



KJELLER  
VINDTEKNIKK

# Analysis of the icing conditions for offshore wind power in Norwegian waters

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# Background

- NVE (Norwegian Water Resource and Energy Directorate) have established focus areas for offshore development wind power in Norway (Havvind, 2010)
- 15 focus areas suggested.
- focus areas suggested based on a large number of criteria, also climatic considerations and icing.



# In-cloud icing

- Calculation of icing at different coastal locations based on cloud height observations
- Icing from supercooled droplets will be a minimal problem for offshore turbines with 100m hubheight

number of hours of icing per year at 300m and 400m height

<i>Flyplass</i>	<i>300m</i>	<i>400 m</i>
Røst	44	160
Andøya	72	222
Hasvik	36	162
Berlevåg	46	160
Vardø	57	164



# Sea spray

- Strong winds generate sea spray.
- In combination with low temperatures, icing from sea spray is known to be challenging for vessels



A dangerous coating of ice on the NOAA Ship Miller Freeman in the Bering Sea, Alaska. Such icing can affect a ship's stability and cause capsizing. Photo from the NOAA Library Ship Collection. Photo courtesy of NOAA NMAO Pacific Marine Center



The forward bulkhead of the Research Vessel Knorr during a scientific cruise in the Labrador Sea in late winter 1997. Photographed by George Tupper. From Pickart (1997) in Oceanus Magazine.

# Sea spray icing

- The amount of sea spray is related to the wind speed near the water surface.
- In combination with low temperatures sea spray will freeze.
- Simple algorithm used in forecasting of sea spray icing for offshore vessels (Overland, 1990):

$$PPR = \frac{V_a (T_f - T_a)}{1 + 0.3(T_w - T_f)}$$

**PPR** = Icing Predictor

**V<sub>a</sub>** = Wind Speed (m s<sup>-1</sup>)

**T<sub>f</sub>** = Freezing point of seawater (usually -1.7 °C or -1.8 °C)

**T<sub>a</sub>** = Air Temperature (°C)

**T<sub>w</sub>** = Sea Temperature (°C)

# Icing Predictor

PPR	<0	0-22.4	22.4-53.3	53.3-83.0	>83.0
Icing Class	None	Light	Moderate	Heavy	Extreme
Icing Rates (cm/hour) (inches/hour)	0	<0.7 <0.3	0.7-2.0 0.3-0.8	2.0-4.0 0.8-1.6	>4.0 >1.6

$$PPR = \frac{V_a (T_f - T_a)}{1 + 0.3(T_w - T_f)}$$

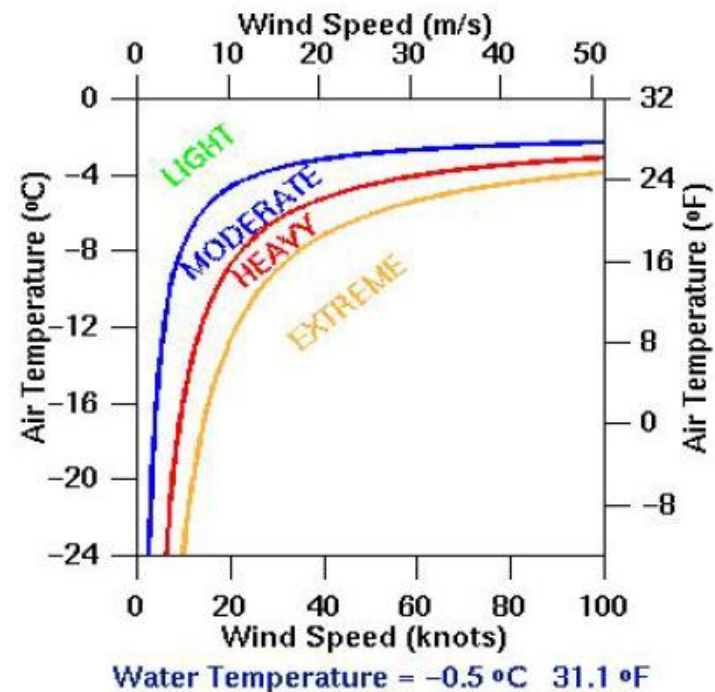
PPR = Icing Predictor

$V_a$  = Wind Speed ( $m\ s^{-1}$ )

