion

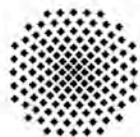
- Required power for anti-icing

- Boundaries for designing a thermal anti-icing system





„What does the process of heat transfer on an iced airfoil look like?“





Nusselt number = heat transfer

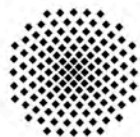
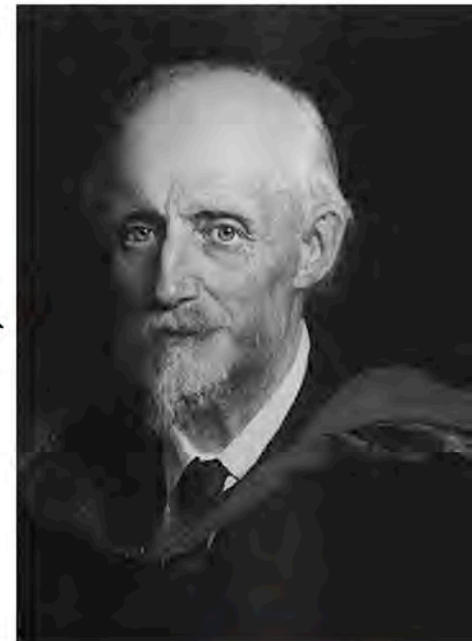
Nu: Nusselt number [-]
htc: total heat transfer coefficient [W/m² K]
x: distance from stagnation point [m]
 λ : thermal conductivity [W/m K]

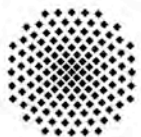
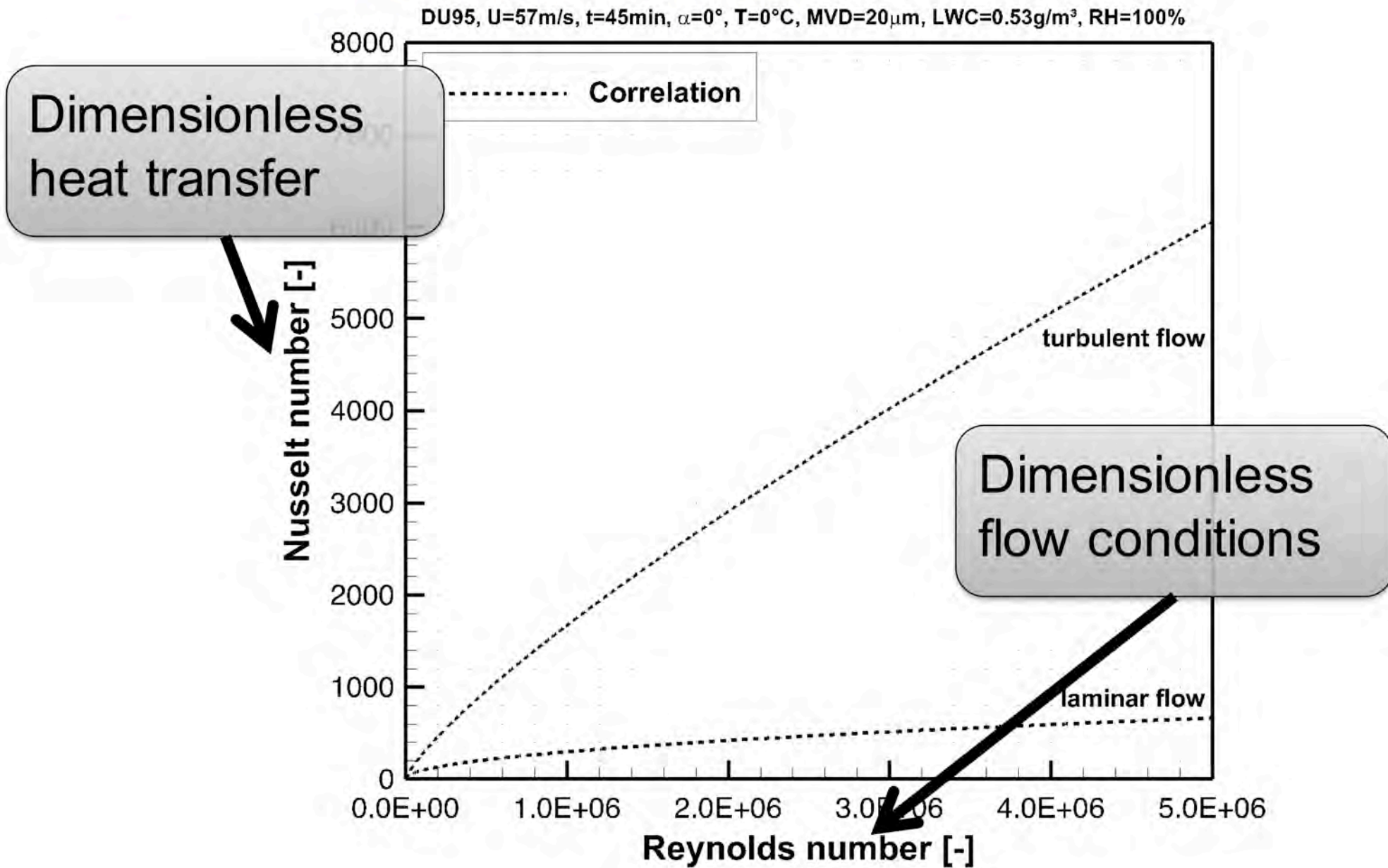
W. Nusselt
(1882-1957)

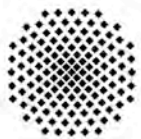
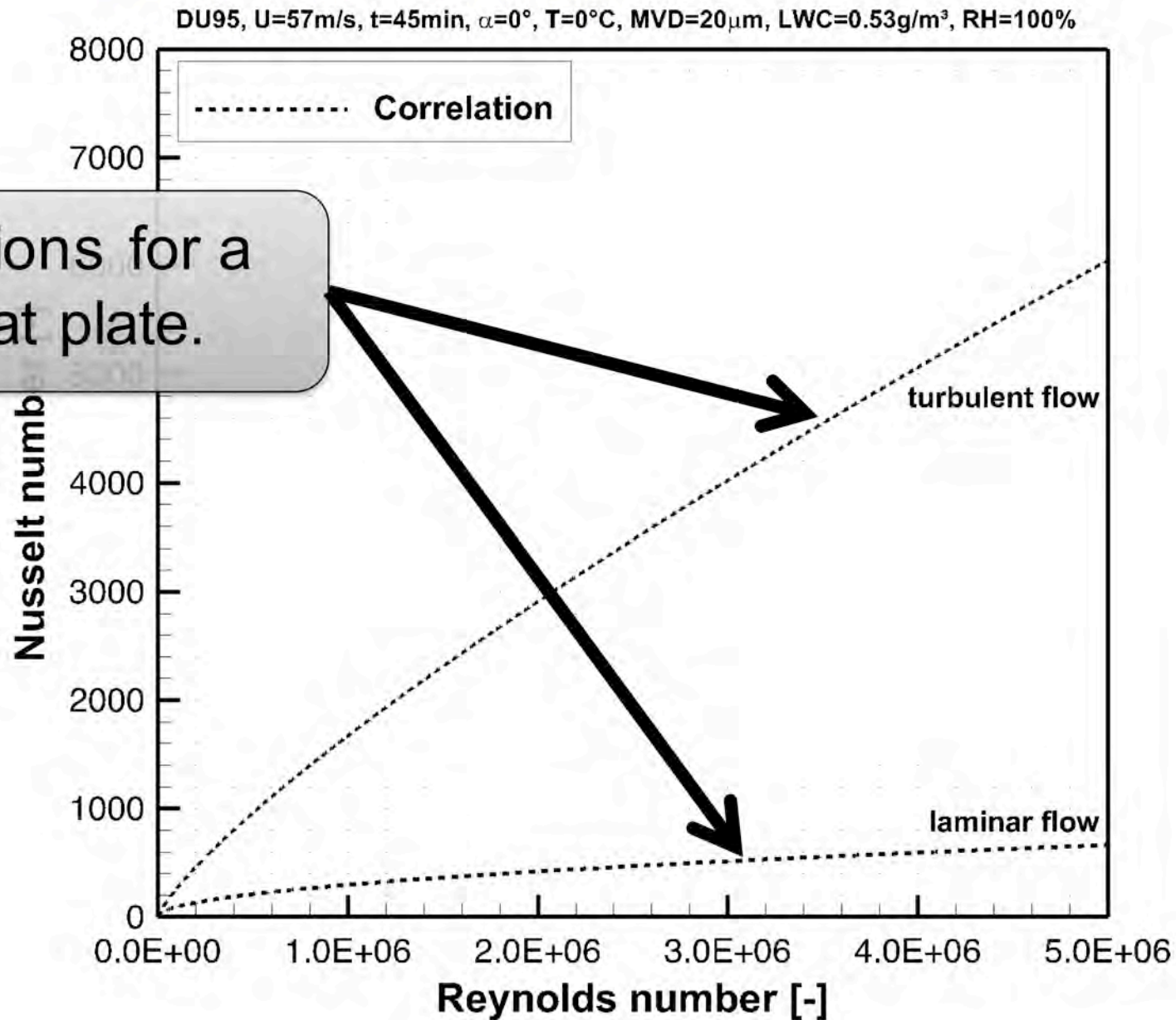
O. Reynolds
(1842-1912)

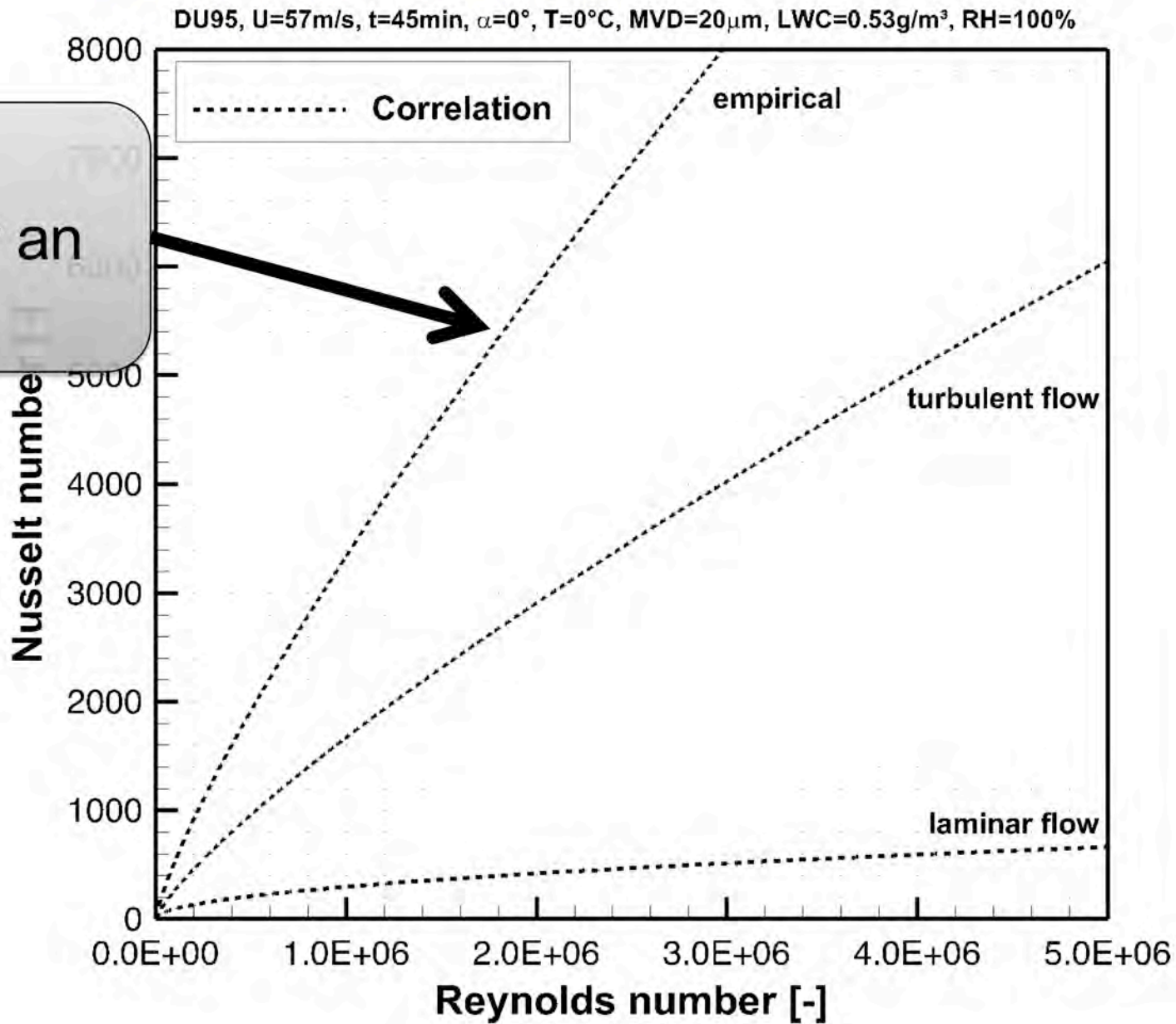
Reynolds number = local flow condition

Re: Reynolds number [-]
v: air velocity [m/s]
x: distance from stagnation point [m]
 ν : kinematic viscosity [m²/s]

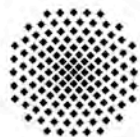




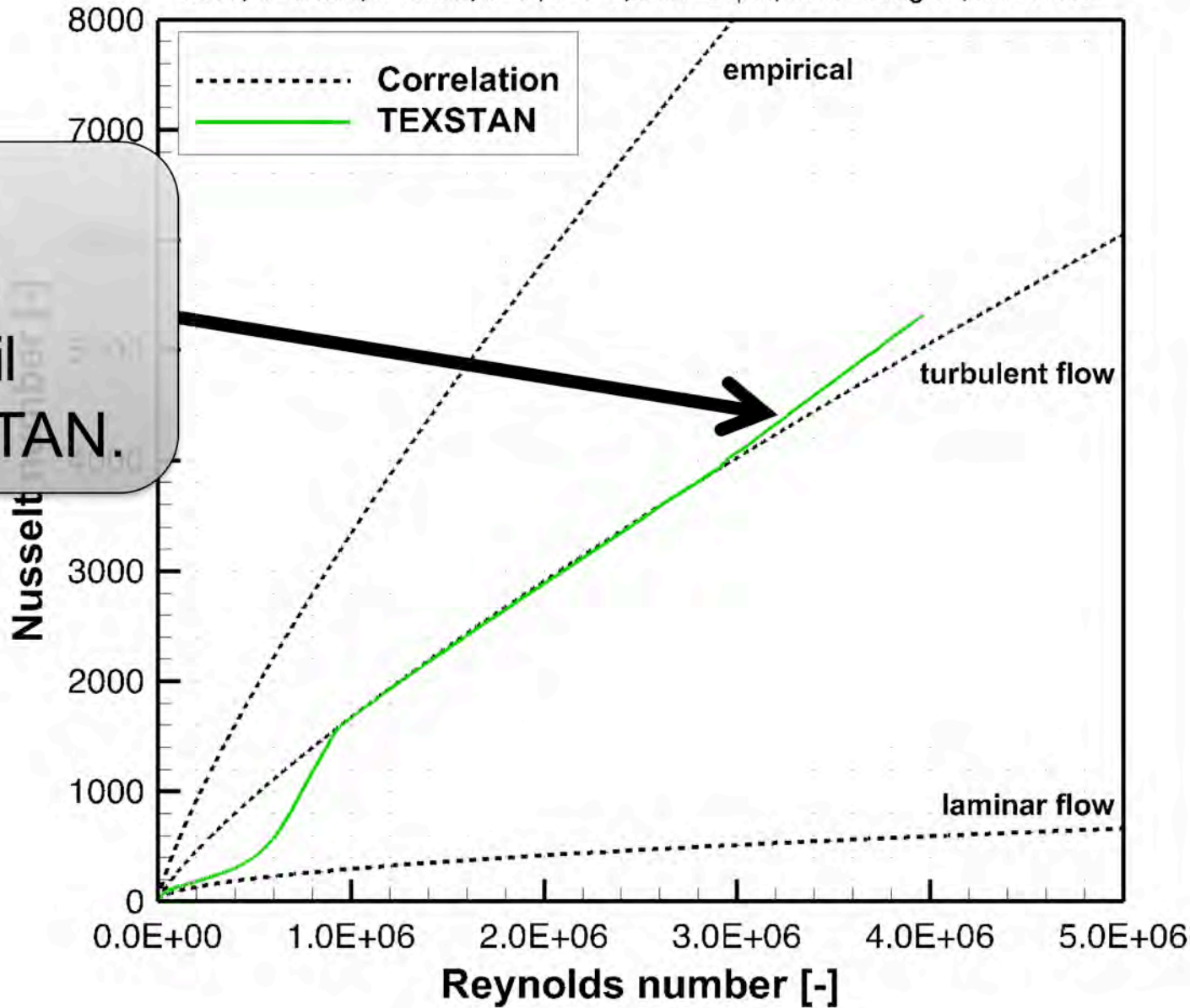




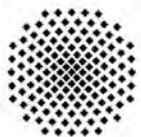
Empirical solution for an iced-airfoil.



