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Development of a reliable modeling system for the calculation of rime ice loads on overhead transmission lines

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FRonTLINES - main objective :

”To develop a toolbox for assessing frost and rime ice impacts on overhead power lines”



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Meteorologisk
institutt

UiT / NORGES ARKTISKE
UNIVERSITET
Statnett



The Research Council
of Norway

Development of icing test stations

Meteorological
measurements

420 kV line

Test span

Ice sensor

Power
supply

Ålvikfjellet (1100 m a s l)

Test station - Instrumentation

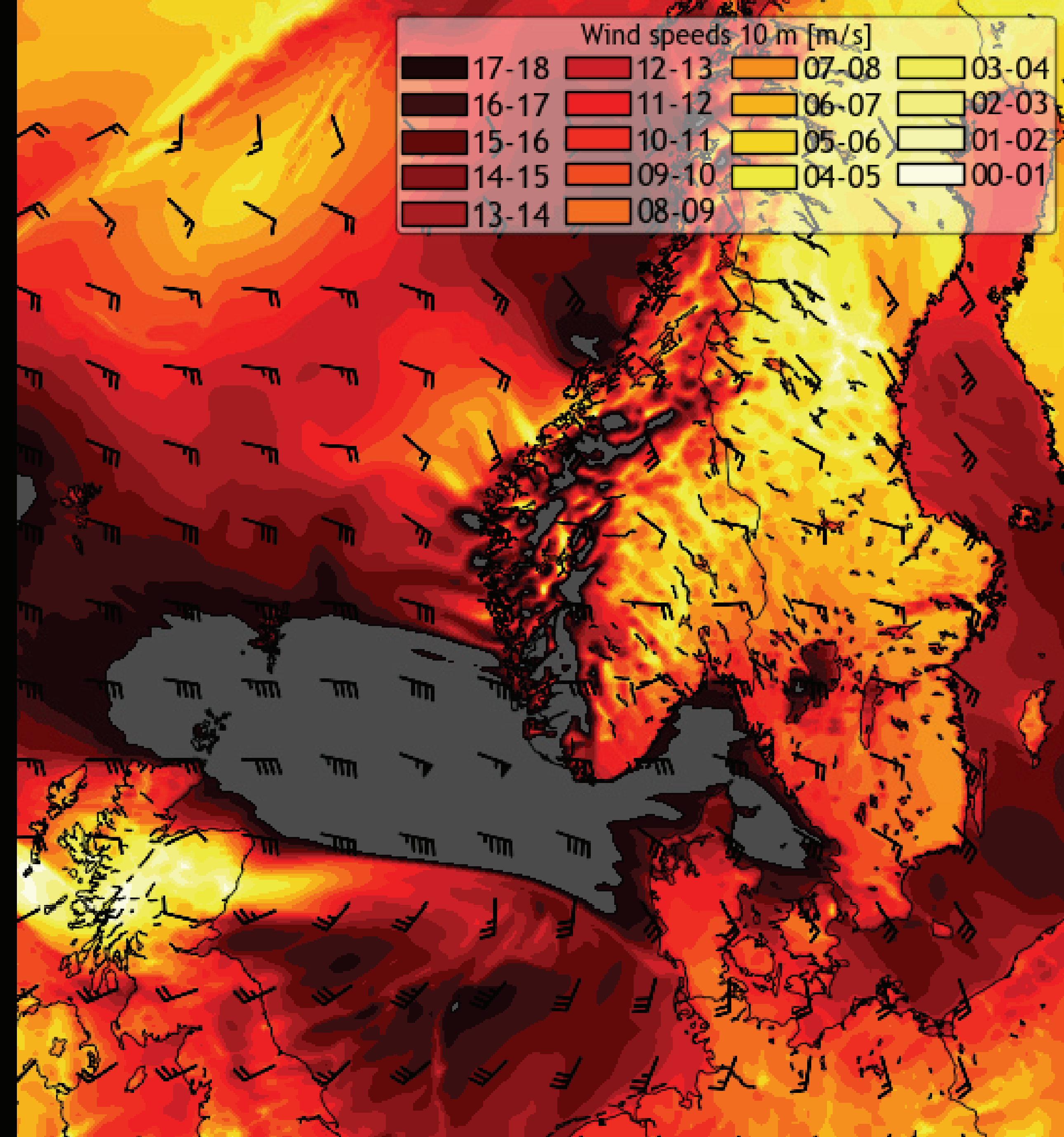
- Ice load measurements with vertical cylinder with forced rotation (IceTroll)
- Load tension recorders on the power line and test span
- Wind measurements with a heated ultrasonic anemometer
- Temperature measurements
- Web cameras