$T_f$  = Freezing point of seawater (usually  $-1.7\ ^\circ C$  or  $-1.8\ ^\circ C$ )

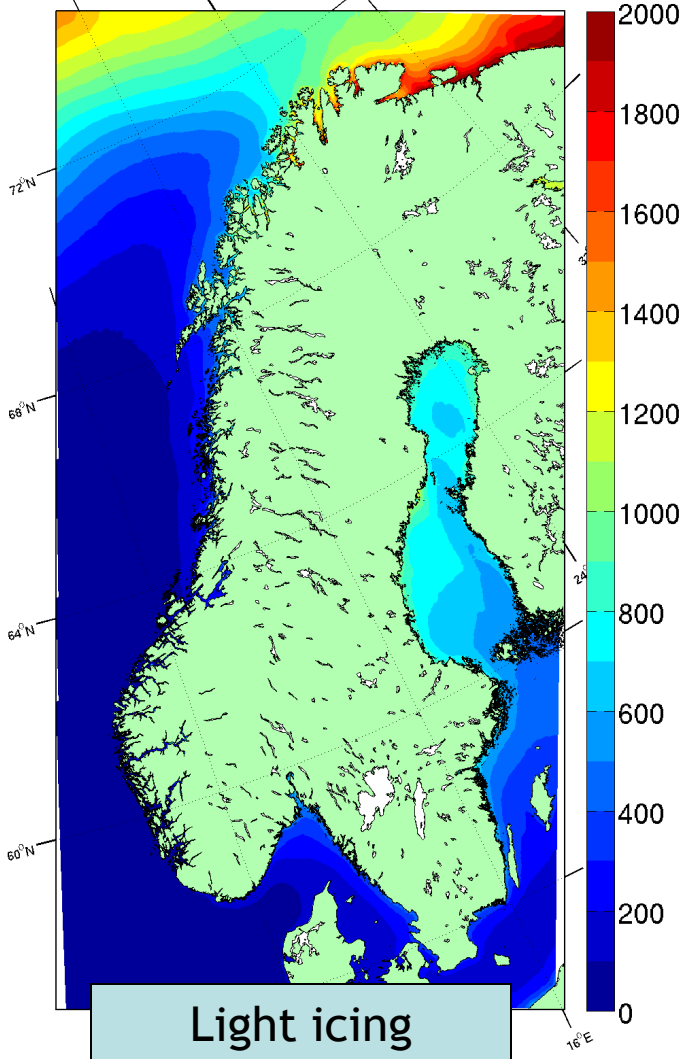
$T_a$  = Air Temperature ( $^\circ C$ )

$T_w$  = Sea Temperature ( $^\circ C$ )