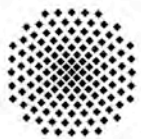
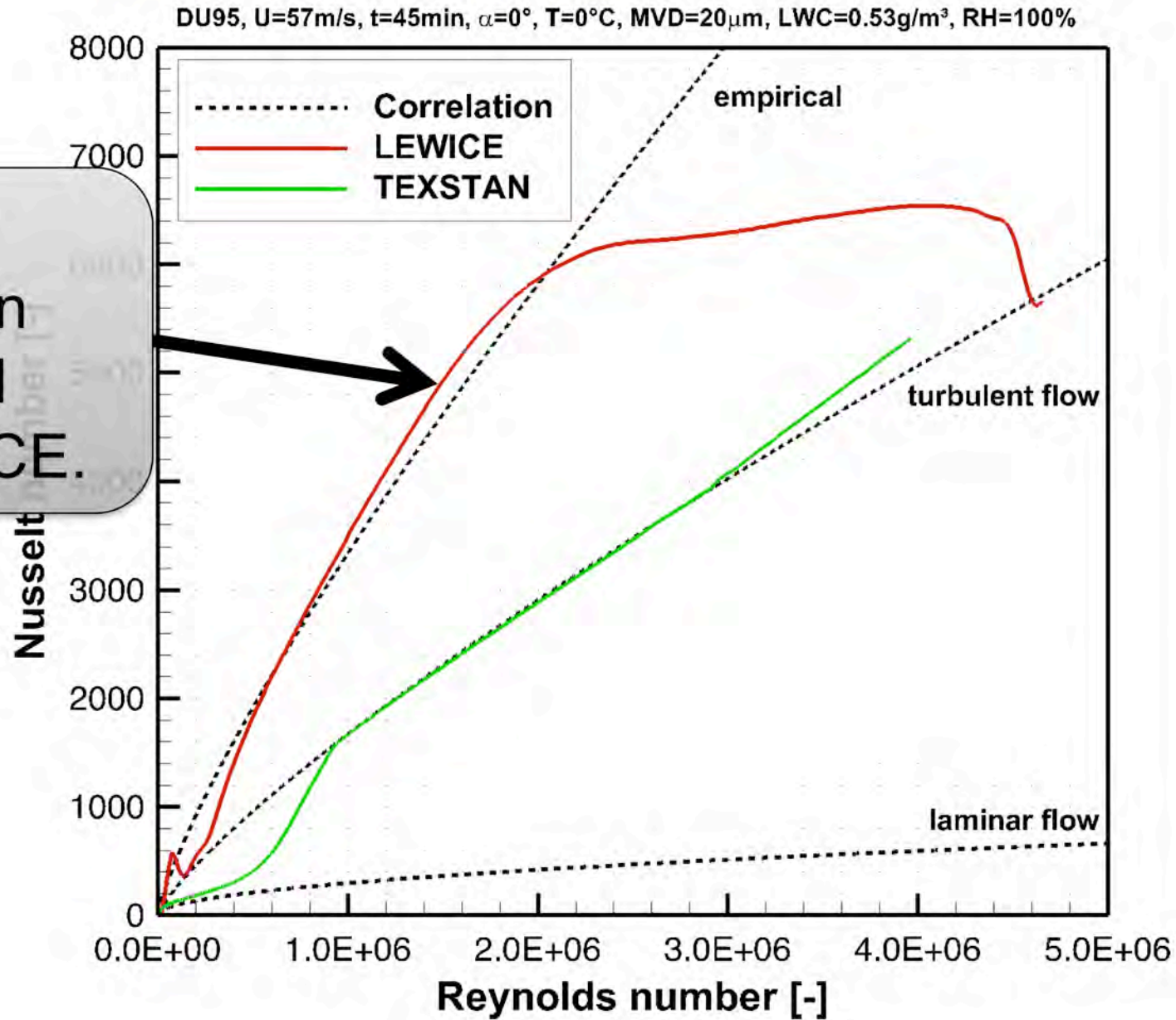
DU95, $U=57\text{m/s}$, $t=45\text{min}$, $\alpha=0^\circ$, $T=0^\circ\text{C}$, $\text{MVD}=20\mu\text{m}$, $\text{LWC}=0.53\text{g/m}^3$, $\text{RH}=100\%$



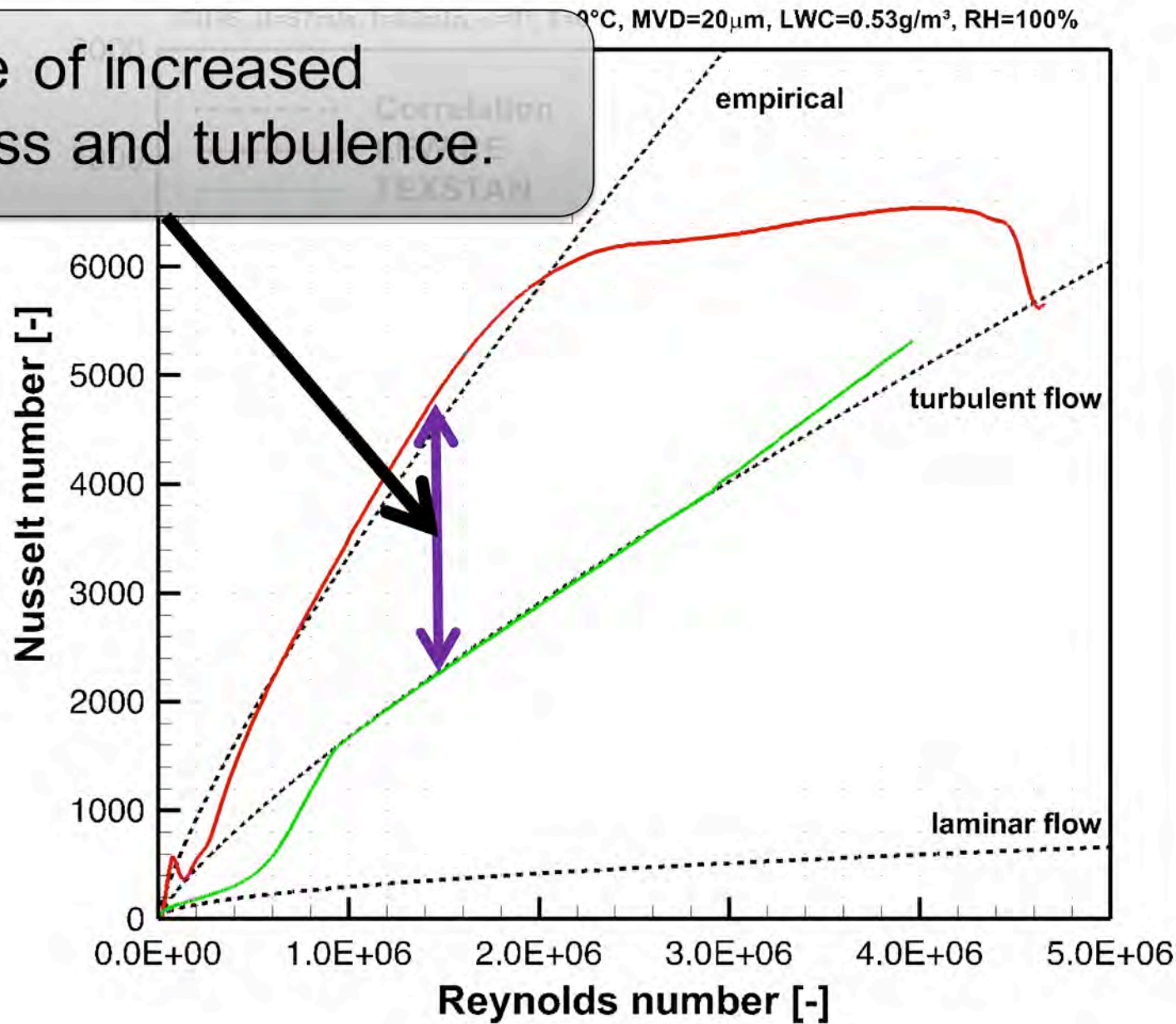
Simulation result for a **clean** airfoil with TEXSTAN.



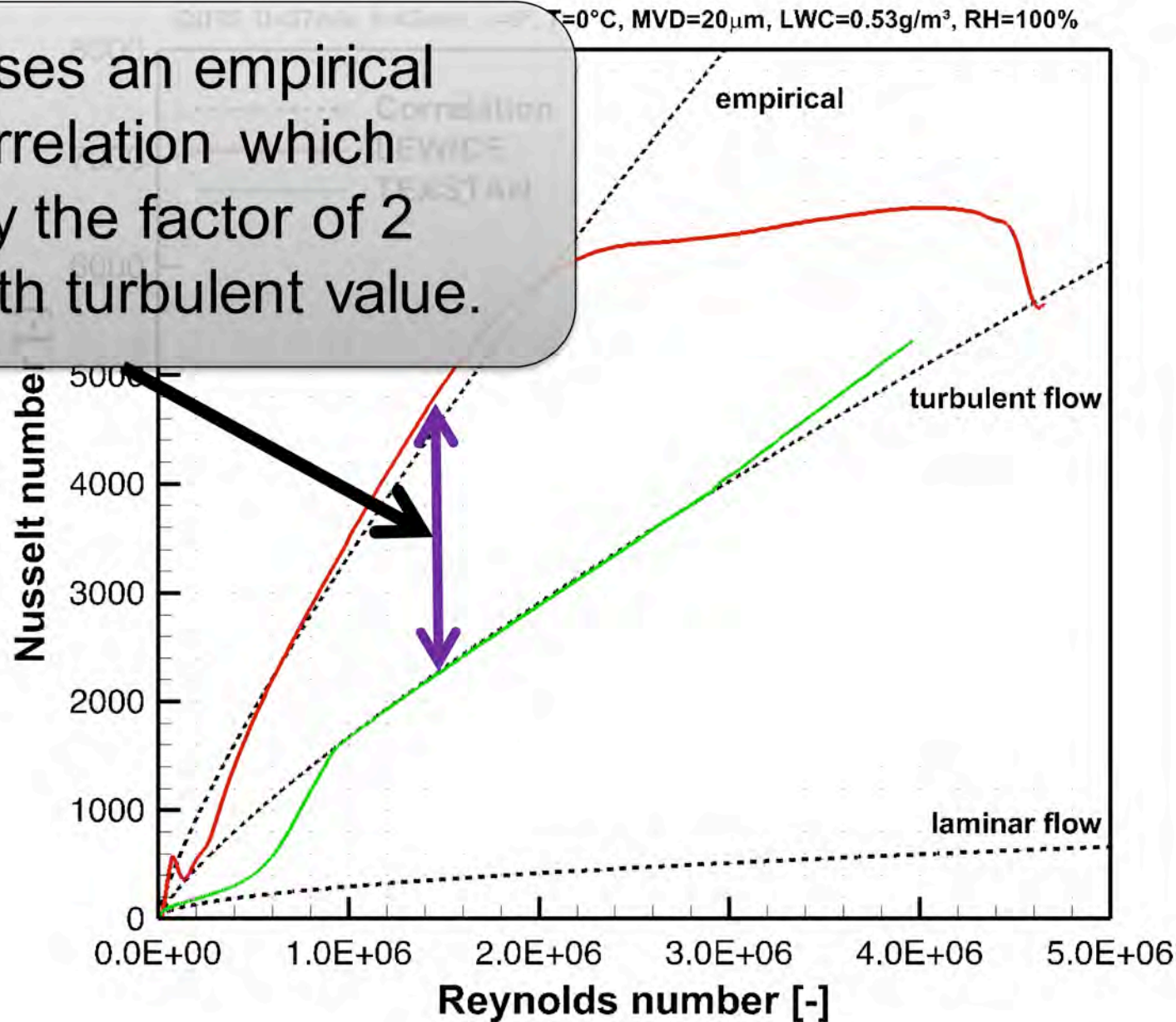
Simulation result for an iced-airfoil with LEWICE.

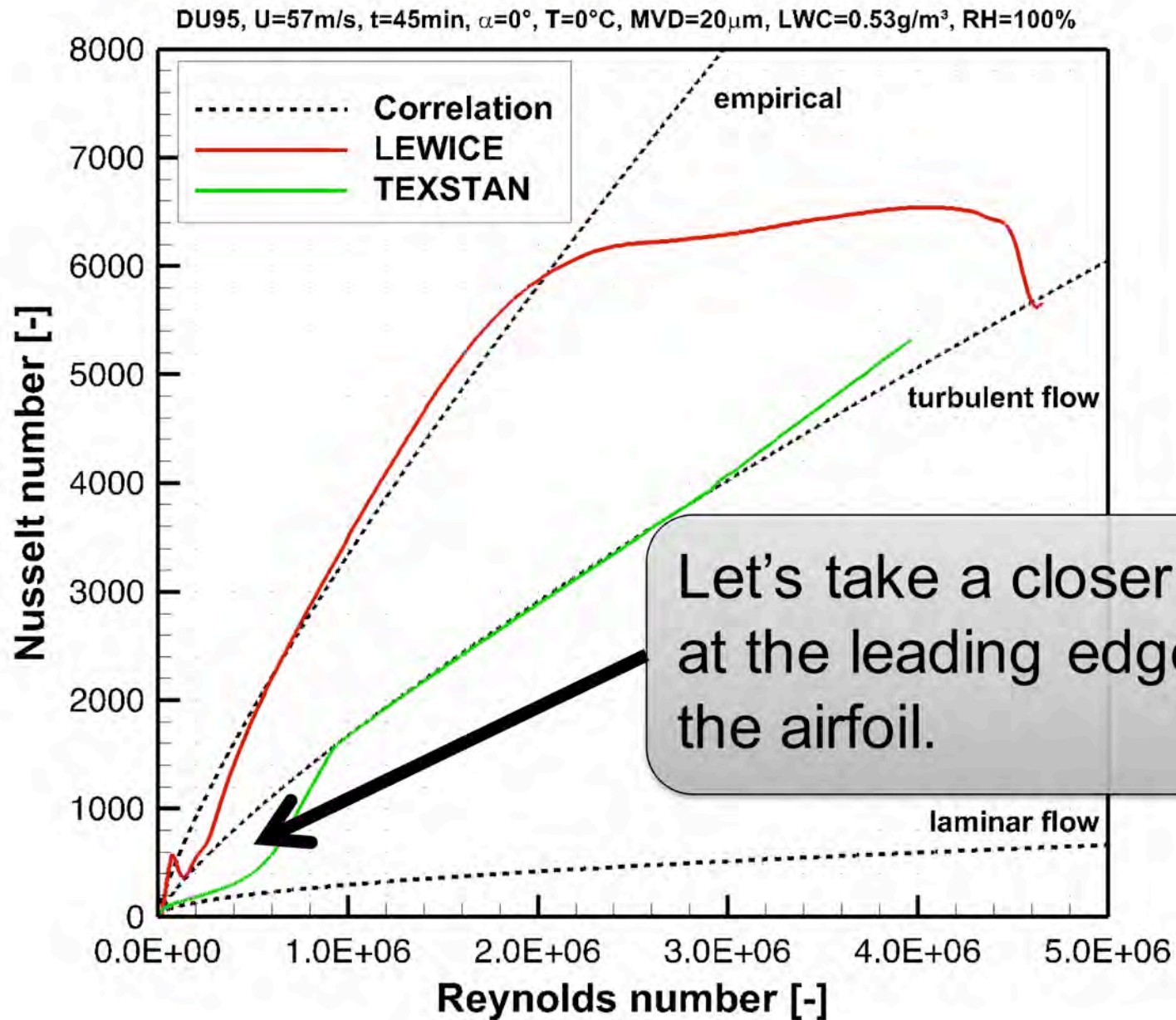


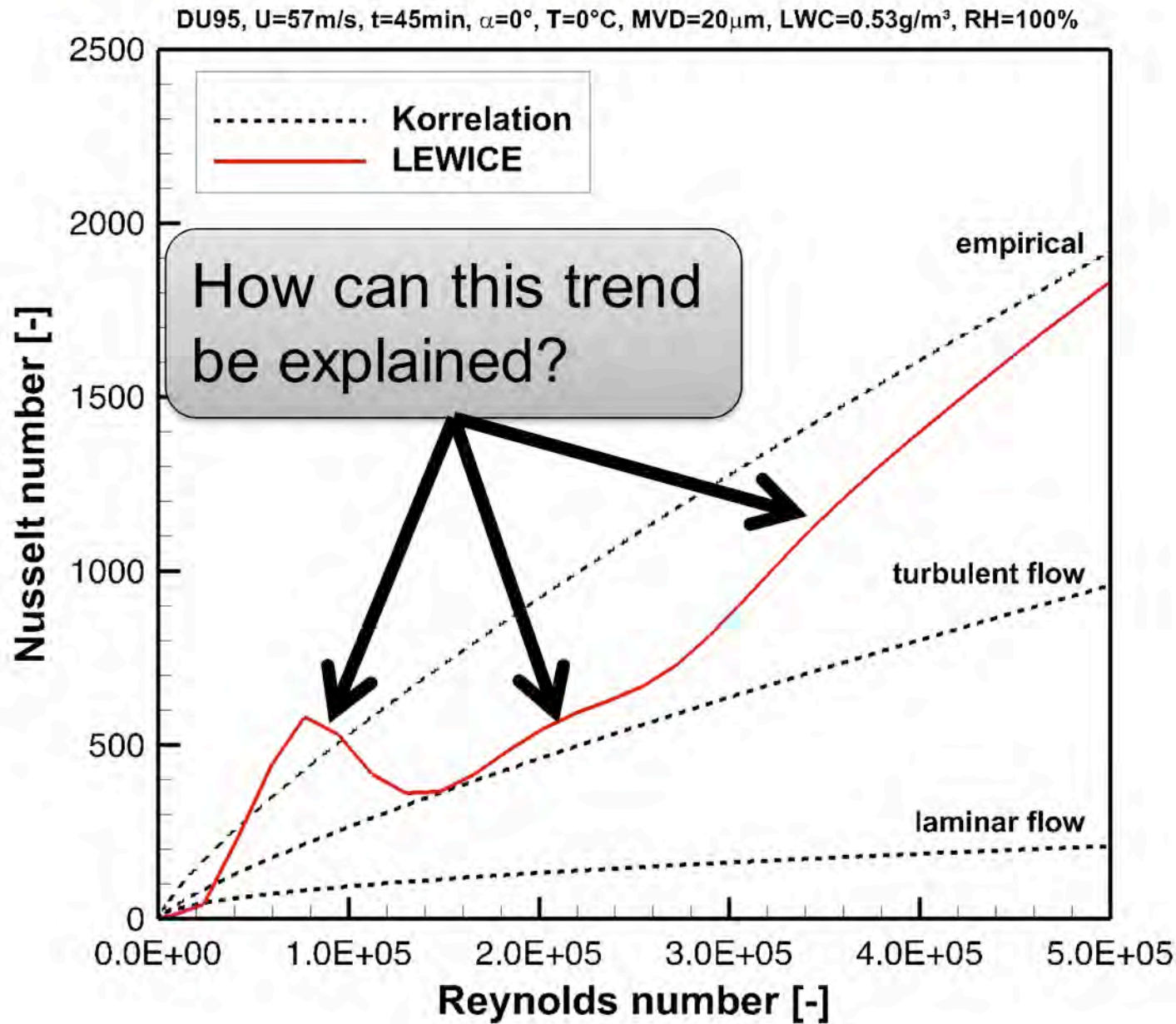
Influence of increased roughness and turbulence.