WRF model simulations

Understand and explain the meteorological processes that result in icing buildup

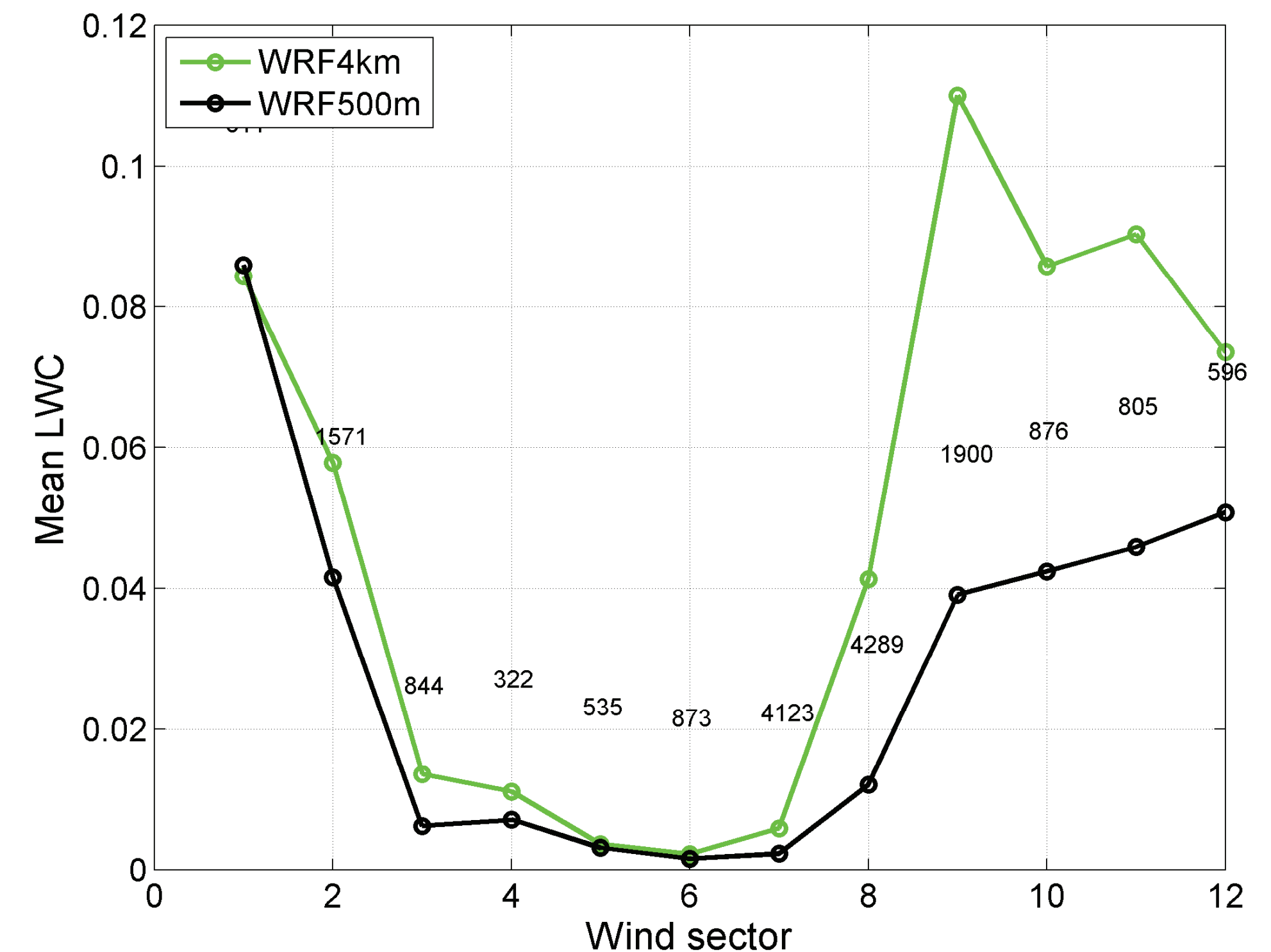
- Long term calculations 1979-2017:
 - 4 km resolution
 - Large coverage
- Fine scale simulations:
 - 500 m resolution
 - Local coverage



Statistical downscaling methods

- Account for **unresolved terrain** in the long term time series
- By the use of **quantile regression** methods the sectorwise distribution of LWC is adjusted to the results from the fine scale model.