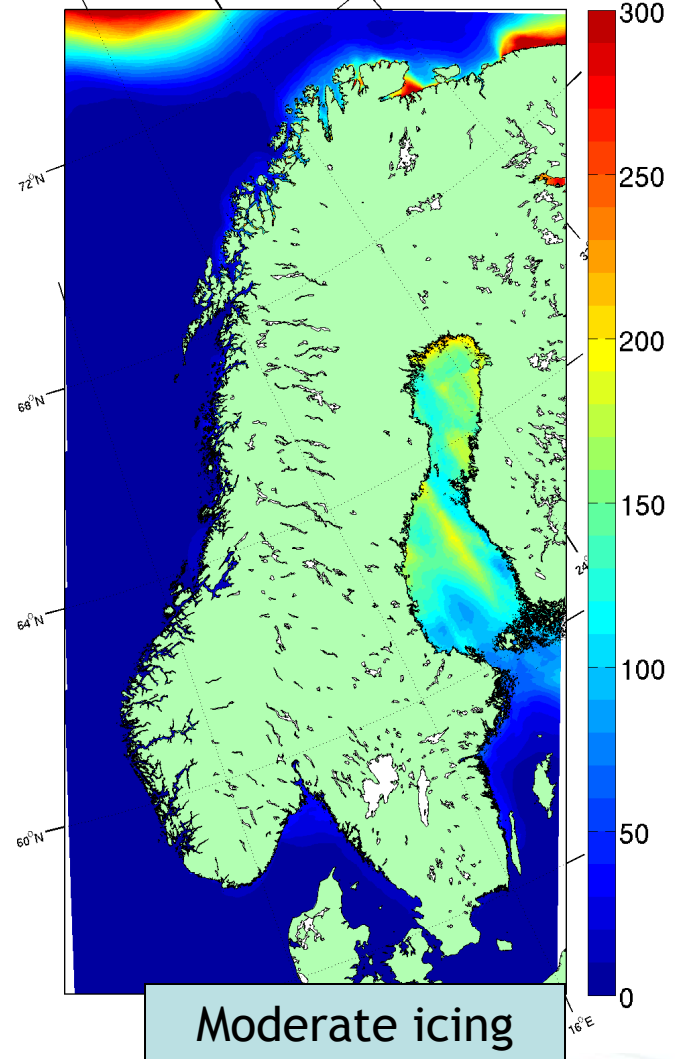
# Frequency of sea spray icing

Frequency of PPR in [0-22] [hours/year]



Light icing

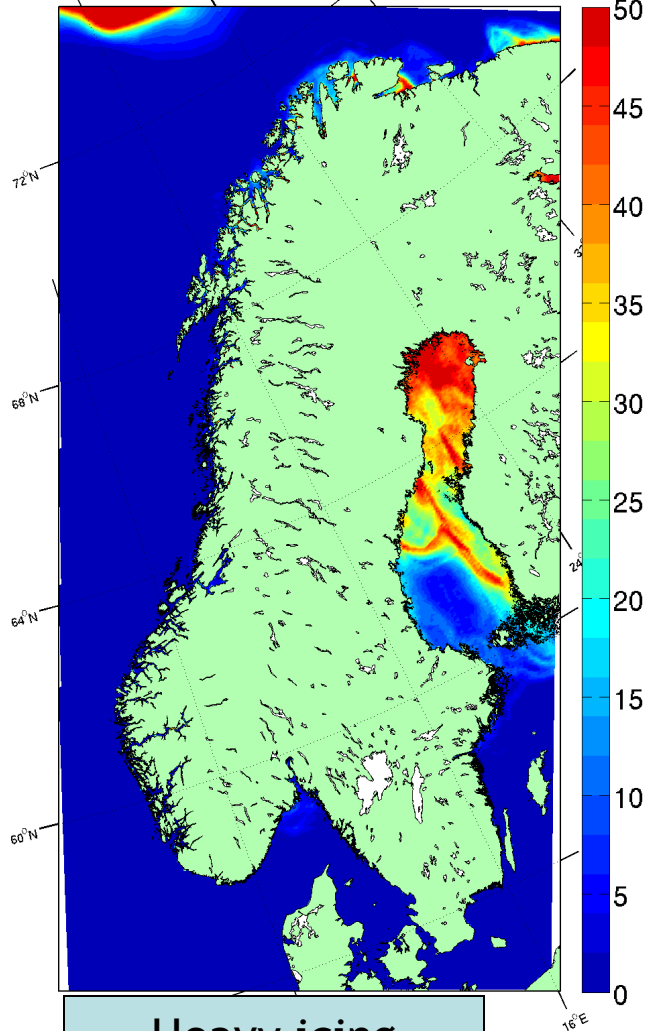
Frequency of PPR in [22-53] [hours/year]