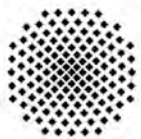
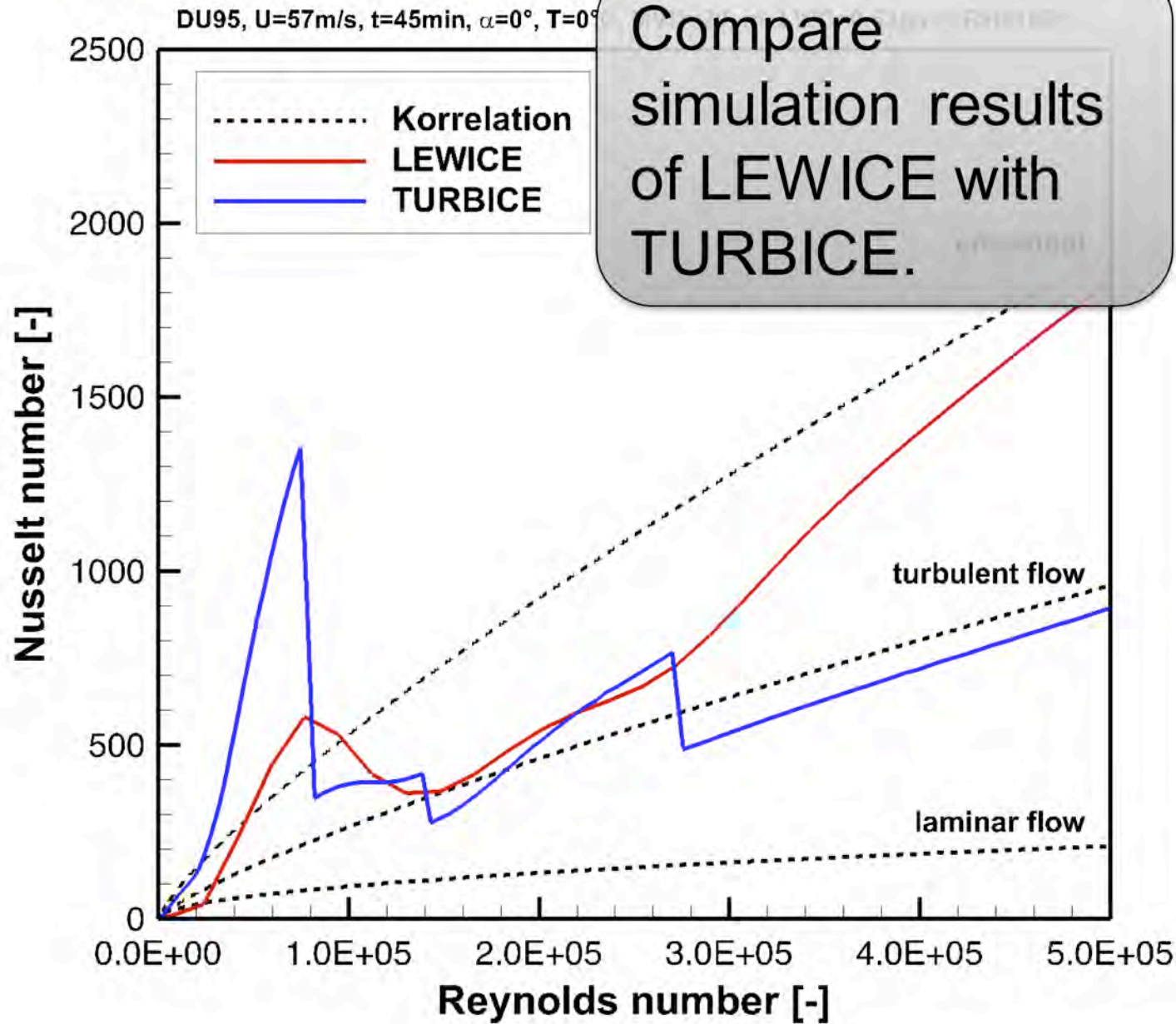


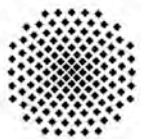
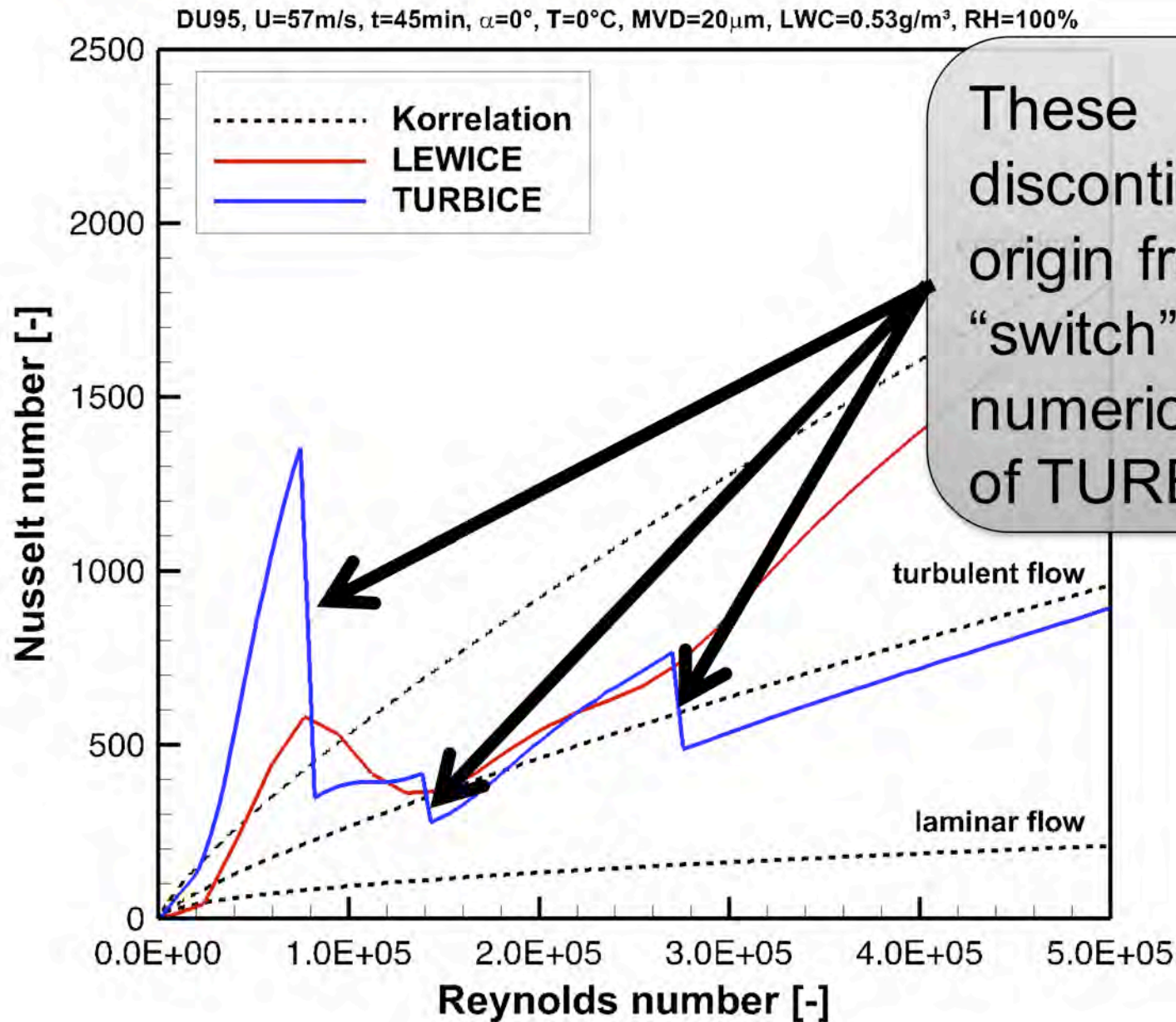
LEWICE uses an empirical Nusselt-correlation which deviates by the factor of 2 from smooth turbulent value.

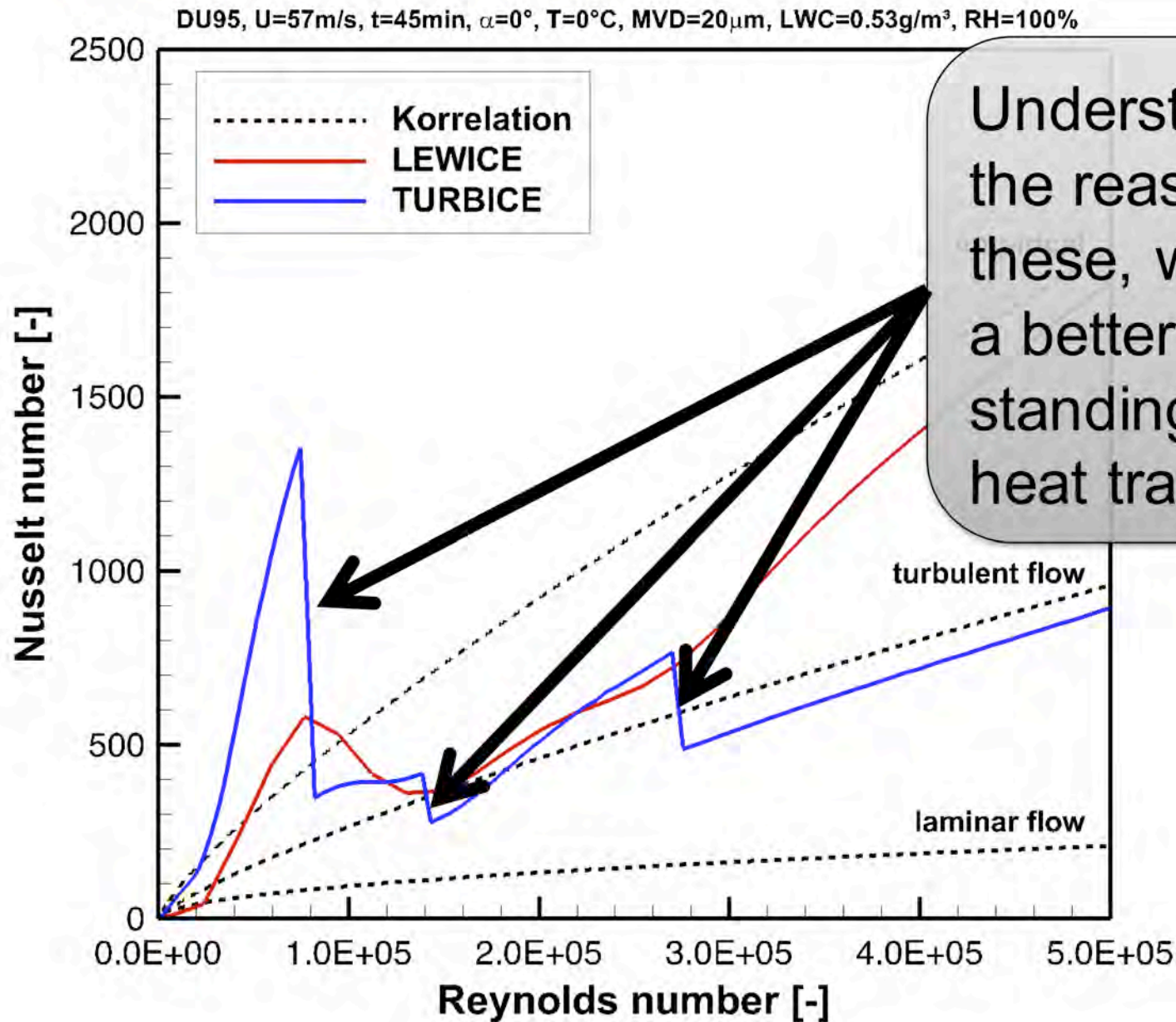




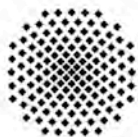


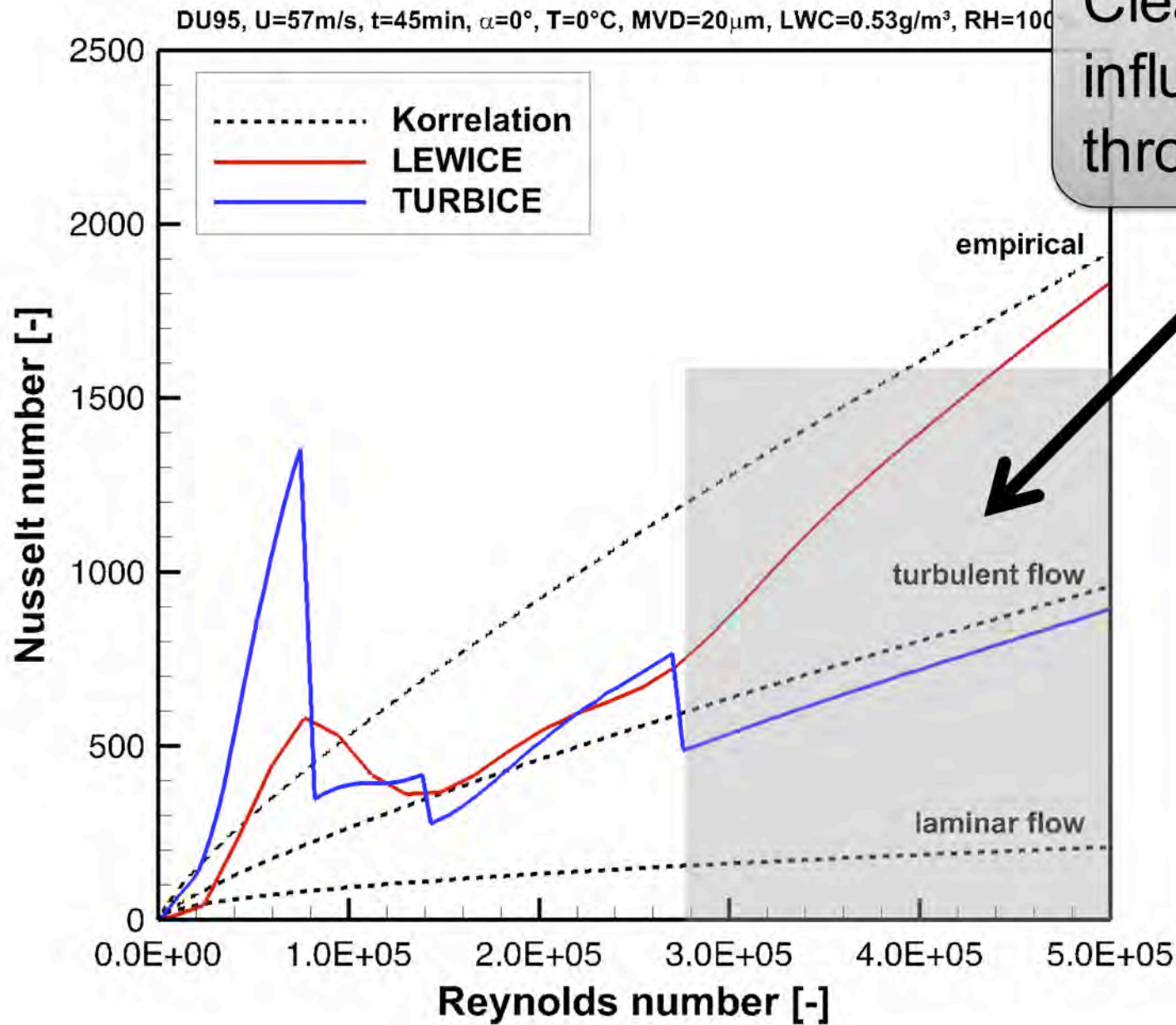




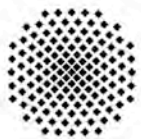


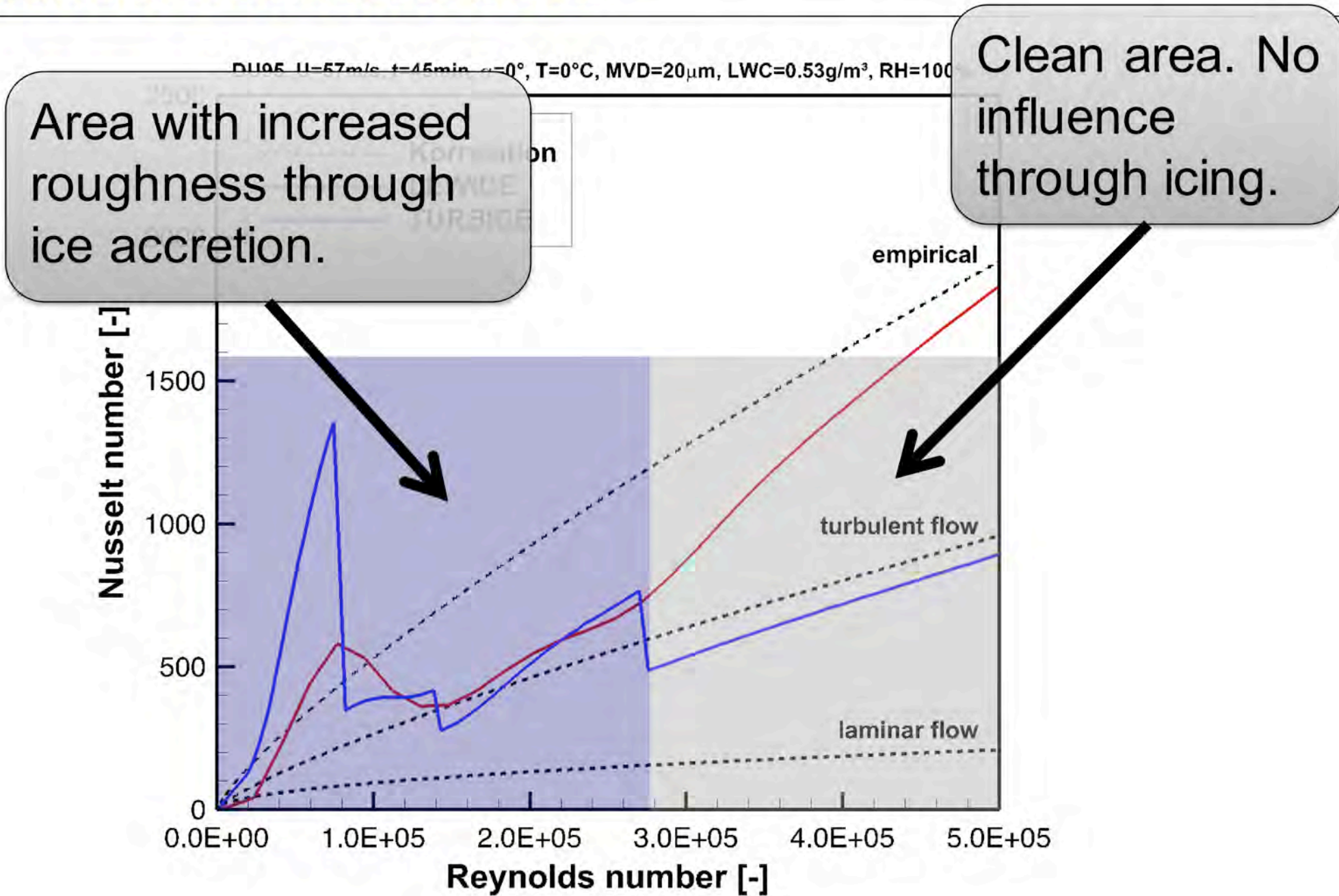
Understanding the reason for these, will lead to a better understanding of the heat transfer.