Liquid water content

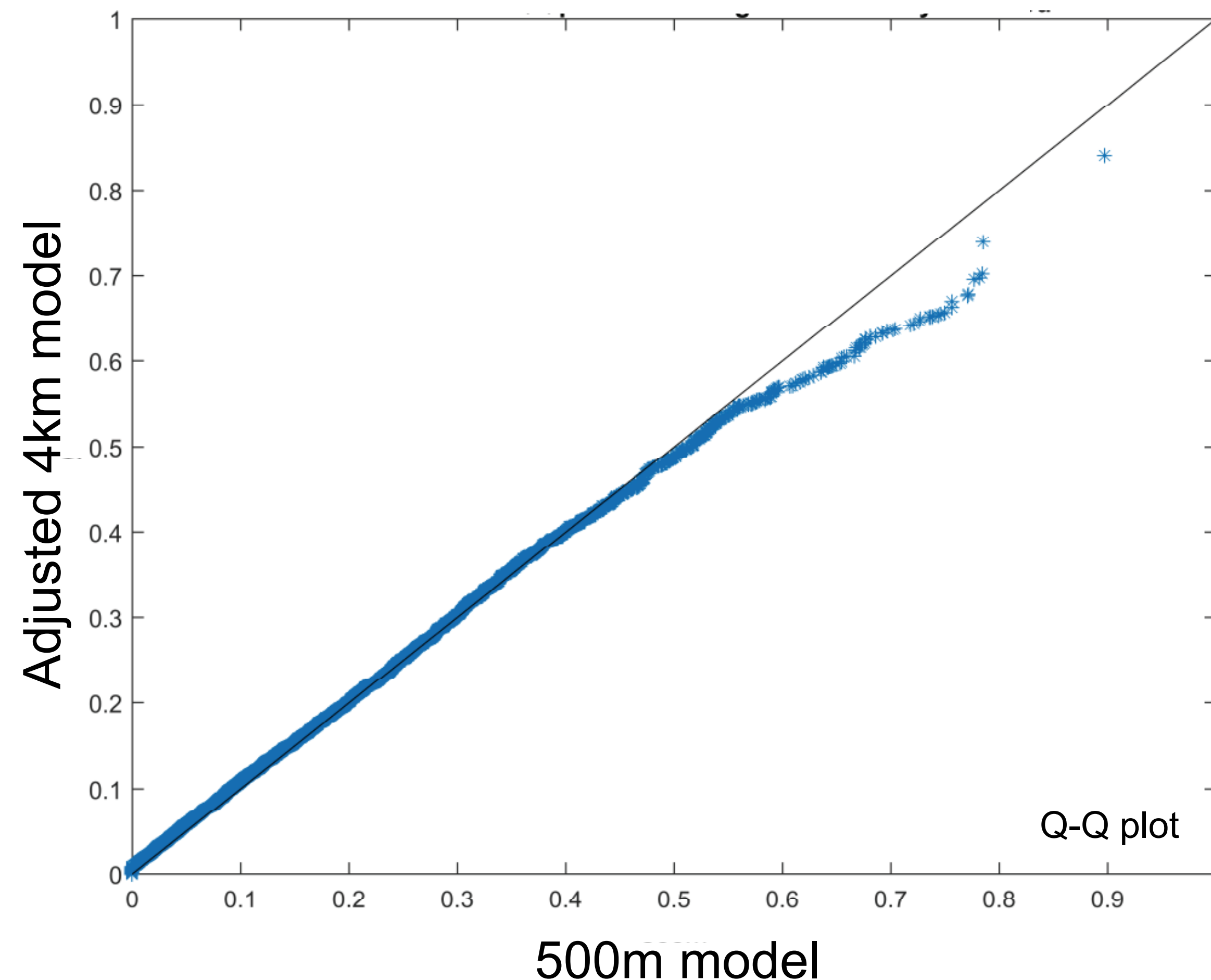


Example: Location with considerable sheltering in sectors 8-11

Statistical downscaling methods

- Account for **unresolved terrain** in the long term time series
- By the use of **quantile regression** methods the sectorwise distribution of LWC is adjusted to the results from the fine scale model.

Liquid water content



Modelling ice accretion

Icing intensity on rotating cylinder (reference object):