Moderate icing

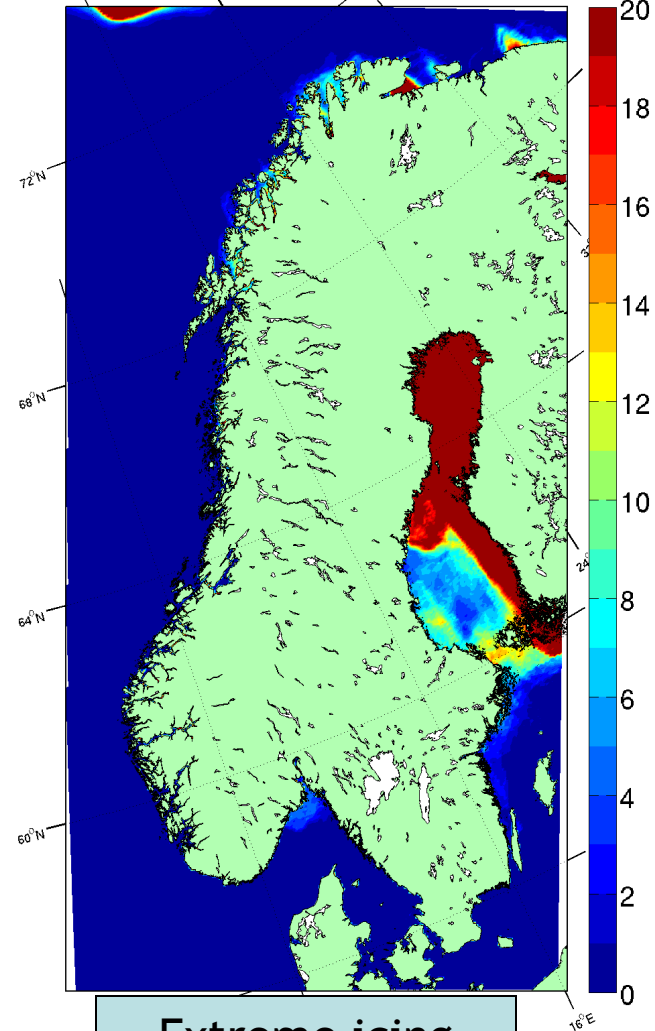
# Frequency of sea spray icing

Frequency of PPR in [53-83] [hours/year]



Heavy icing

Frequency of PPR in [83-1000] [hours/year]



Extreme icing



# Frequency of sea spray icing

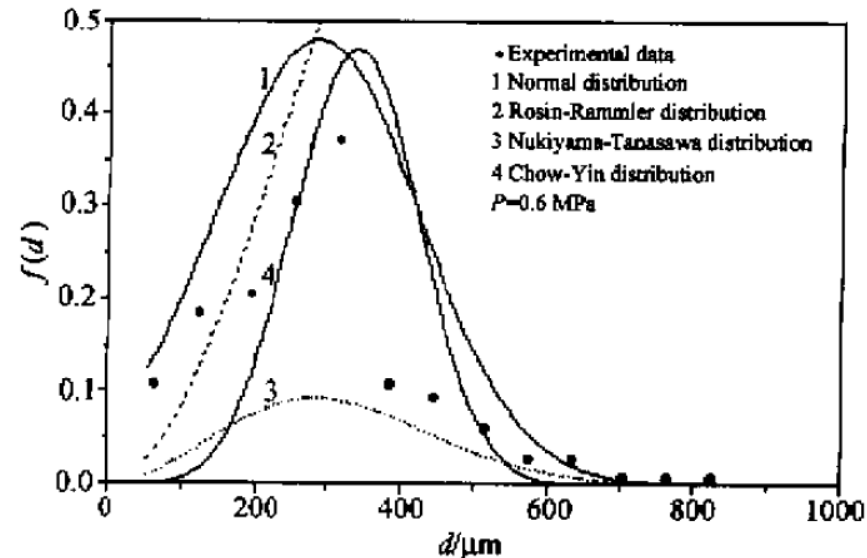
- We will experience cases with sea spray icing in the northern part of the Norwegian coastline.
- But will this be a problem for wind power operations?
- How far up does the sea spray reach?

# Vertical extent of sea spray

- typical median droplet size:
  - sea-spray: 200-300 $\mu\text{m}$
  - cloud droplets: 10-20 $\mu\text{m}$

Sea spray consists of large droplets that does not reach very high.

Over a **free water surface** the number of sea-spray droplets over 20m height will be minimal



Figur 6-3 Dråpefordeling fra et eksperiment. Fra Wang Xishi et.al (2002).