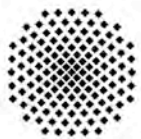
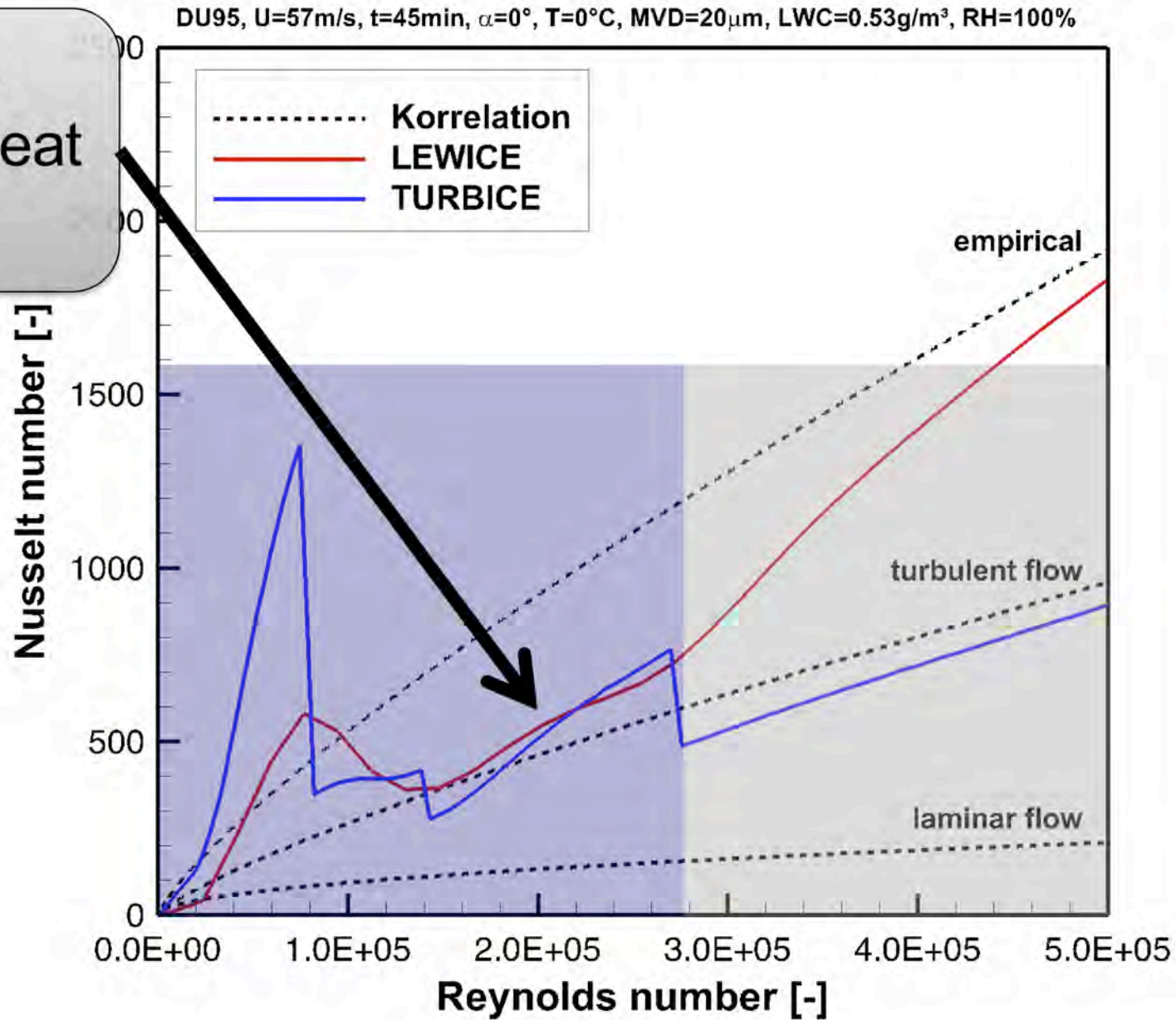


Clean area. No influence through icing.

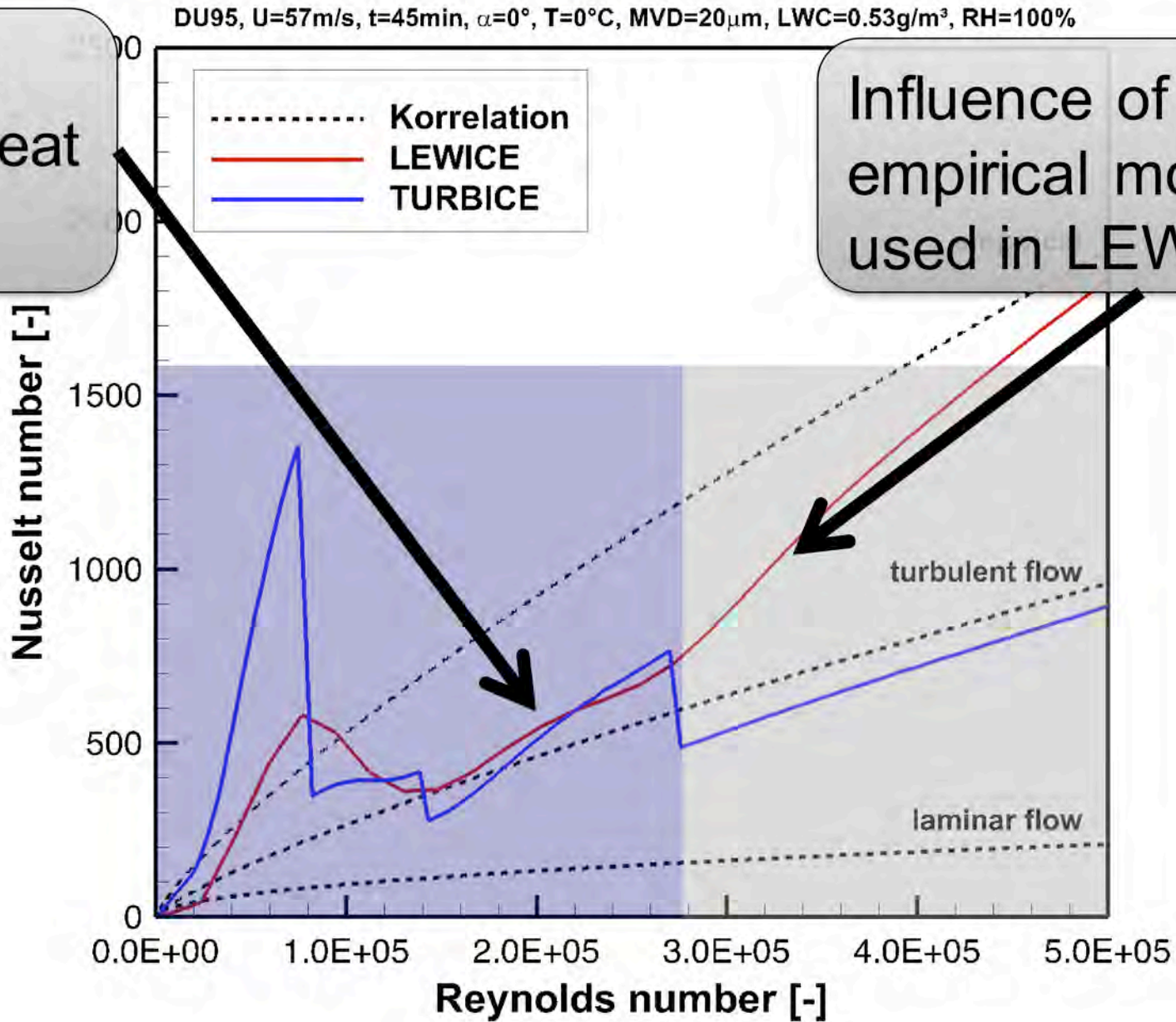




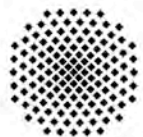
Roughness increases heat transfer.



Roughness increases heat transfer.

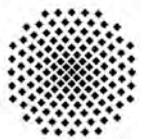
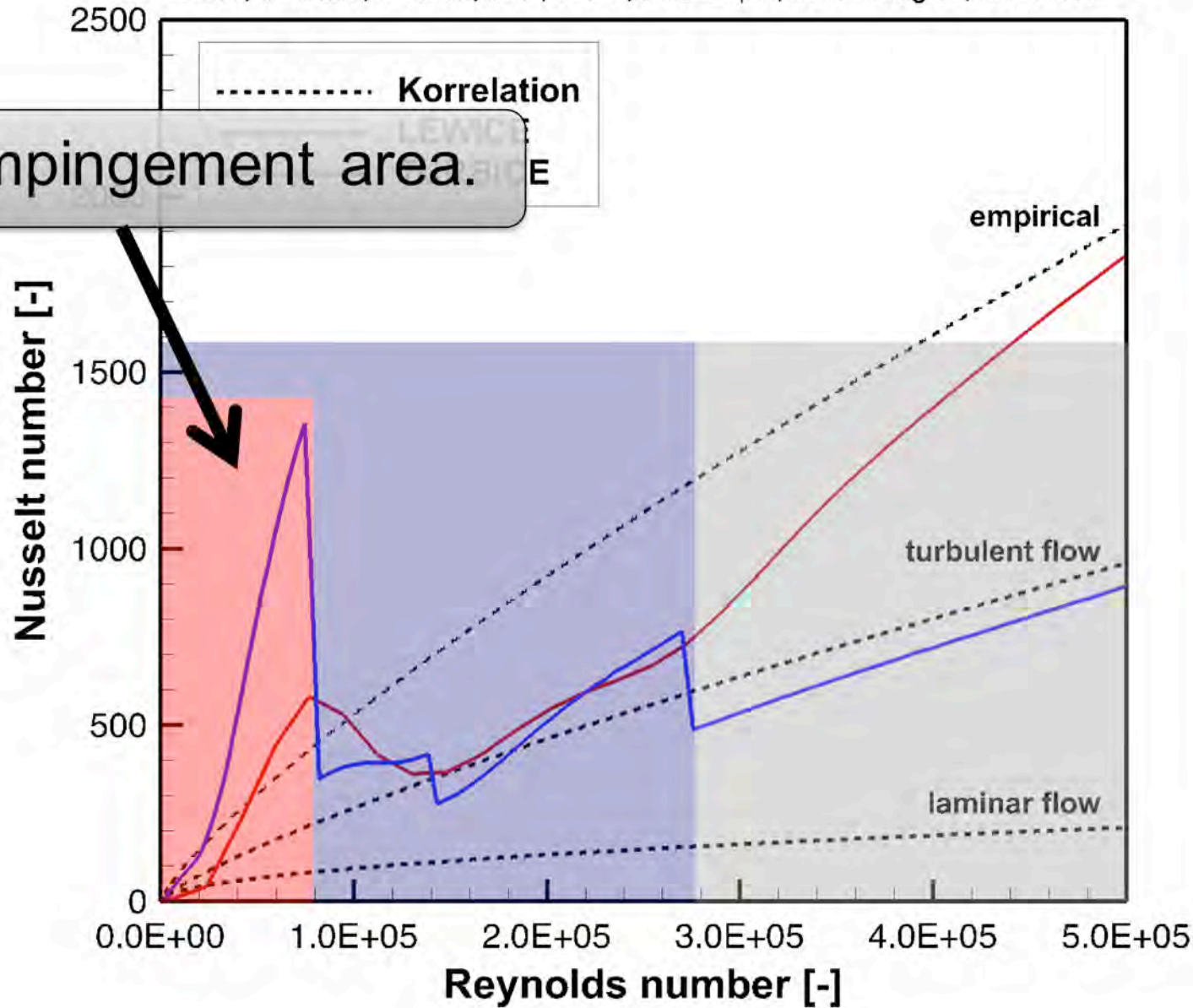


Influence of the empirical models used in LEWICE.

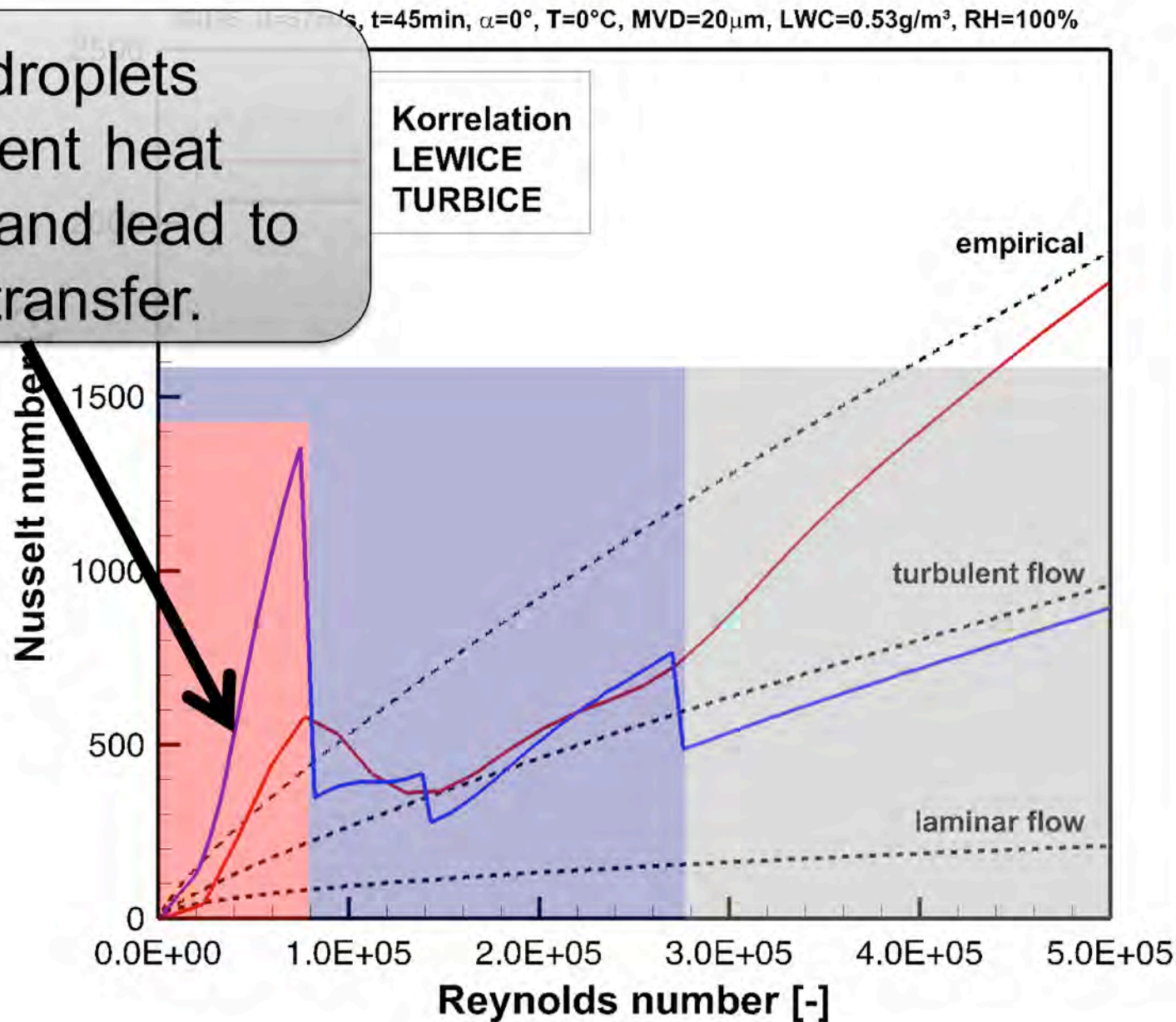


DU95, $U=57\text{m/s}$, $t=45\text{min}$, $\alpha=0^\circ$, $T=0^\circ\text{C}$, $\text{MVD}=20\mu\text{m}$, $\text{LWC}=0.53\text{g/m}^3$, $\text{RH}=100\%$

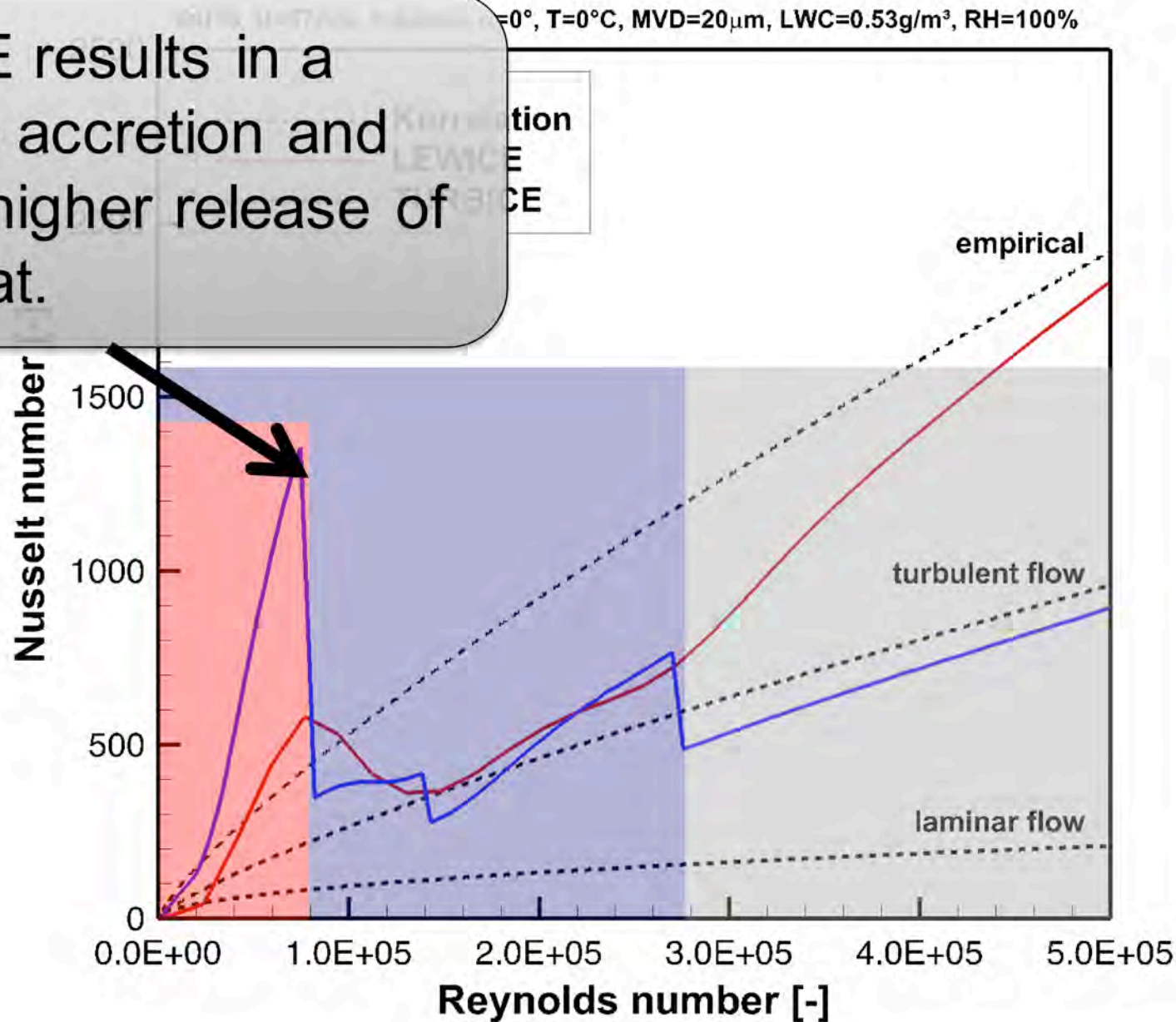
Droplet impingement area.