$$\frac{dM}{dt} = \alpha_1 \alpha_2 \alpha_3 \cdot LWC \cdot A \cdot V$$

α_1 – collision efficiency, $\alpha_1 = f(V, d, D)$

α_2 – sticking efficiency, $\alpha_2 \approx 1$

α_3 – accretion efficiency, $\alpha_3 = f(V, d, LWC, T, e, D, \alpha_1)$

LWC – cloud liquid water content

A – collision area, perpendicular to flow

V – wind speed

d – droplet diameter

D – cylinder diameter

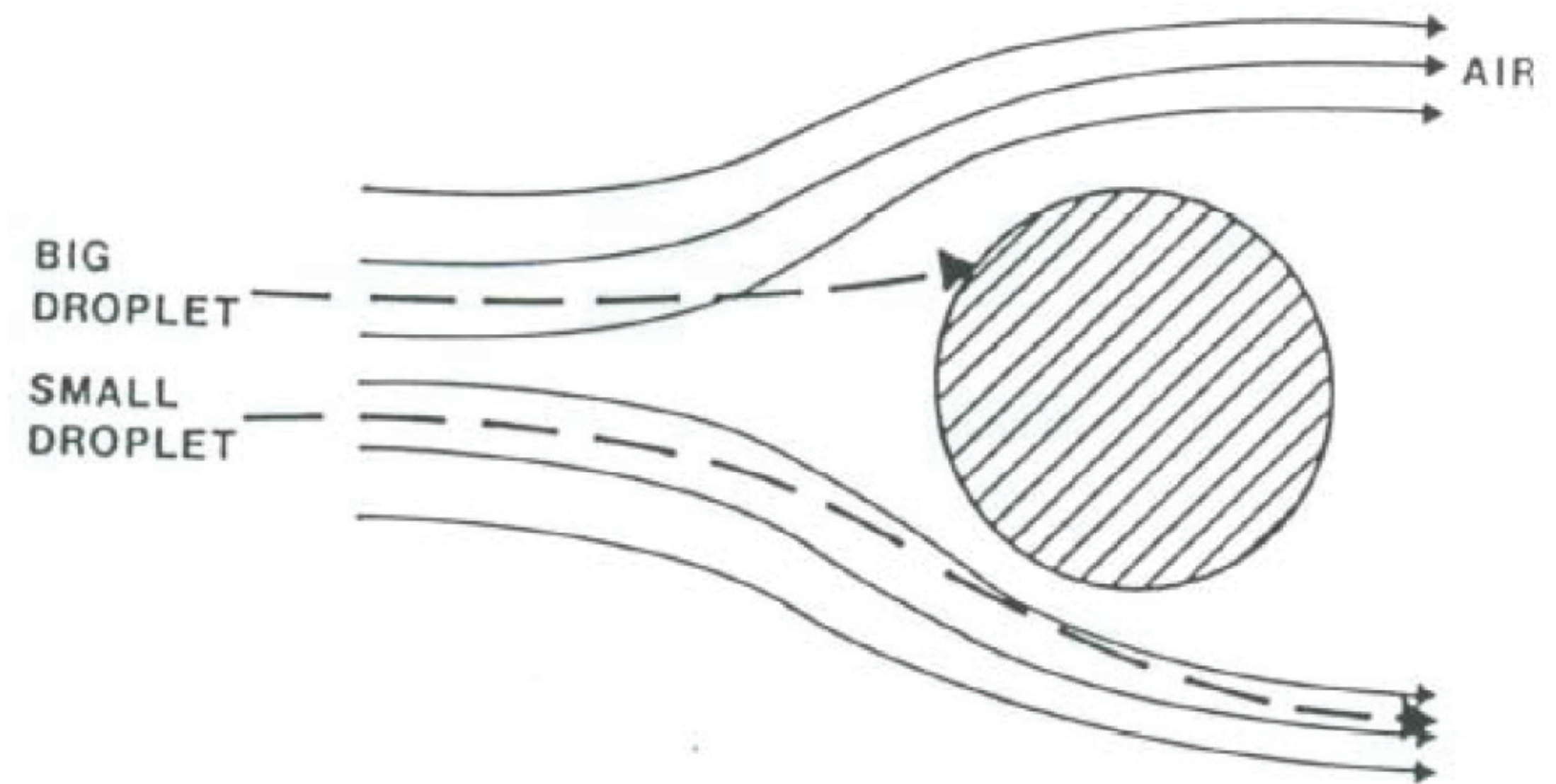
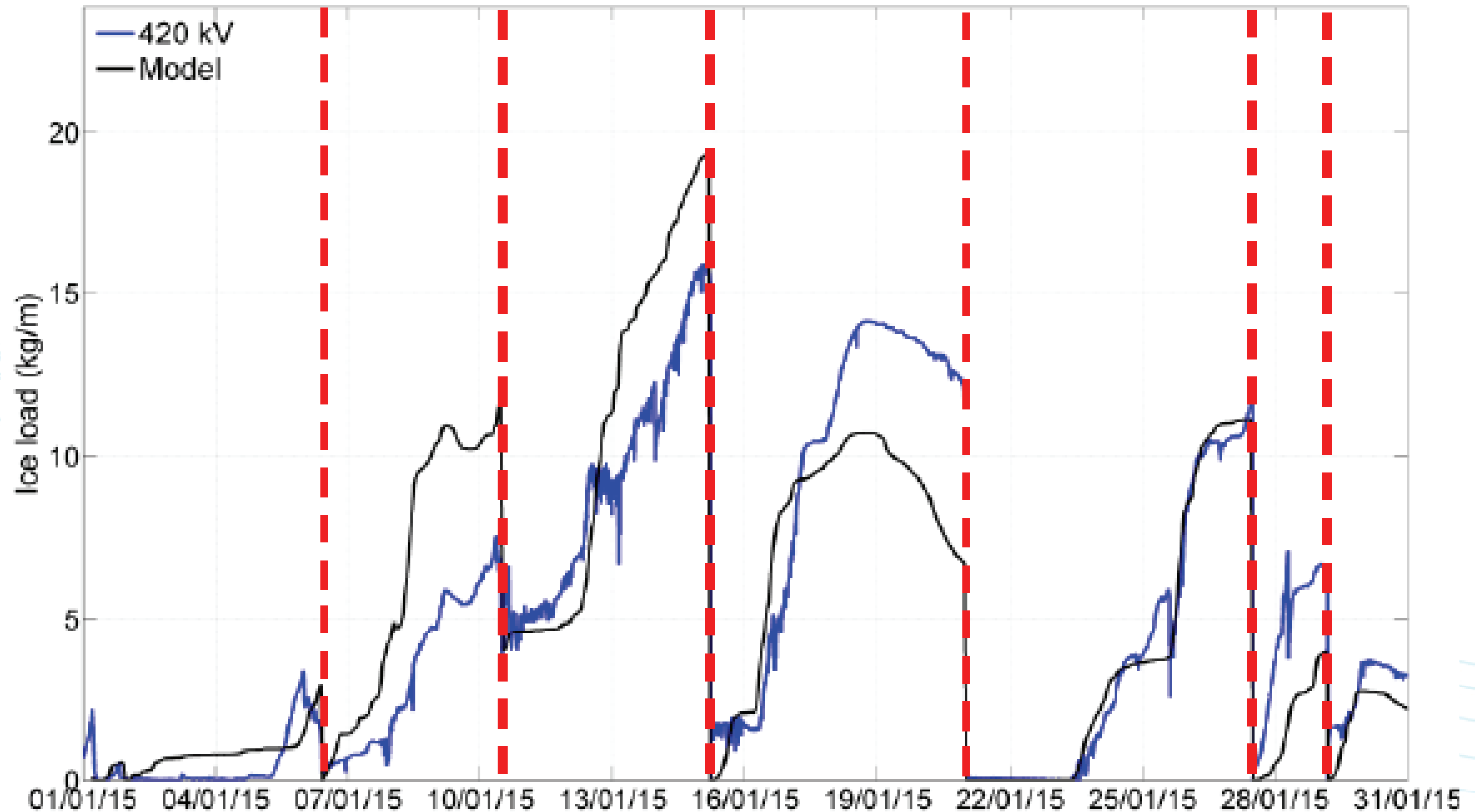
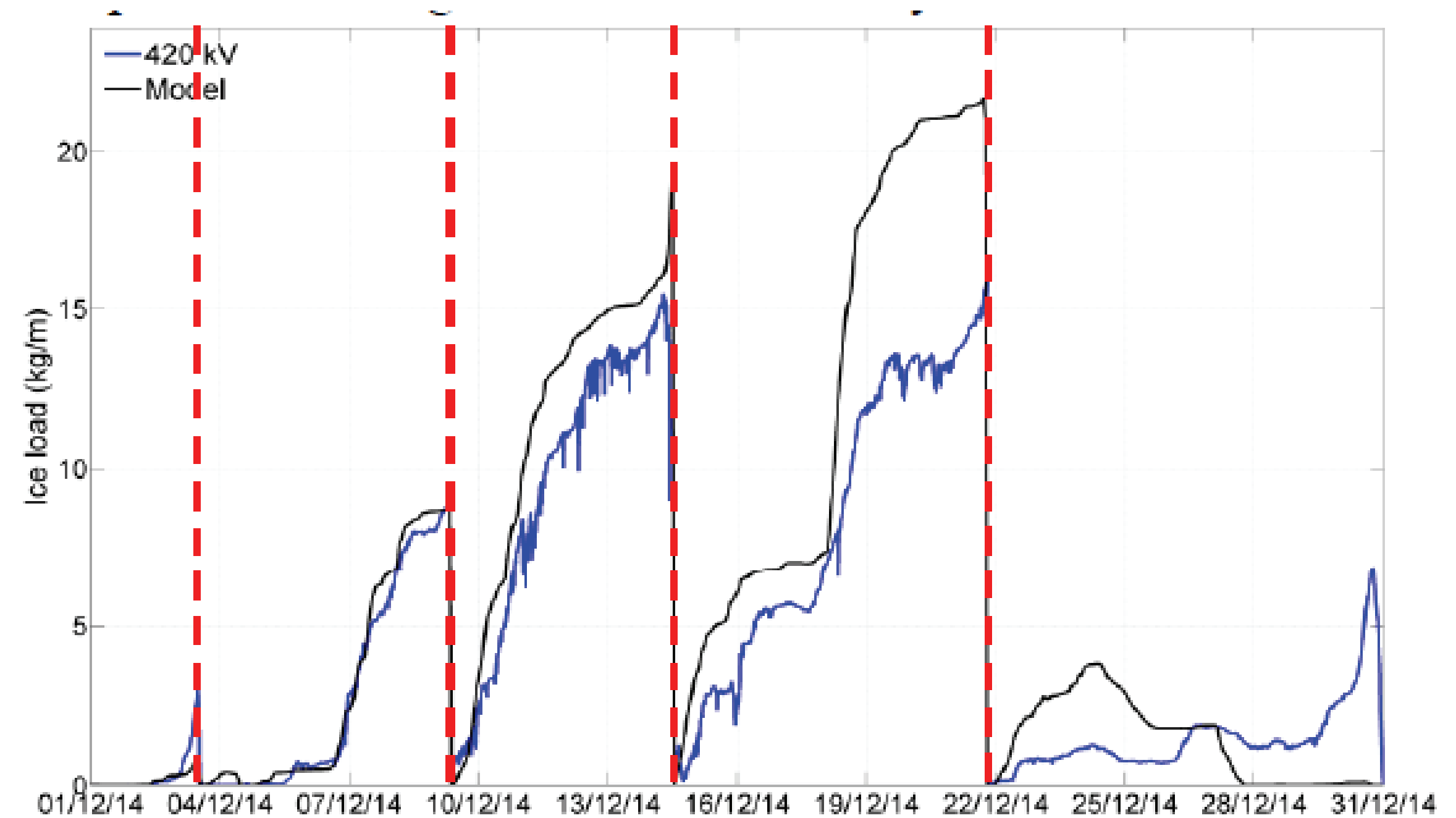