# Sea spray, wave collisions



# Sea spray, wave collisions

- Wave collision will allow the sea spray to reach higher
- some empirical models have been made to estimate this:
  - ICEMOD:  $G(z, U_{10})$
  - Forest et al 2005:  $LWC(z, H_s), H_s(U_{10})$

# F\_L\_G

- Forest et al. (2005):

$$LWC(z) = 1.35 H_s^2 \exp(-0.53z)$$

$H_s = H_s(U_{10})$ , significant waveheight

$U_{10} = 10 \text{ min average wind speed at } 10 \text{ m height}$

# ICEMOD

Horjen and Vefsnmo (1986), Jørgensen et al. (1986):

- $G(z)$  - sea spray flux [ $\text{kg}/\text{m}^2\text{s}$ ]:

$$\bar{G}(z) = M_0 U_{10} \left\{ 1 - (1 - 10^{-2} U_{10}) e^{-\left(\frac{4z'+2}{9}\right)^2} \right\} e^{-k U_{10}^{2/3} (z')^2}$$

$$M_0 = 2\pi 10^{-4} \text{ kg} / \text{m}^3$$

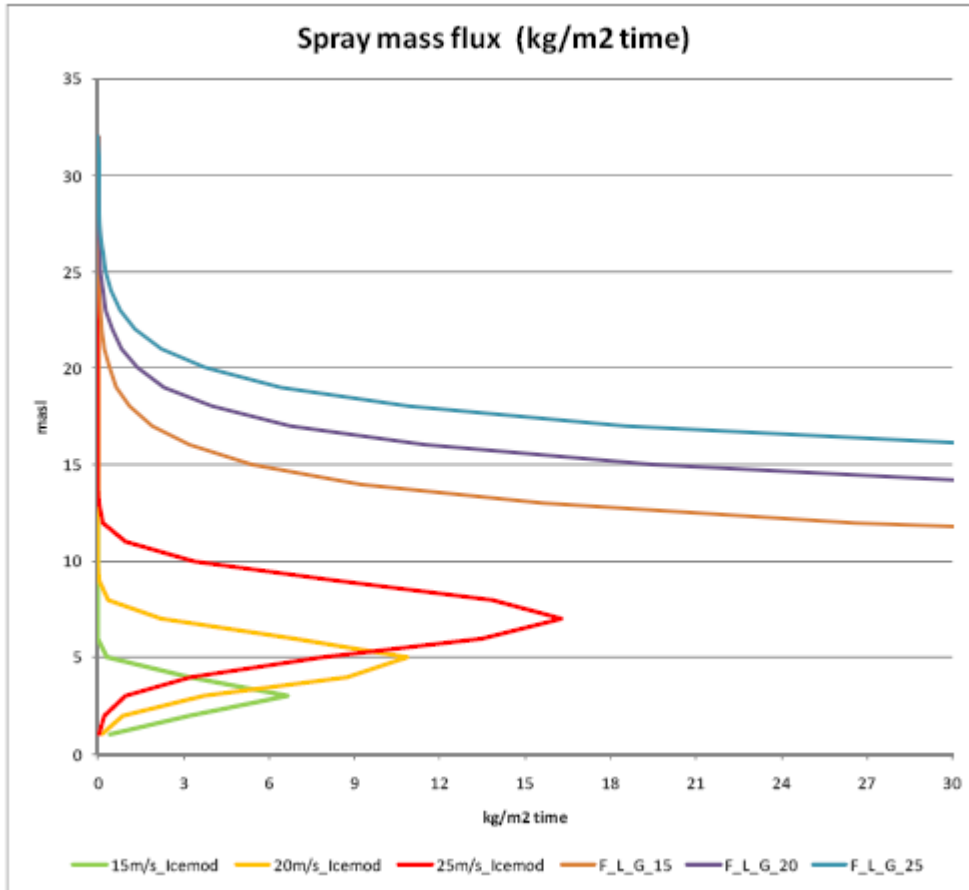
$$k = 5.88 \cdot 10^{-2} (\text{s} / \text{m})^{2/3}$$

$$z' = (2z / H_s) - 1$$

$U_{10}$  = 10 min average wind speed at 10 m height

$H_s$  =  $H_s(U_{10})$ , significant waveheight

# Vertical extent of sea spray



Limit for icing > 10g/hr:

<i>v</i>	<i>ICEMOD</i>	<i>F_L_G</i>
15 m/s	7 m	28 m
20 m/s	10 m	30 m
25 m/s	14 m	33 m

small values above 30 m

# Summary

- Icing from low clouds will be negligible for the offshore wind farms
- Icing on the rotor blades will also be minimal above 30 m height
- icing on the turbine tower and the access to the turbines is probably the largest challenge considering offshore icing in Norwegian waters.