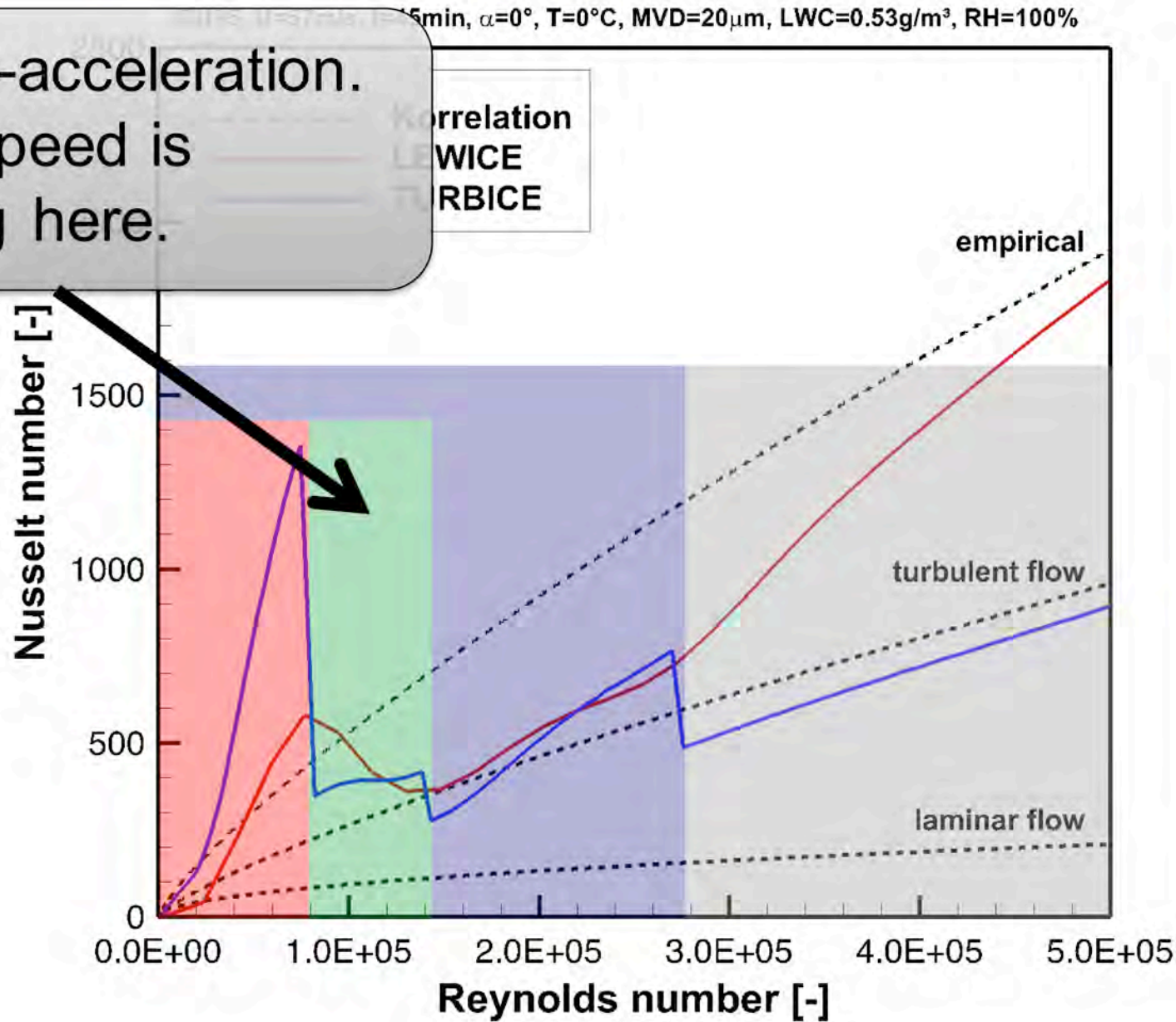
Incoming droplets release latent heat (freezing) and lead to high heat transfer.

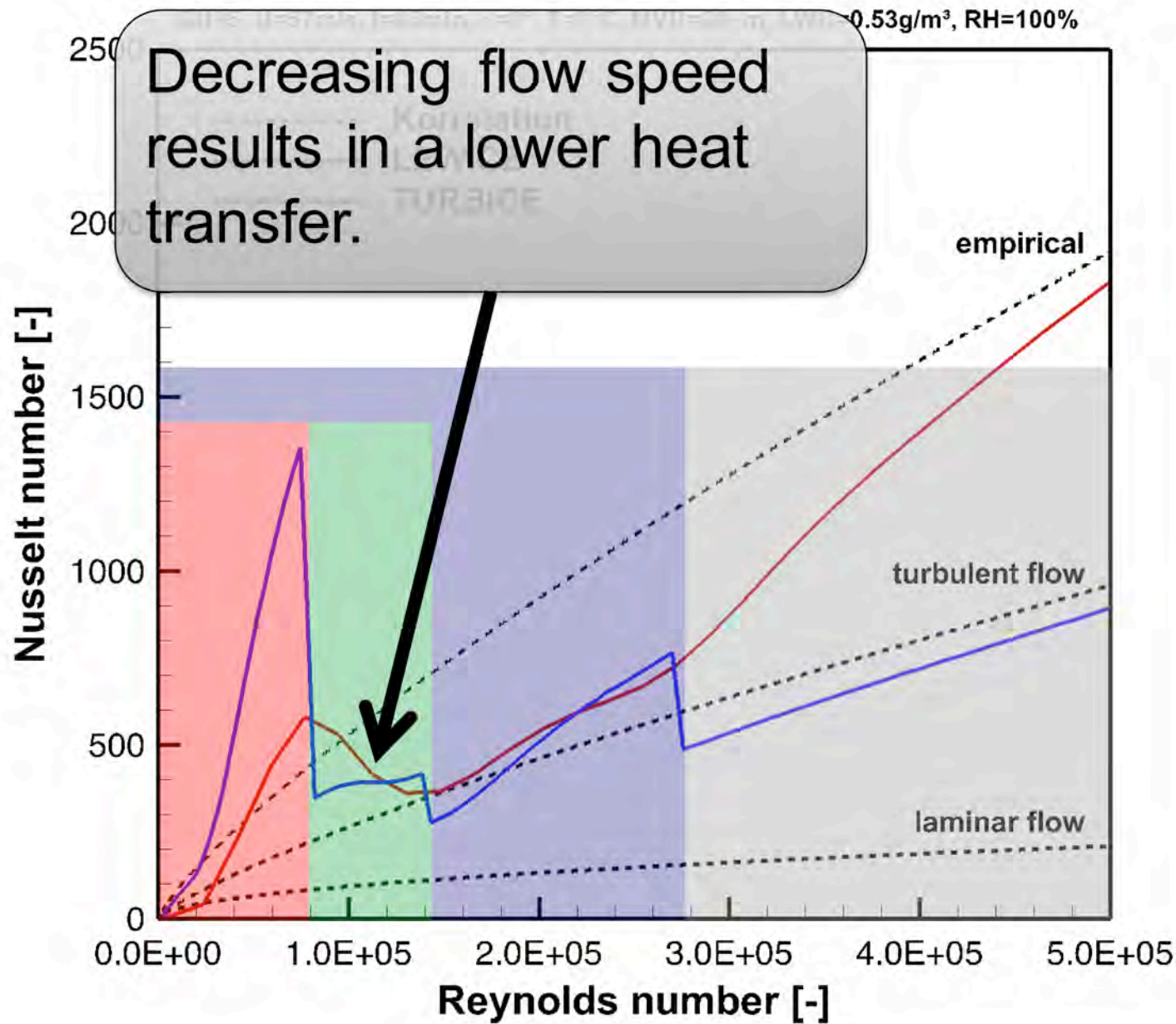


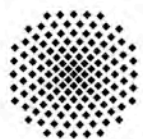
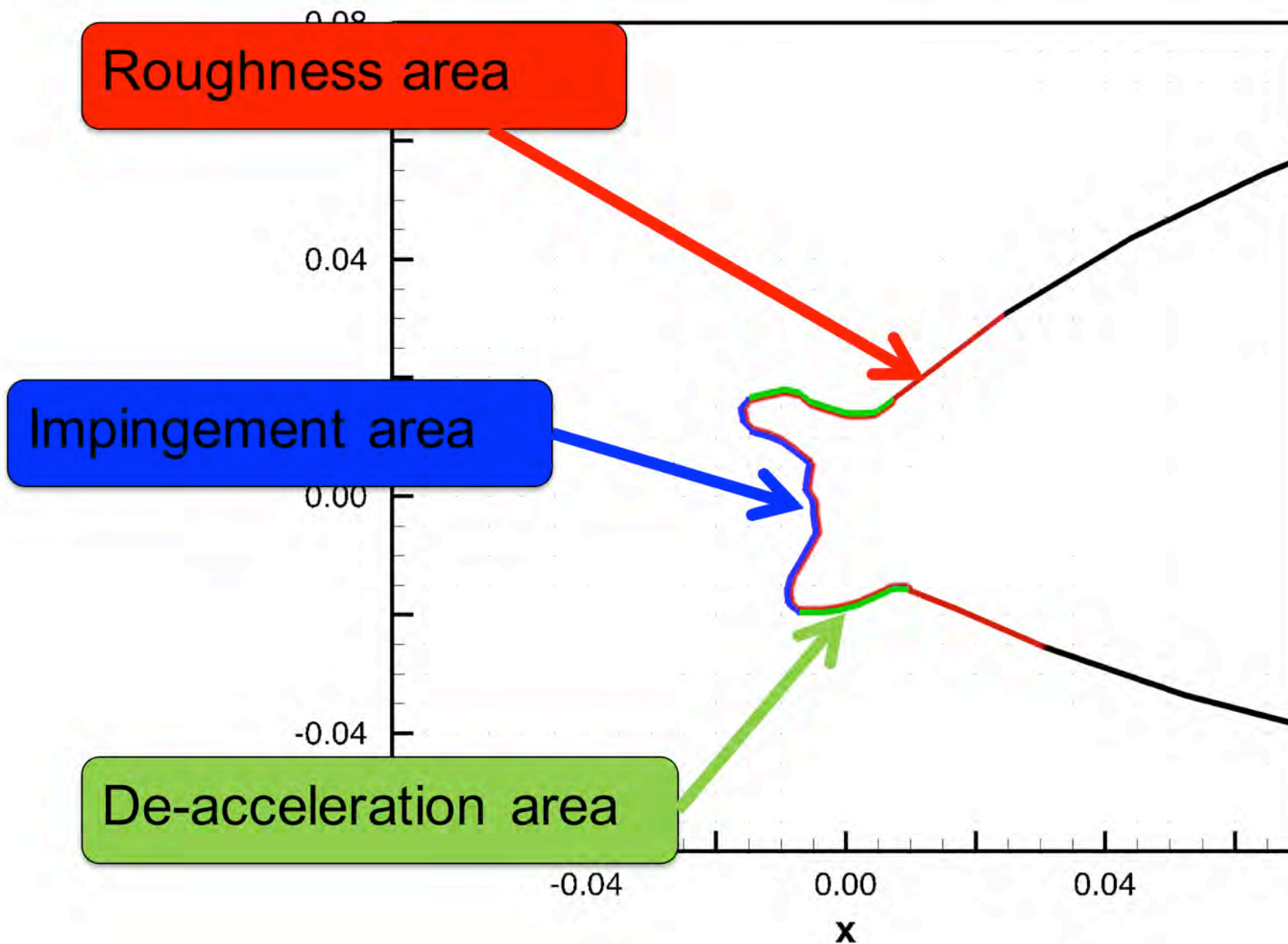
TURBICE results in a larger ice accretion and hence a higher release of latent heat.



Area of de-acceleration.
The flow speed is
decreasing here.

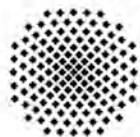






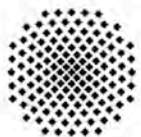


- The numerical models used for the heat transfer are highly influenced by empirical correlations.
- Closer investigation of the physical processes is required!
- BUT: the numerical models of LEWICE and TURBICE are still valid. Just because empirical correlations are used does not mean that the results are incorrect.

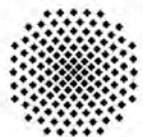
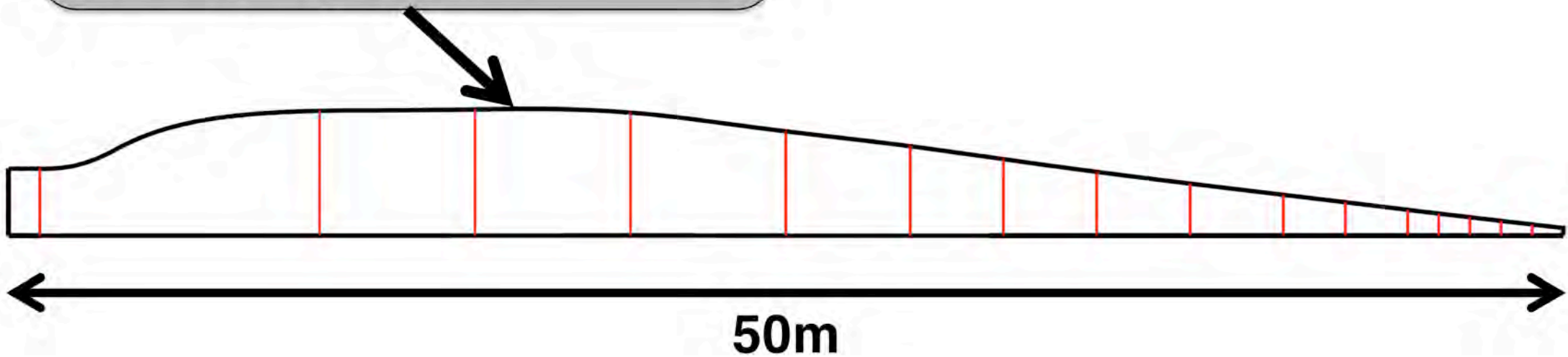