Figure 9 Air flow around a cylinder (from ISO 12494, Annex C, Figure 1)

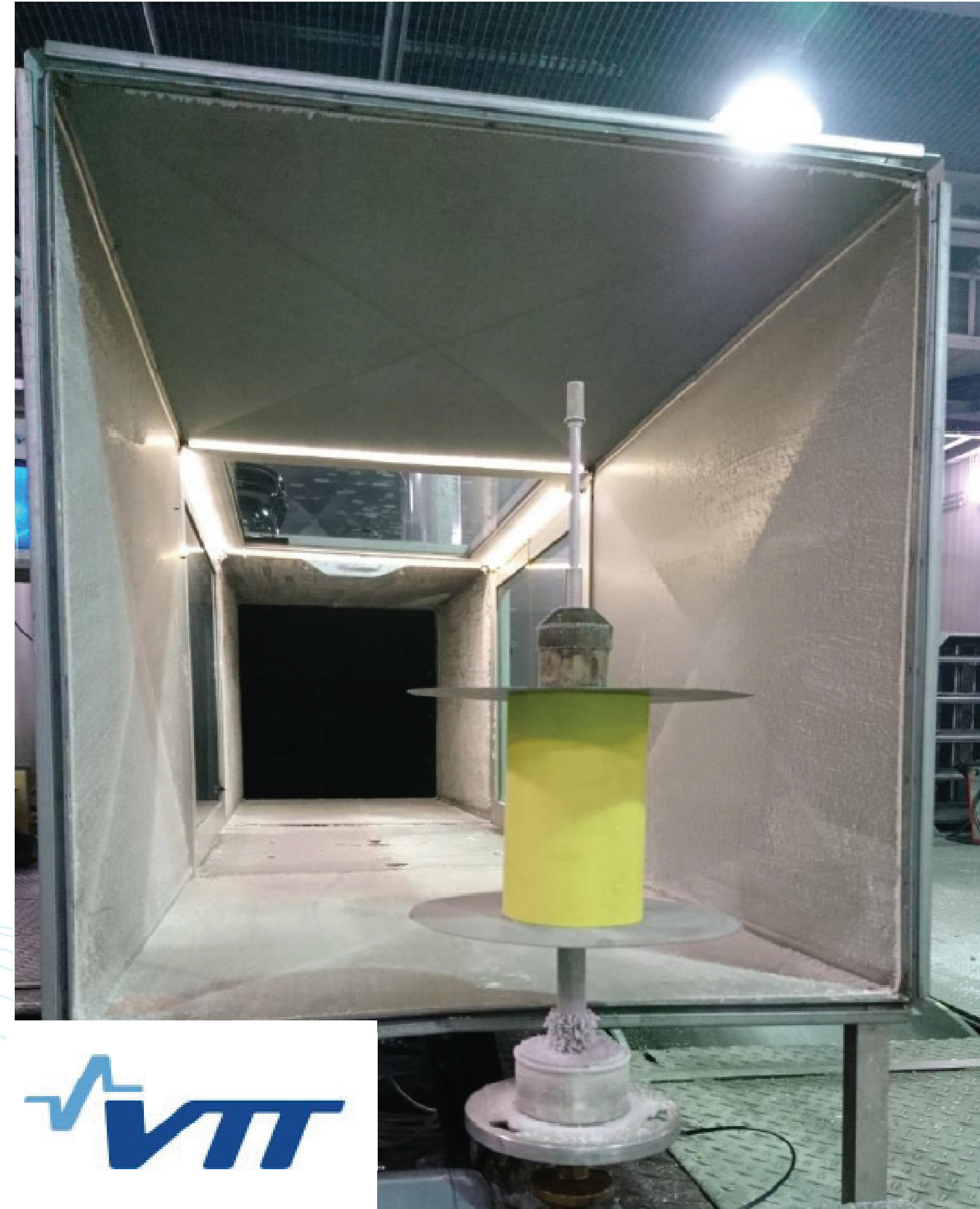
Modeling the ice load

- Ice load modeled from WRF compared to observations from the 420 kV power line
- Ice shedding not modeled. The ice load in the model is reset every time the ice sheds off the power line



Wind tunnel tests

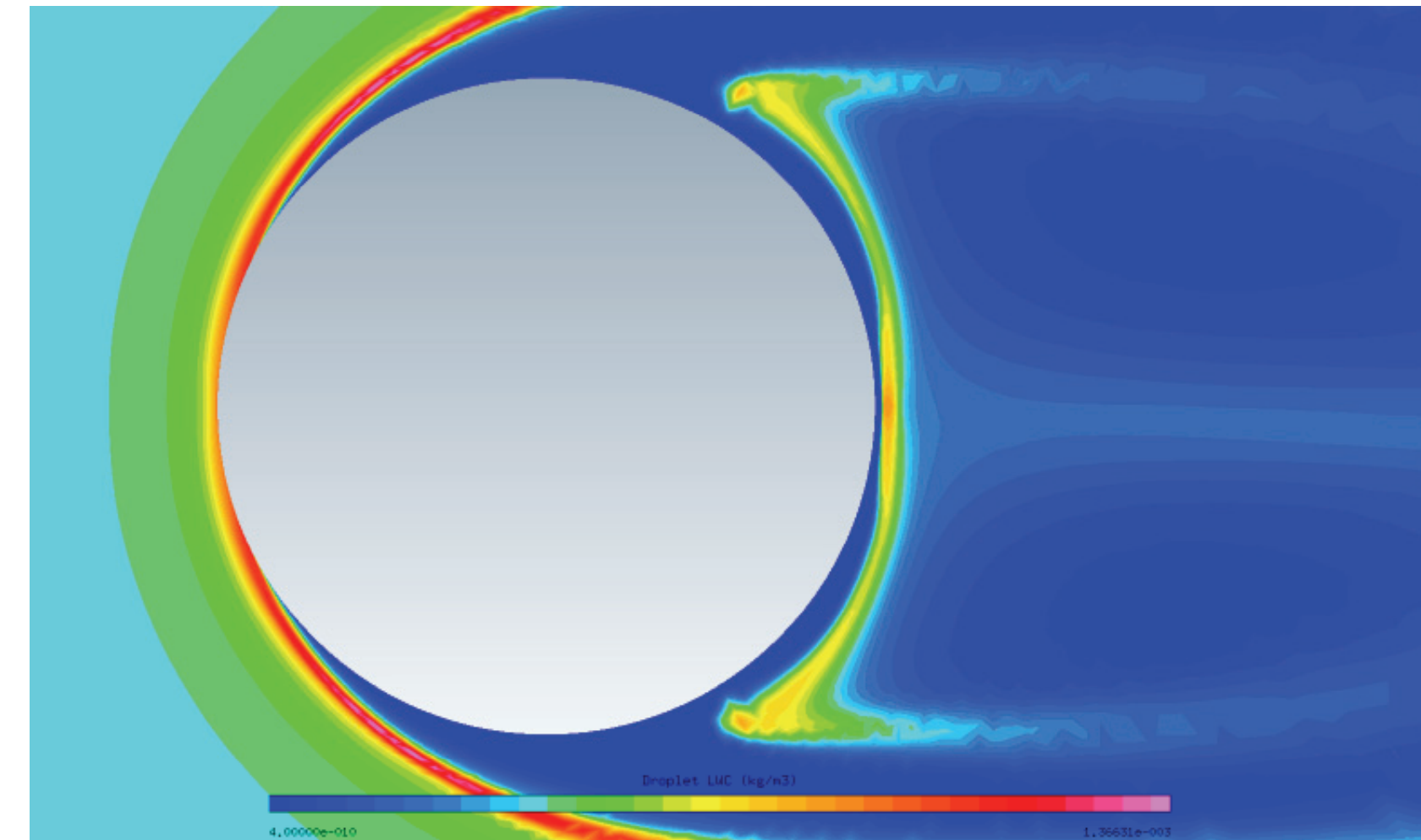
- Study ice accretion under controlled conditions:
 - Influence of surface roughness
 - Large cylinders
 - Low wind speeds
 - Conductor bundles
- Validation and development of ice accretion models