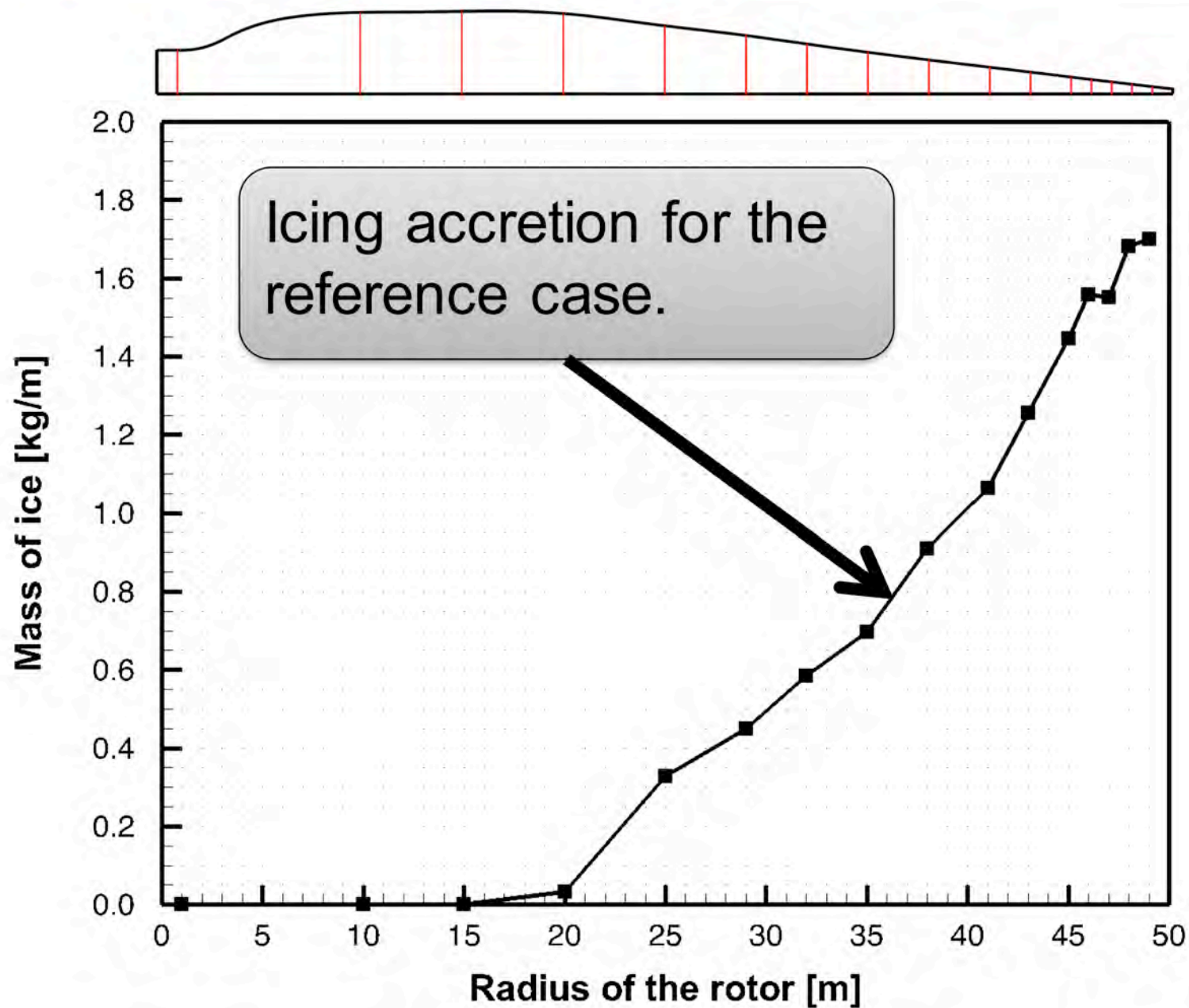


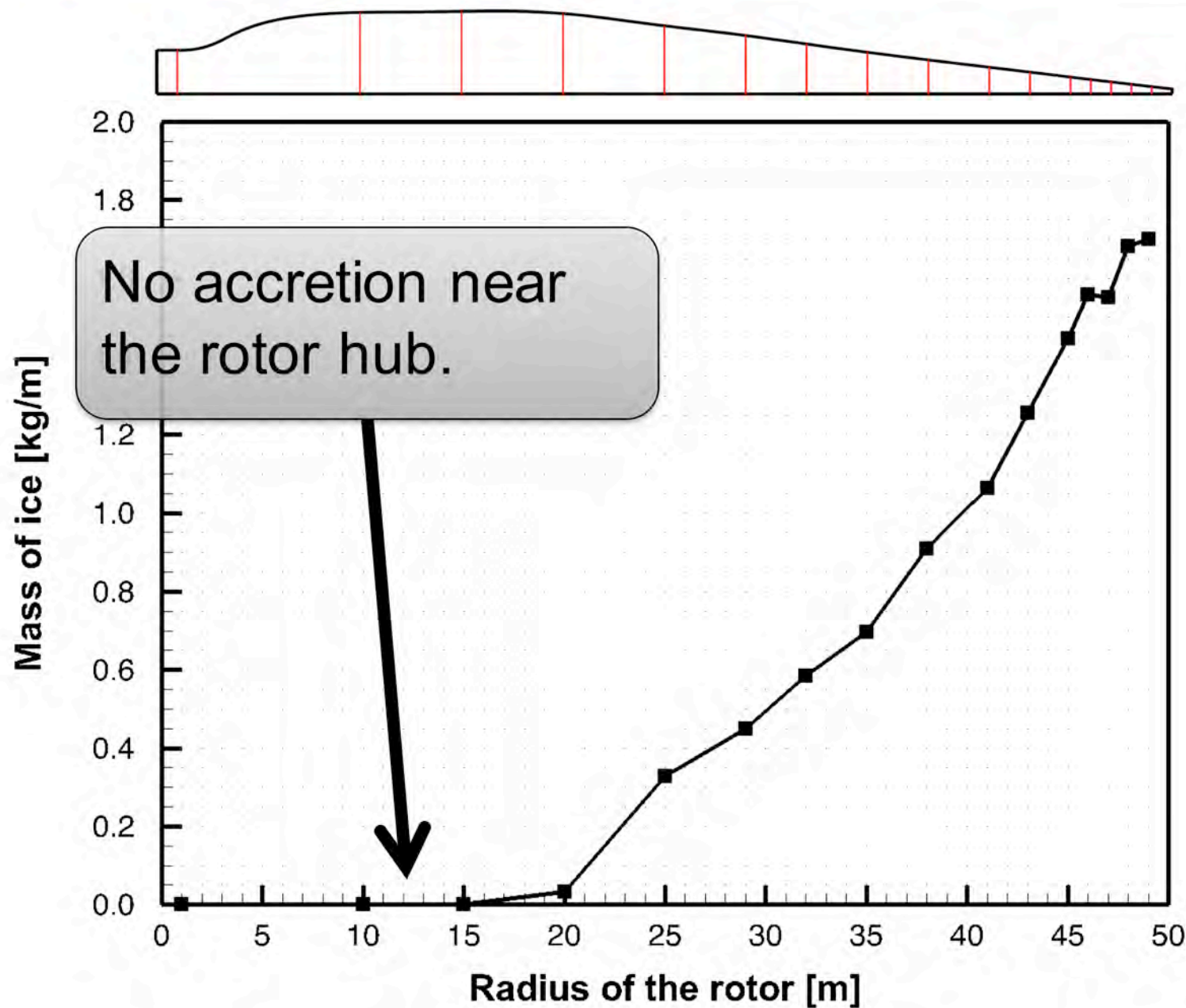
„Where does ice accrete on a rotor blade?“

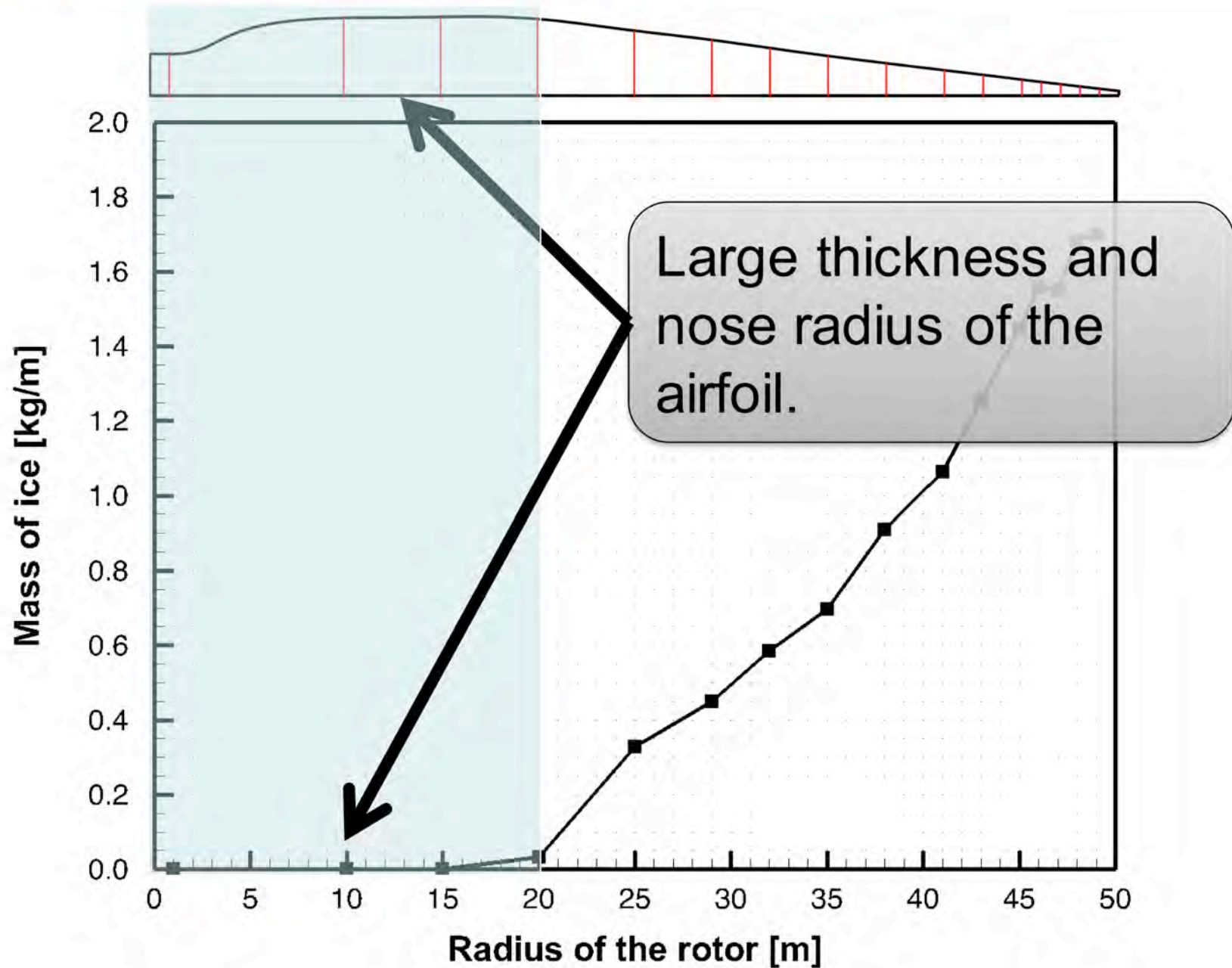


Generic rotor blade for a
2.5MW wind turbine.
16 sampling points.



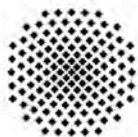


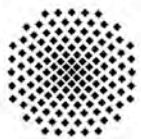
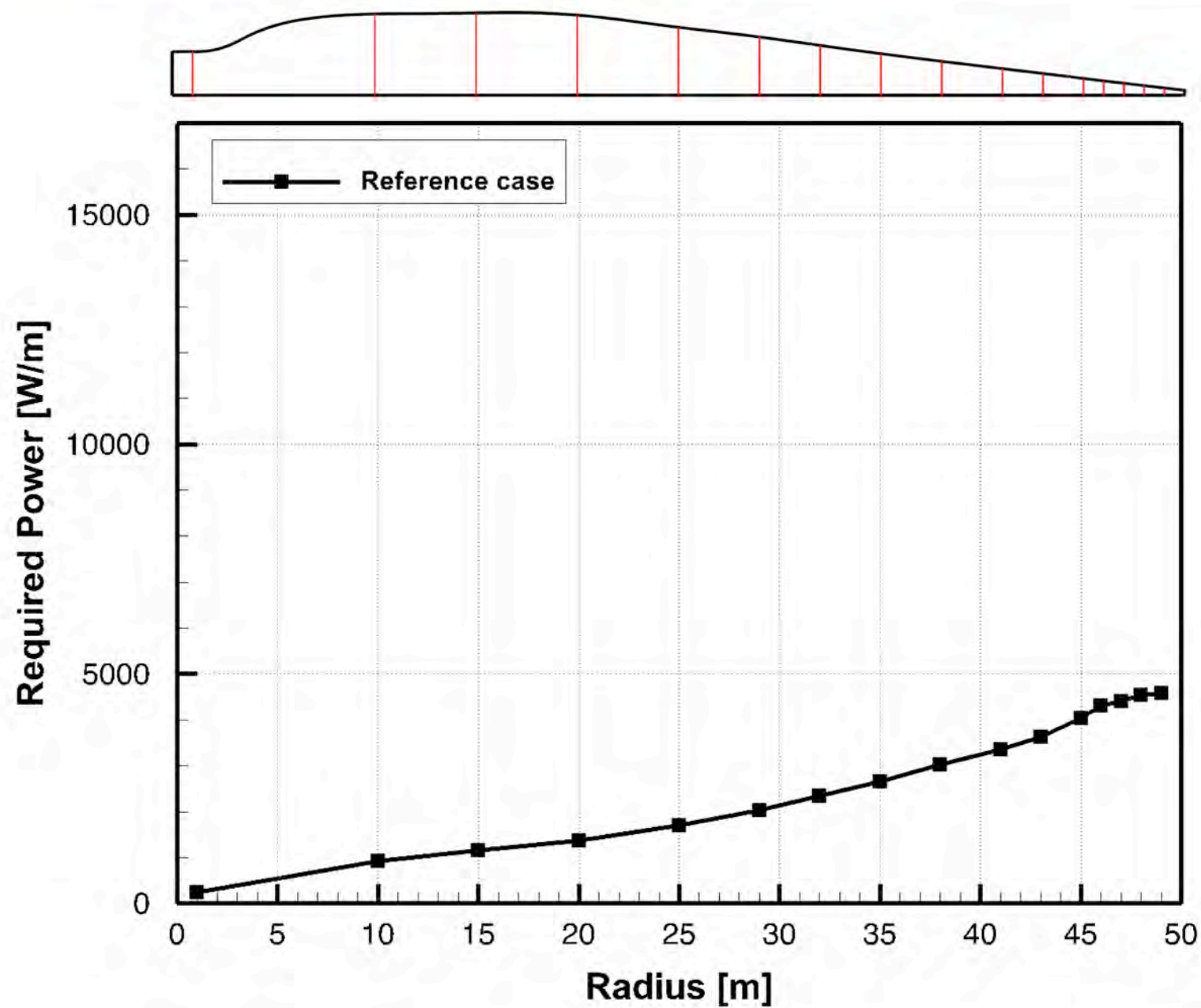


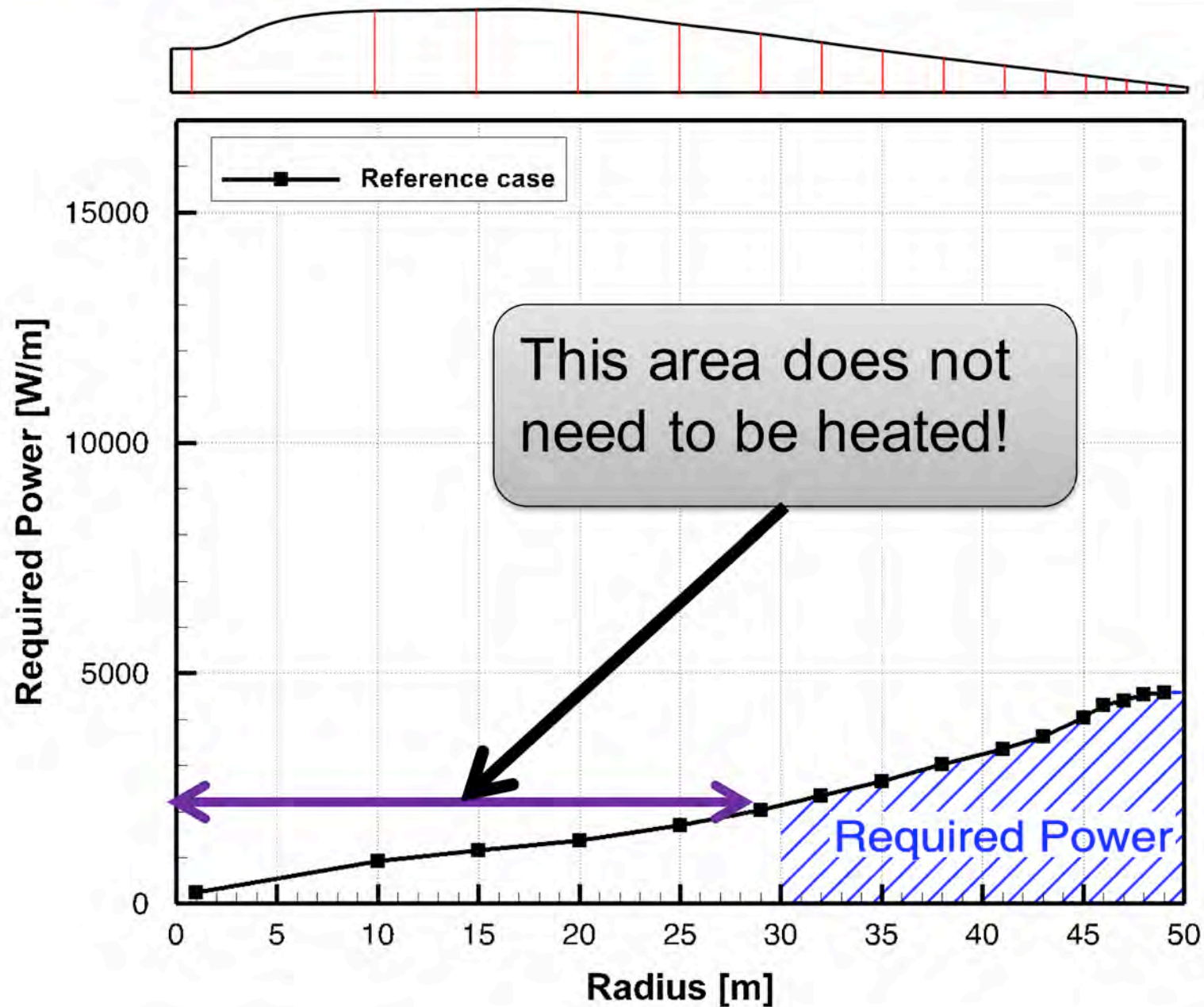


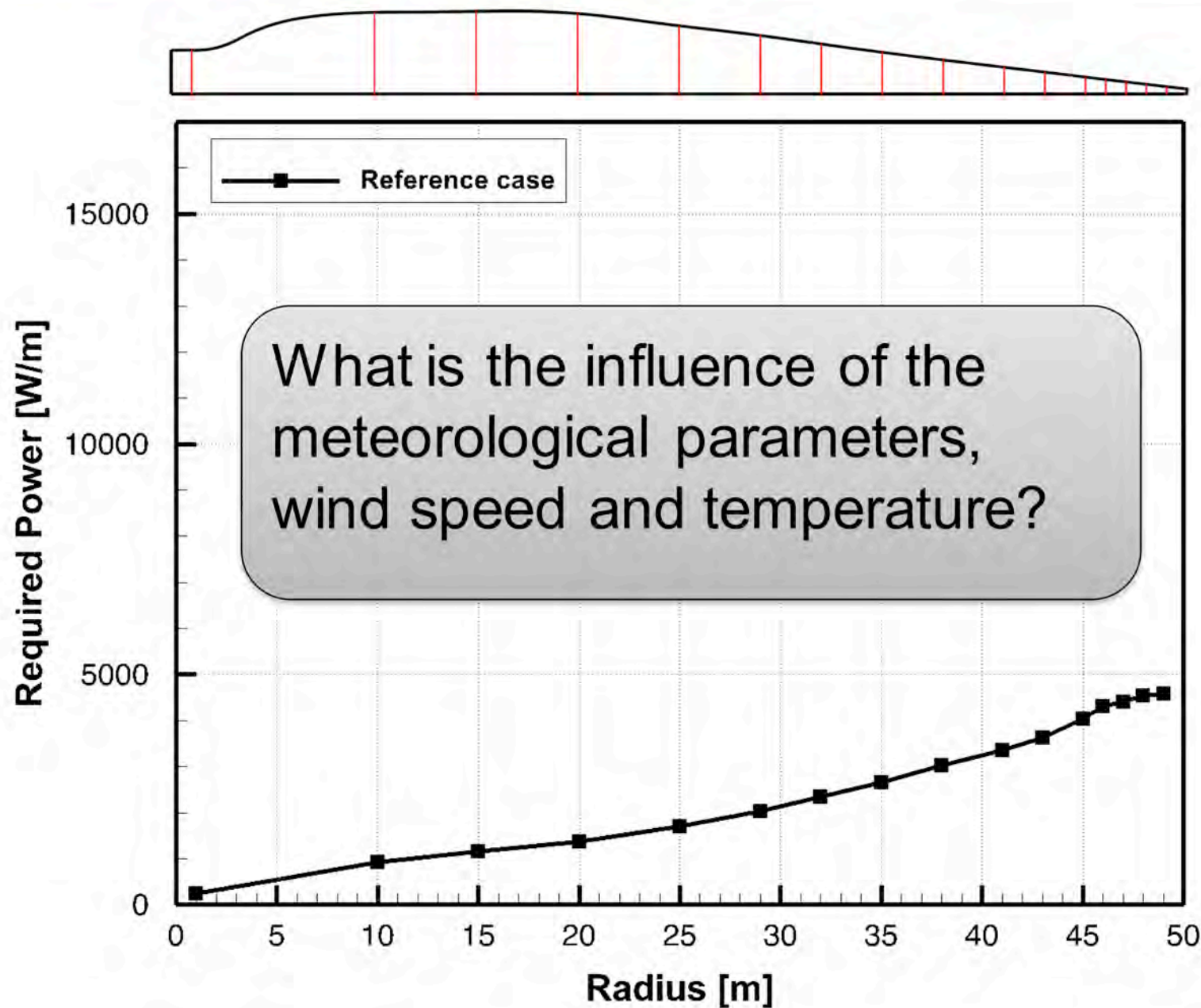


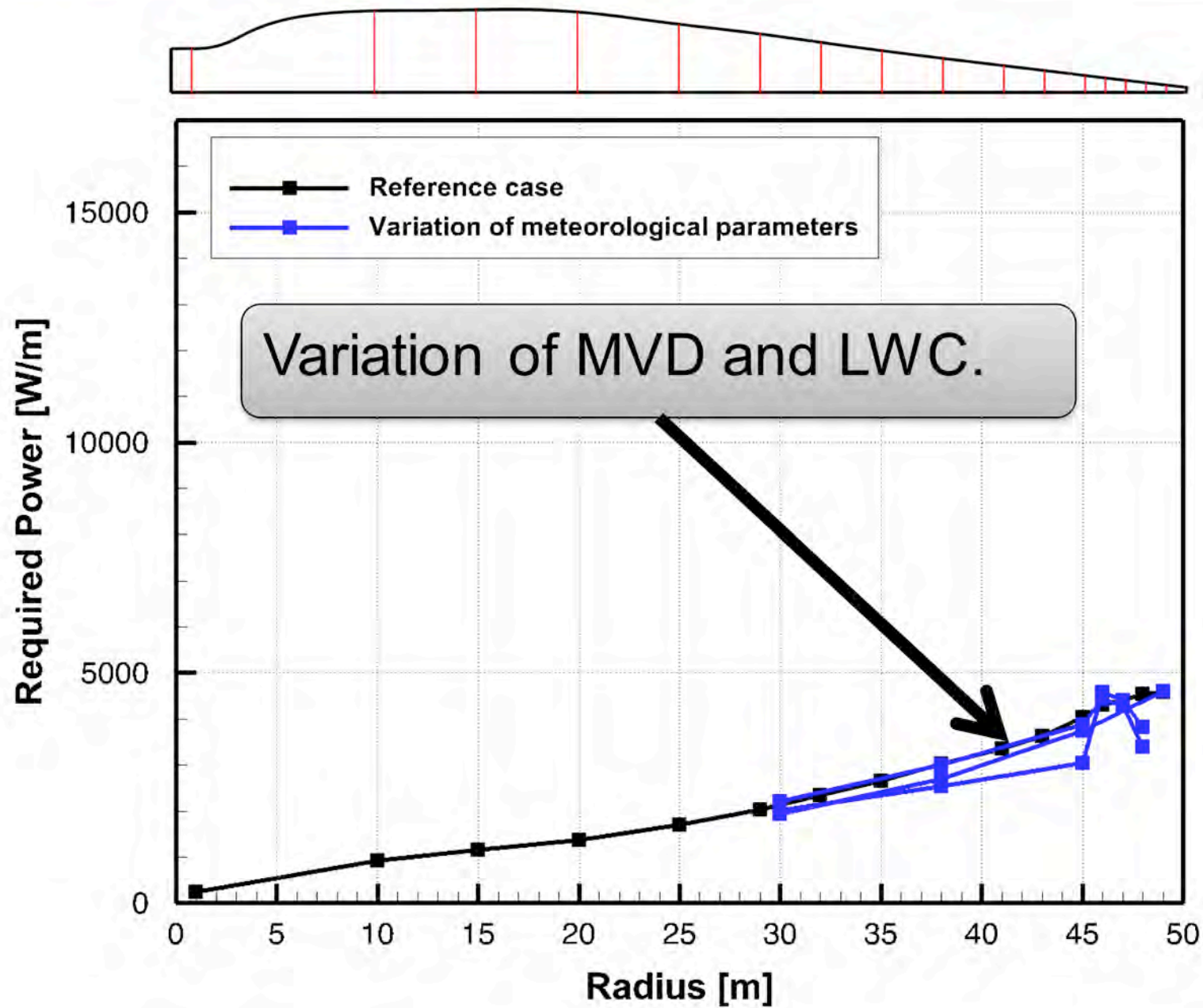
„How much power is required for anti-icing?“

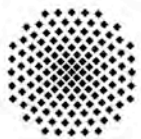
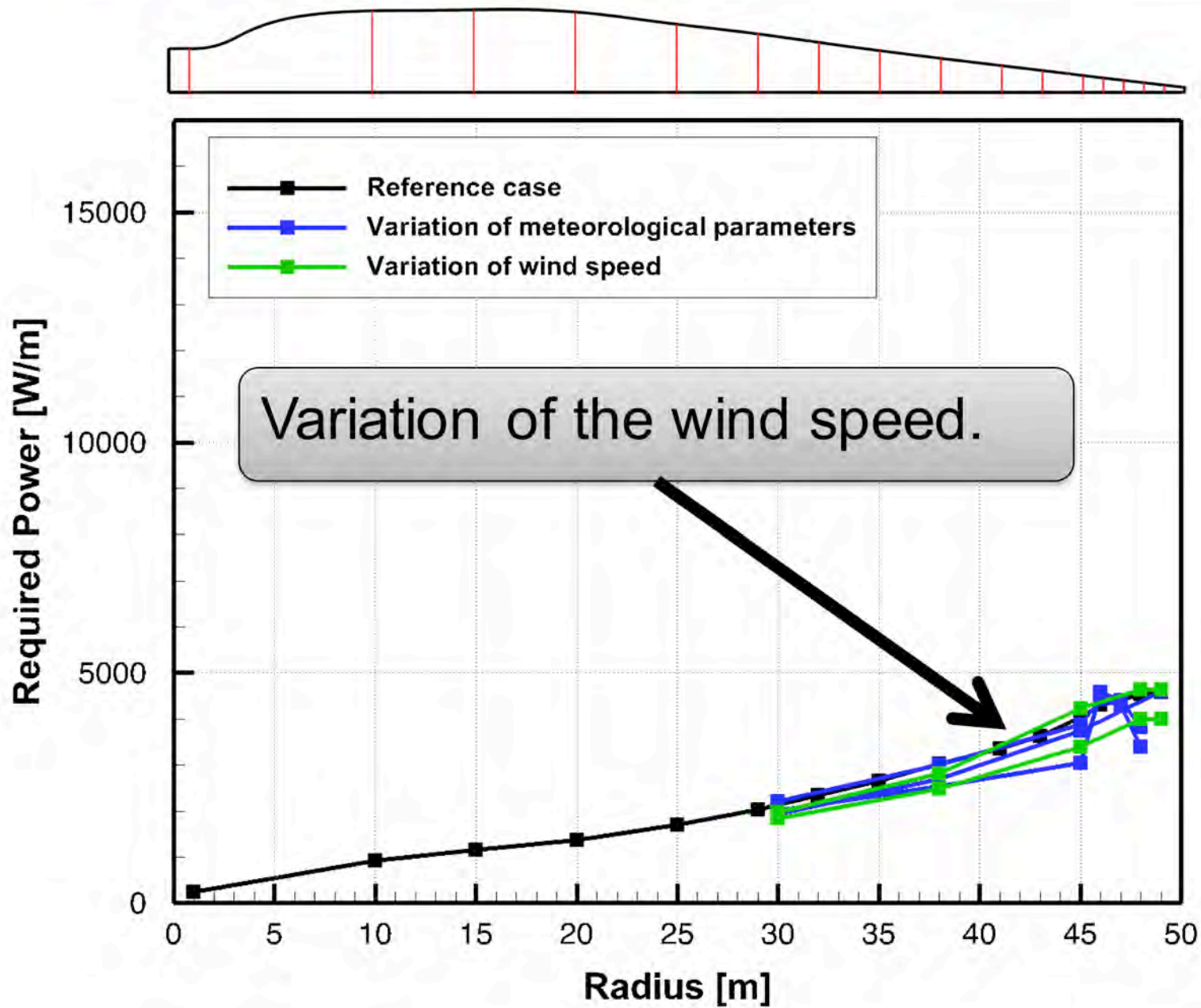


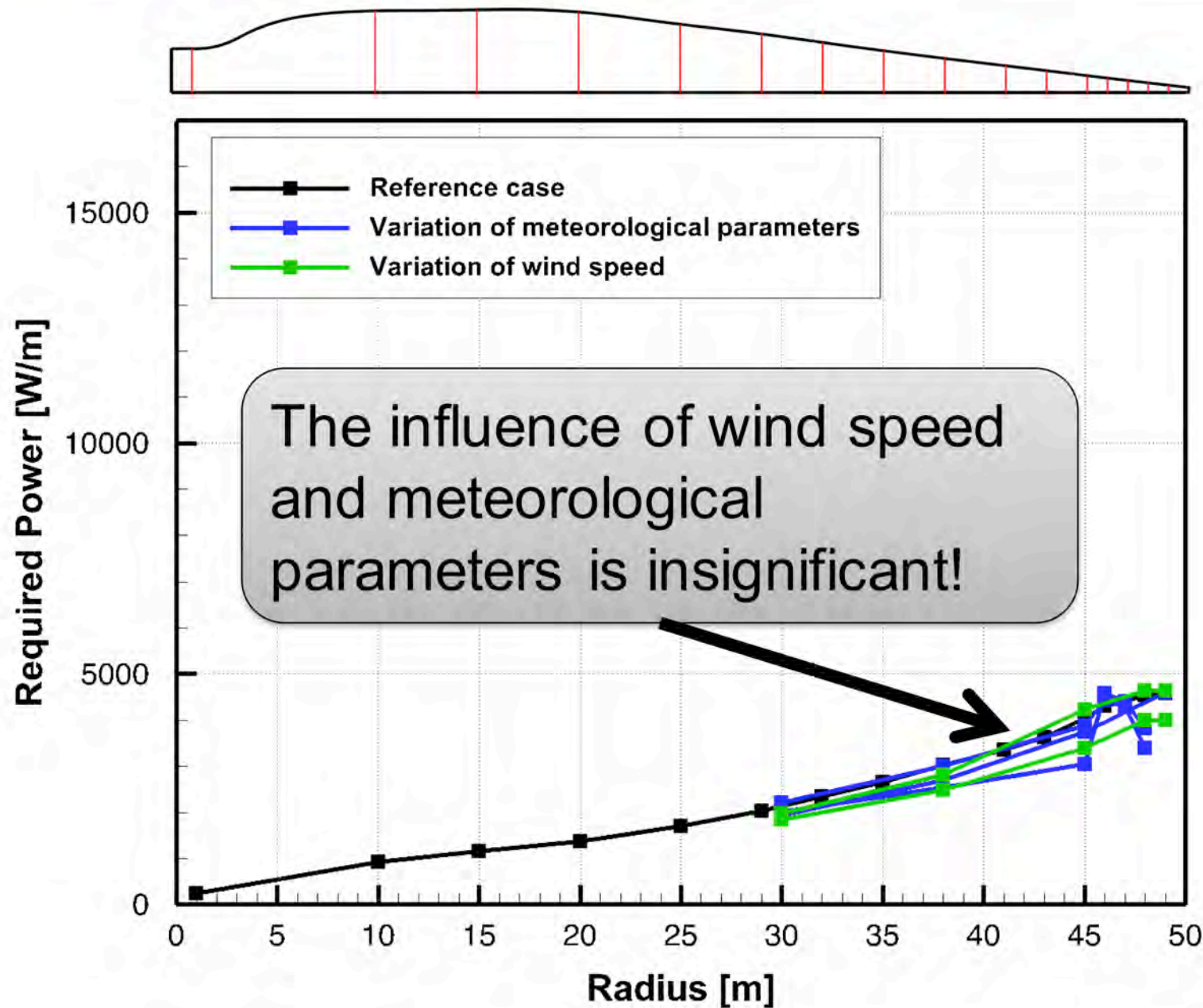


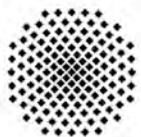
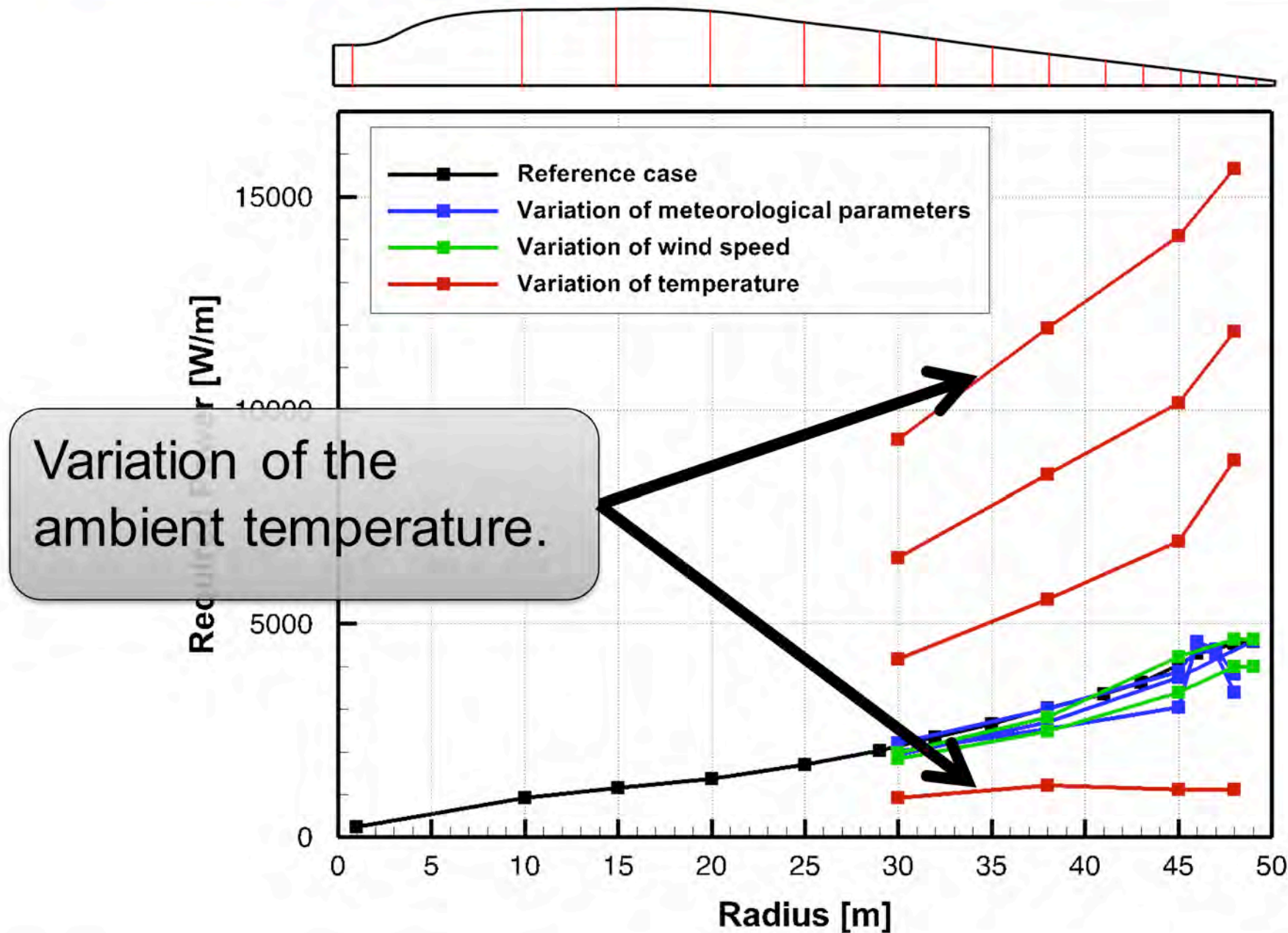