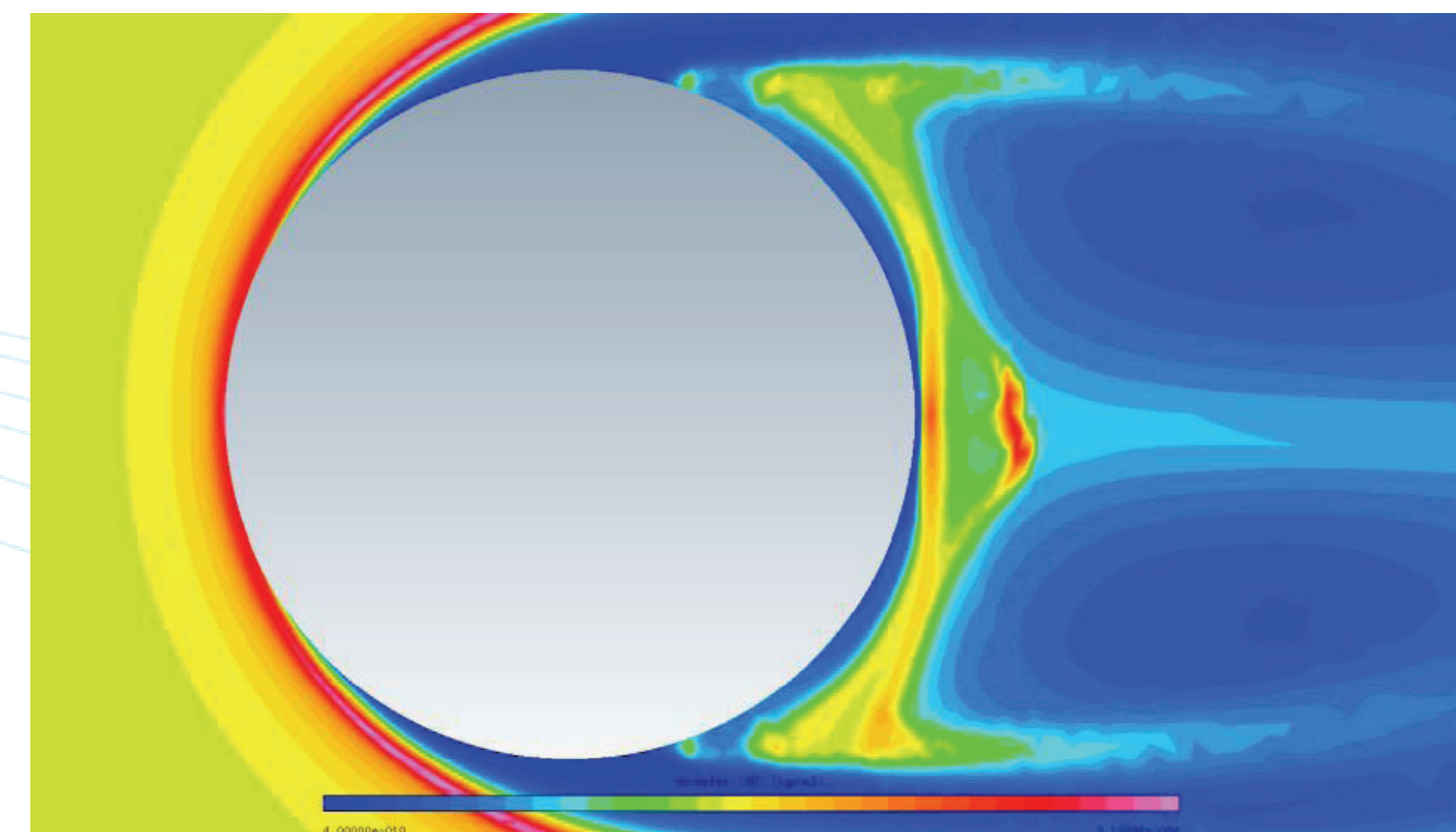
CFD calculation of ice accretion

- FENSAP ICE
- Revealed **limitations to ISO 12494** under the following conditions:
 - Low wind speeds ($<10\text{m/s}$)
 - Large objects ($>15\text{ cm diameter}$)
- Under such conditions the collision efficiency is highly dependent on the **droplet distribution spectra**.