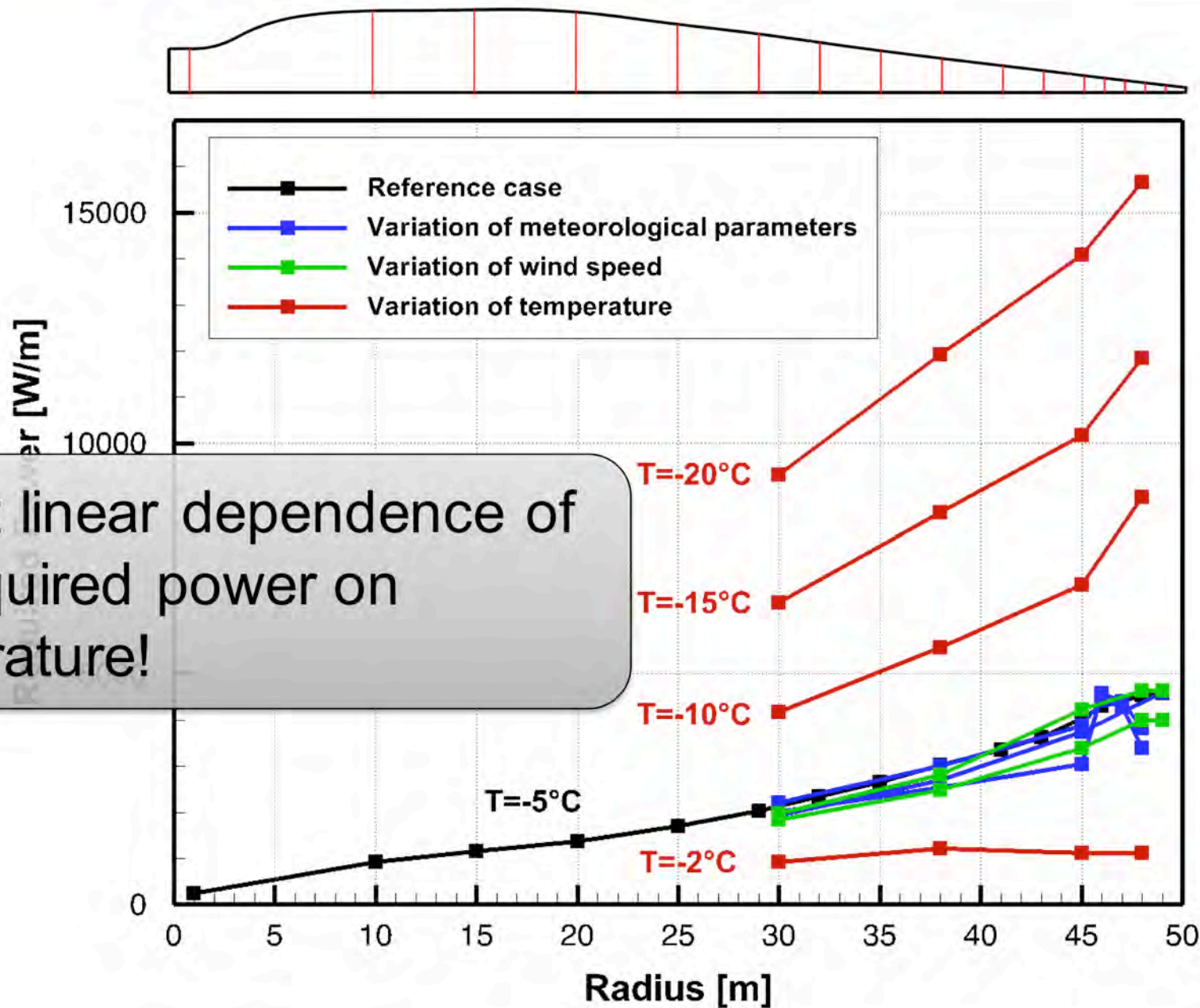




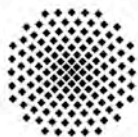




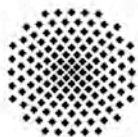
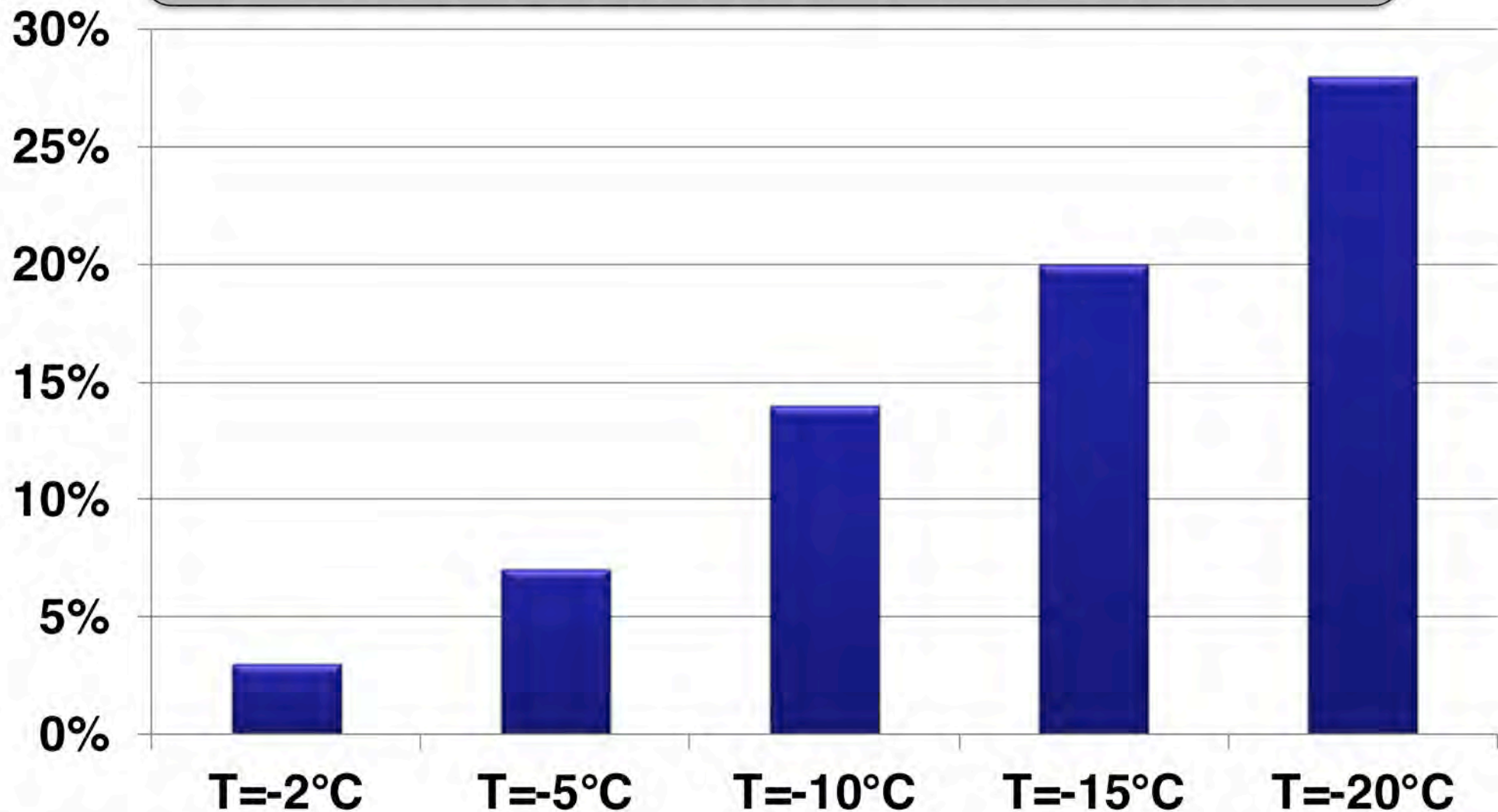




Almost linear dependence of the required power on temperature!



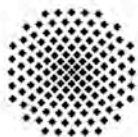
Fraction of the required heating power on the output of a 2.5MW wind turbine (\varnothing 100m).



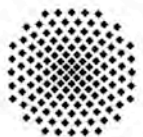
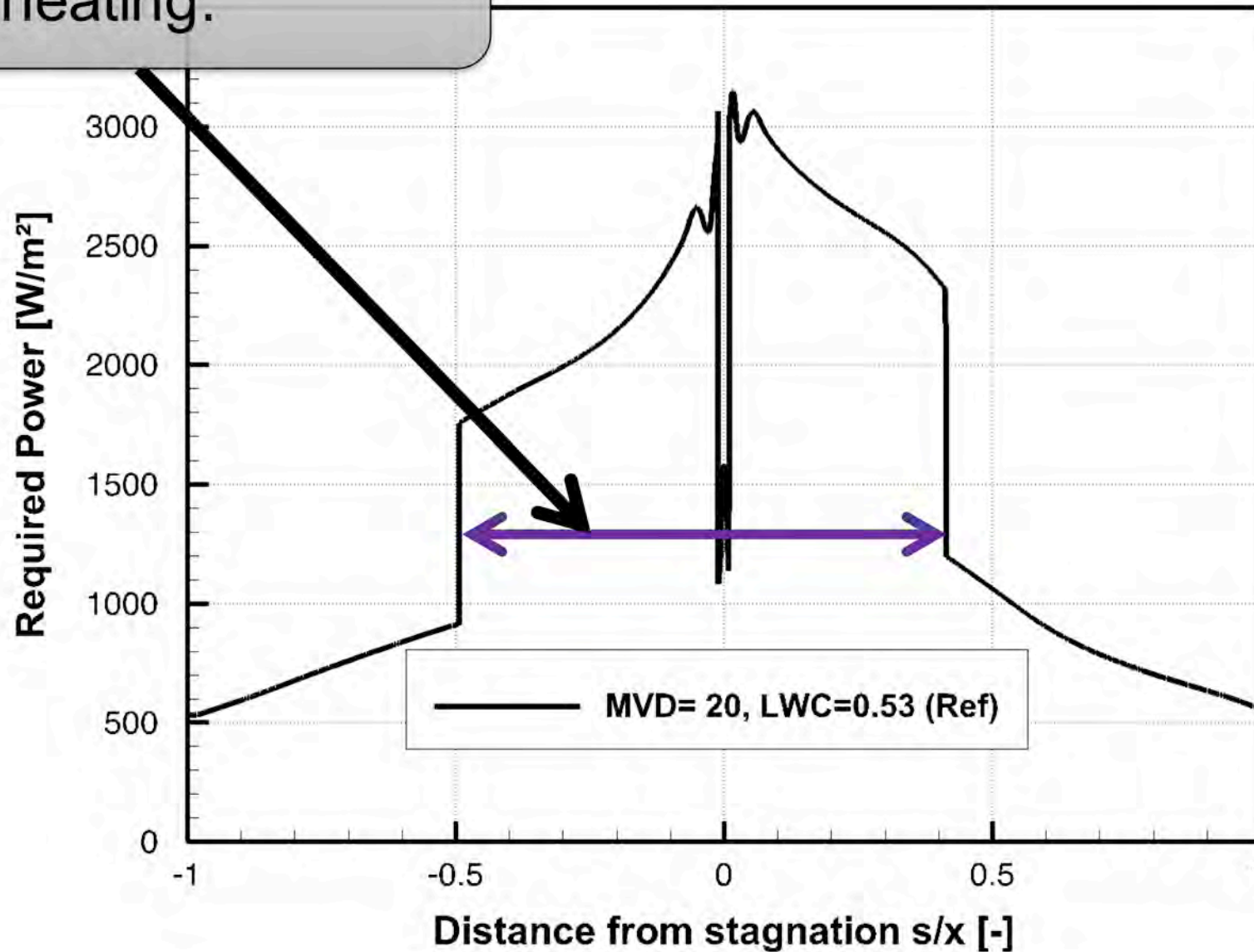


- The amount of required power for anti-icing mainly depends on the ambient temperature and the size of the rotor.
- Very low ambient temperatures will result in very high required heating amounts.
- Efficiency can be increased by only heating the outer parts of the blade.

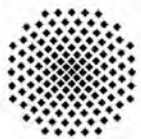
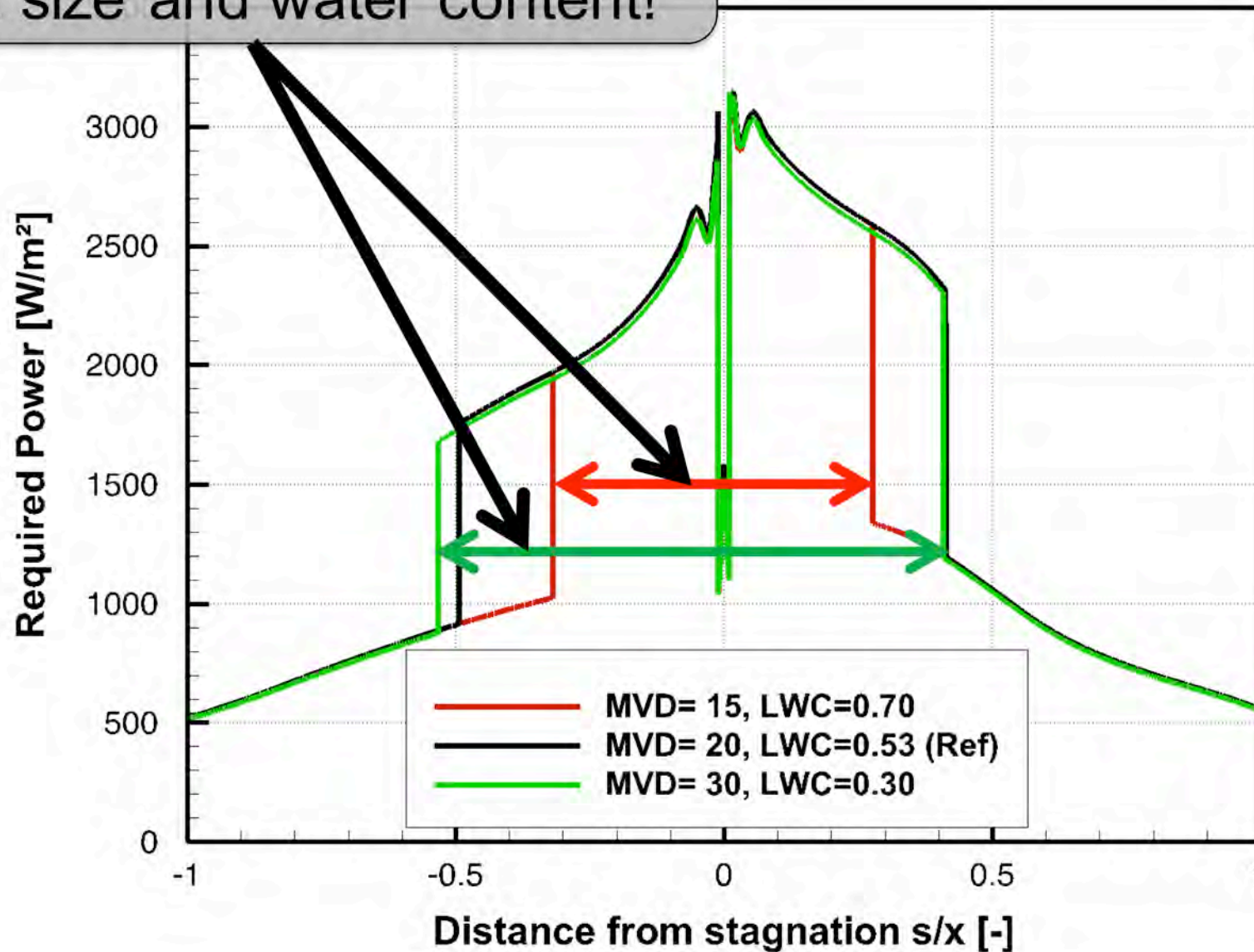
Further improvement of the efficiency can be obtained by only heating the leading edge.



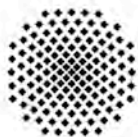
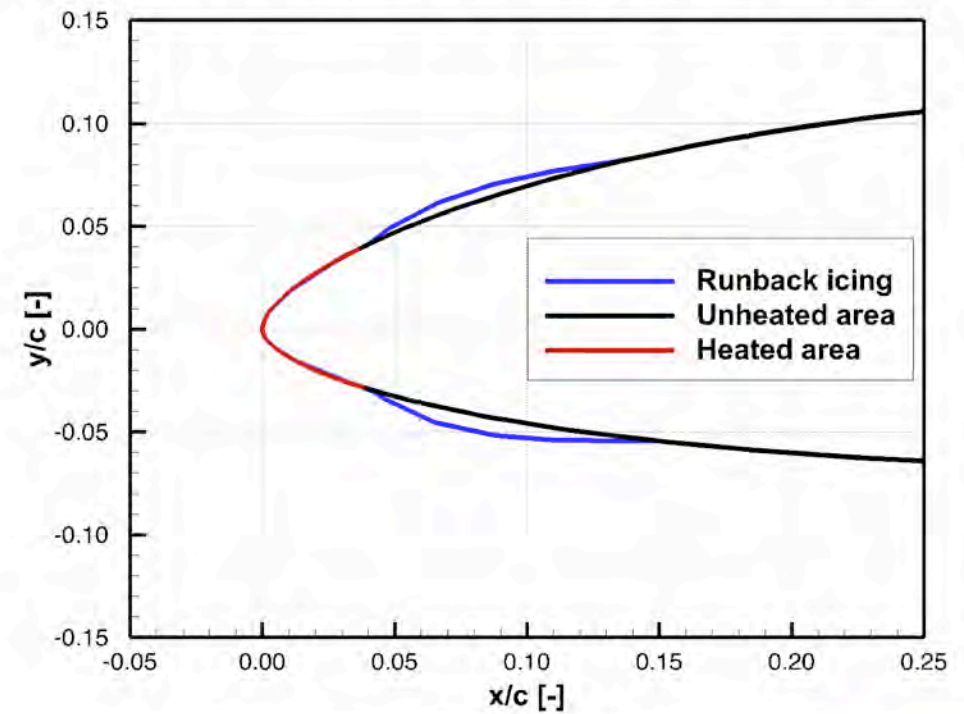
Only the leading edge needs heating.



Heated area is depended on droplet size and water content!



- It is sufficient to only heat the leading edge of an airfoil to prevent icing.
- The area that is required to be heated is depending on the droplets.
- Insufficient heating may lead to icing due to runback water.





Thermal Analysis of a Heated Rotor Blade for Wind Turbines

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