Liquid water content



D=30mm
Mono dispersed
distribution



D=30mm
Langmuir D
distribution

Hoar frost

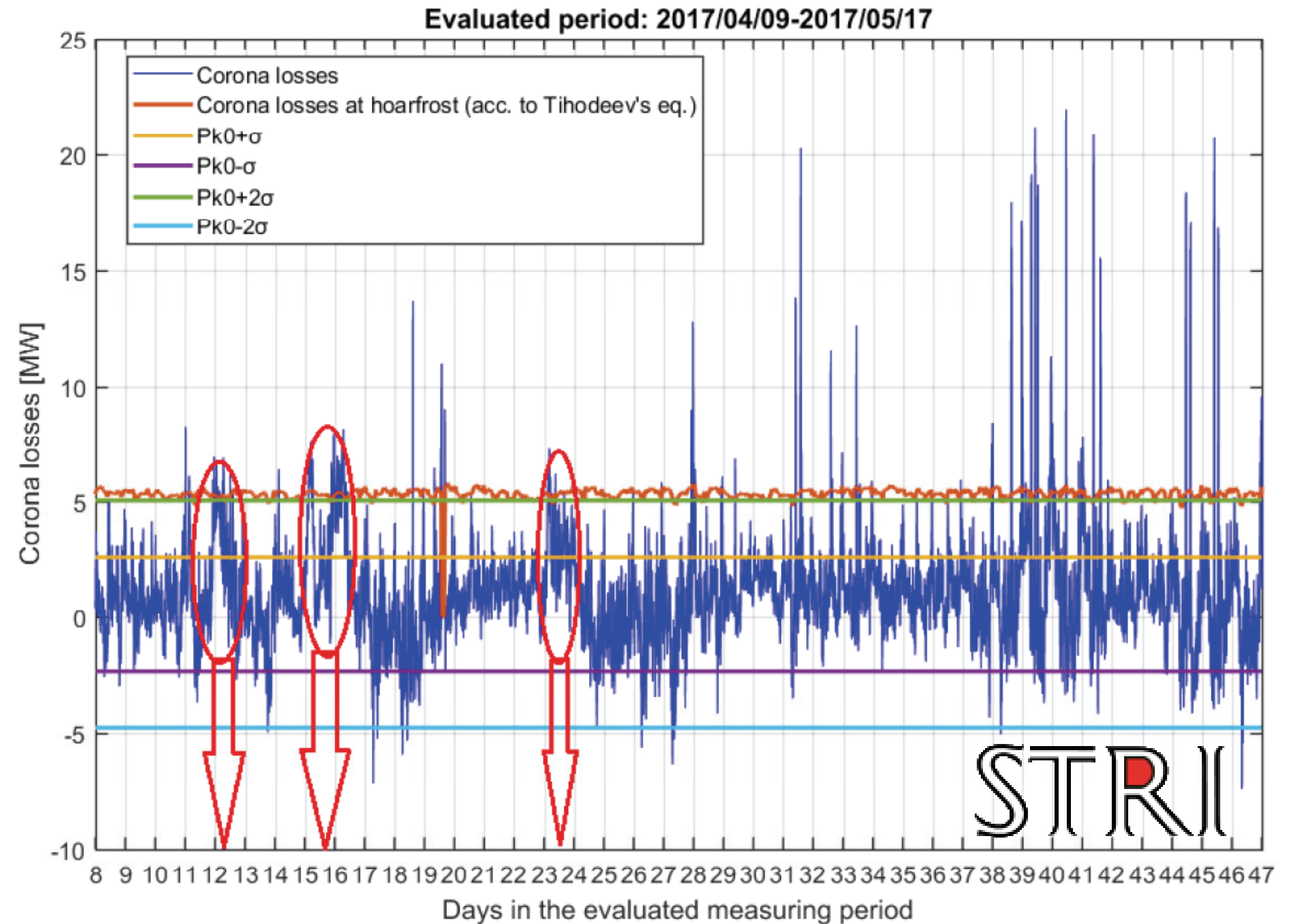
Hoar frost on conductors may cause high power losses due to **corona discharge activity** on the hoar frost needles.



Example of hoar frost on a conductor

Hoar frost

- A method to identify and quantify hoar frost corona losses has been developed
- The example shows 3 such events during April 2017 on a 420 kV line



FRonTLINES in summary

- **3 icing test stations** has been established
- Meteorological models have been developed and improved to **calculate icing in complex terrain**
- CFD calculations and wind tunnel experiments have been applied to **increase our understanding and study the limitations** to the current ice accretion models.
- Methods to **identify and quantify hoar frost corona losses** from power lines have been developed



Ålvikfjellet test station
(Photo: Øyvind Welgaard, Statnett, Feb 02 2018)

Thank you for your attention!

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